

## SSC DETECTOR SOLENOID DESIGN NOTE #20

TITLE: Charge/Discharge Times, Eddy Current Power and Energy  
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SUMMARY: A charge voltage of  $\sim 30$  V will permit the magnet to be charged in about 3 hours with an eddy current power of a few watts in each 2-m coil/LHe vessel module. The eddy current heat load during a fast dump ( $R_{FD} = 0.1 \Omega$ ,  $\tau = 600$  s) is 645 W per 2-m coil module, which would probably quench the module. I propose that the coil be discharged through  $R_{FD}$  only if a quench is detected; otherwise it would be discharged through a slow dump resistor ( $R_{SD} = 0.01 \Omega$ ,  $\tau = 6000$  s,  $P_E'(\text{max}) = 6.5$  W).

## I. Charge time

During a charge

$$V_L = \text{voltage across coil} \\ = L \, dI_L(t) / dt$$

Assuming a constant voltage charge from  $I_L(t) = 0$  to  $5 \text{ kA}$  and  $L$  the inductance of an 8-m assembly (four, 2-m coils in series electrically),

$$t_{\text{chg}} = L I_L(t_{\text{chg}}) / V_L = (60 \text{ H})(5000 \text{ A}) / V_L \\ = 30 \times 10^4 \text{ s} / V_L$$

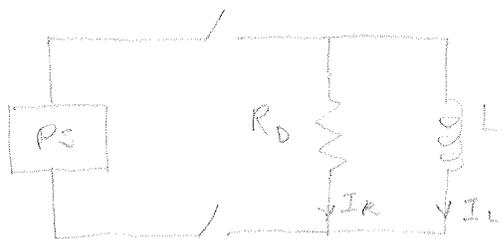
$$P_{\text{PS}}(t) = \text{power drawn from power supply} \\ = V_L [I_L(t) + I_R(t)]$$

$$\text{At } t = 0: I_L(0) = 0, I_R(0) = V_L / R_D$$

$$t = t_{\text{chg}}: I_L(t_{\text{chg}}) = 5 \text{ kA}, I_R(t_{\text{chg}}) \sim 0$$

$$P_{\text{PS}}(\text{max}) = V_L I_L(t_{\text{chg}})$$

Circuit



$$L = 60 \text{ H (8-m unit)}$$

$V_L$ (V)	$P_{PS}$ (max.) (kW)	$dI_L/dt$ (A/s)	$t_{chg}$ (s)	$t_{chg}$ (h)
15	75	0.25	$20 \times 10^3$	5.6
20	100	0.33	$15 \times 10^3$	4.2
30	150	0.50	$10 \times 10^3$	2.8
60	300	1.0	$5 \times 10^3$	1.4

II. Discharge time - fast dump

$R_{FD} = 0.1 \Omega$  to limit discharge to 500V across terminals

$$I_L(t) = I_L(0) e^{-\frac{R_{FD} t}{L}}$$

$$= (5000A) e^{-t/600}$$

$$V_L = I_L(t) R_{FD} \quad (\text{No quench, or for } R_{FD} > R_a)$$

$$= (500V) e^{-t/600}$$

III. Eddy current heating in helium vessel during charge

The changing current in the coil induces a voltage  $V_E = M dI_L/dt$  in the helium vessel and hence an eddy current  $I_E = V_E/R_E$ .

The power dissipated in the vessel due to the eddy current

$$P_E(t) = V_e^2 / R_E = (M dI_L / dt)^2 / R_E$$

where

$M$  = the mutual inductance between the coil and the helium vessel

$R_E$  = circumferential resistance of the helium vessel

To estimate  $R_E$  of J-m module



Plate A :  $1880 \times 35 \text{ mm}^2$

B :  $1880 \times 50 \text{ mm}^2$

C :  $2114 \times 35 \text{ mm}^2$

$A_E$  = cross section of helium vessel

$$= (1880 \times 35 + 1880 \times 50 + 2 \times 2114 \times 35) \times 10^{-6} \text{ m}^2$$

$$= 0.1769 \text{ m}^2$$

$$R_E = \frac{(\rho_{Cu} @ 4.5K) (\text{vessel circumference})}{A_E}$$

$$= \frac{(50 \times 10^{-10} \text{ } \Omega\text{-m}) * (9.5\pi \text{ m})}{0.1769 \text{ m}^2}$$

$$= 84.4 \text{ } \mu\Omega$$

\* From S.O. Machinery Handbook for 304L at 4.5K

To estimate M

M = flux linked by the vessel per unit coil current

$$= \frac{\Phi(I_{L \max}) (1 \text{ turn})}{I_{L \max}}$$

$$\sim \frac{(2T) \left(\frac{1}{4} \pi 9.5^2\right) (1)}{5000}$$

$$= 0.028 \text{ H}$$

To estimate P<sub>E</sub> during charge (2-m module)

$$P_E(t) = (0.028)^2 (dI_L/dt)^2 / 84.4 \times 10^{-6}$$

$$= 9.3 (dI_L/dt)^2 \text{ W}$$

V <sub>L</sub> (V)	dI <sub>L</sub> /dt (A/s)	For 2-m module	
		P <sub>E</sub> (W)	E <sub>E</sub> (kJ)
15	0.25	0.58	11.6
20	0.33	1.01	15.2
30	0.50	2.33	23.3
60	1.0	9.3	46.5

Where E<sub>E</sub> = energy absorbed by helium vessel during charge

$$= P_E t_{\text{chg}}$$

#### IV. Eddy current heating during fast discharge

$P'_E(t)$  = power dissipated during fast discharge - 2-m module

$$= (M \, dI_L/dt)^2 / R_E$$

$$\frac{dI_L}{dt} = \frac{d}{dt} \left( I_0 e^{-t/600} \right)$$

$$= - \frac{I_0}{600} e^{-t/600}$$

$$P'_E(t) = \frac{M^2 I_0^2}{600^2 R_E} e^{-2t/600}$$

$$P'_E(\text{max}) = \left[ \frac{(0.028)(5000)}{600} \right]^2 / R_E$$

$$= 645 \text{ W per 2-m module}$$

$$E'_E(t) = \left( \frac{MI}{600} \right)^2 \frac{1}{R_E} \int_0^{\infty} e^{-2t/600} dt$$

$$= \left( \frac{MI}{600} \right)^2 \frac{1}{R_E} (300) = 300 P'_E(\text{max})$$

$$= 194 \text{ kJ per 2-m module}$$

This heat load appears to be unacceptably large for a routine discharge, i.e. it may cause the coil to quench. Therefore the coil will be discharged through the  $0.1 \Omega$  resistor only if a quench is detected. A "slow" discharge resistor,  $R_D' = 0.01 \Omega$ , could be used to reduce the eddy current heat load to  $6.5 \text{ W}$  during discharge. The energy deposited in the vessel during a slow dump is  $19.4 \text{ kJ}$ .