

# SPREADER BAR

I.D. N<sup>o</sup> 10

COLOR OF BAR :

Red Primer

LOAD CAPACITY PAINTED

ON BAR 22 TONS.

DATE CAP. & I.D. N<sup>o</sup> PAINTED

ON BAR Aug-1988

BAR WT

~ 1550<sup>#</sup>

DATE OF LAST LOAD

TEST. August 9, 1988

TEST LOAD WEIGHT 26.5 TONS

TESTED WITH (2)  
STEEL BLOCKS  
3' x 3' x 6' h.

TEST LOAD % 120.3%

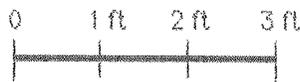
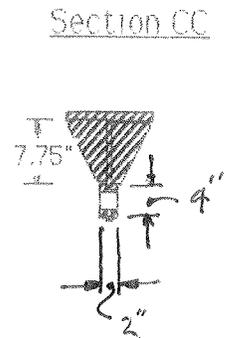
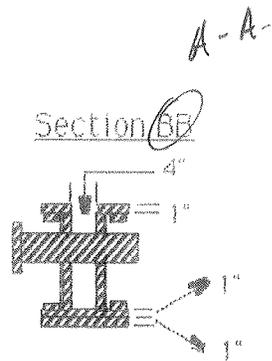
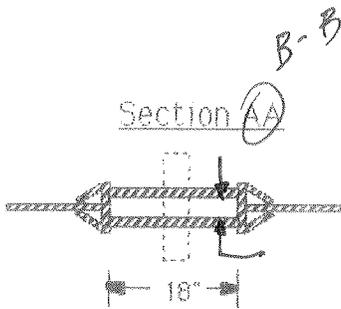
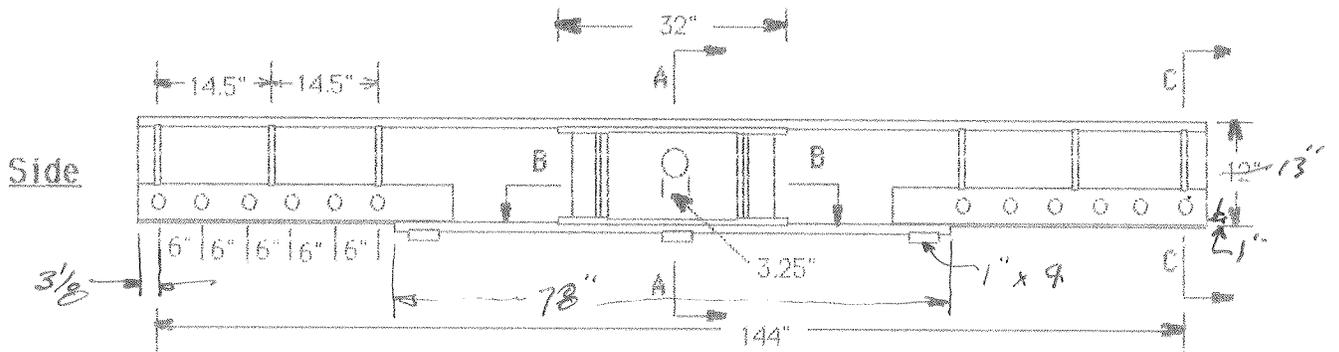
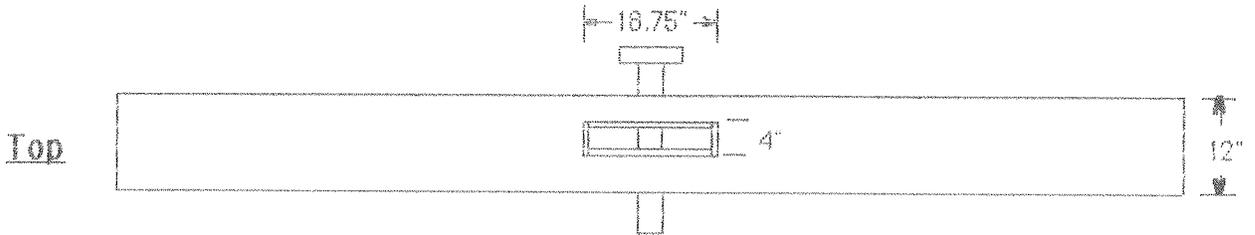
STRESS CALCULATIONS :

DONE BY Bosek & Miranda

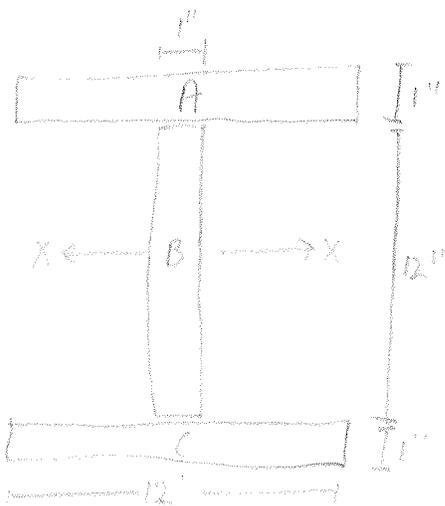
DATE July 1988

REMARKS : TESTED OK

# Primer Q10



scale: 1/2" = 1'



$$I_A = \frac{b^3}{12} = \frac{12}{12} = \underline{1 \text{ in}^4}$$

$$I_B = \frac{(12)^3}{12} = \underline{144 \text{ in}^4}$$

$$I_C = \underline{1 \text{ in}^4}$$

$$A_A = \underline{12 \text{ in}^2} \quad A_B = \underline{12 \text{ in}^2} \quad A_C = \underline{12 \text{ in}^2}$$

$$Y_A = \underline{6.5 \text{ in}} \quad Y_B = \underline{0} \quad Y_C = \underline{6.5 \text{ in}}$$

$$c = \underline{7 \text{ in}}$$

$$\begin{aligned} I_x &= I_A + A_A Y_A^2 + I_B + I_C + A_C Y_C^2 \\ &= 1 + (12)(6.5)^2 + 144 + 1 + (12)(6.5)^2 \\ &= \underline{1160 \text{ in}^4} \end{aligned}$$

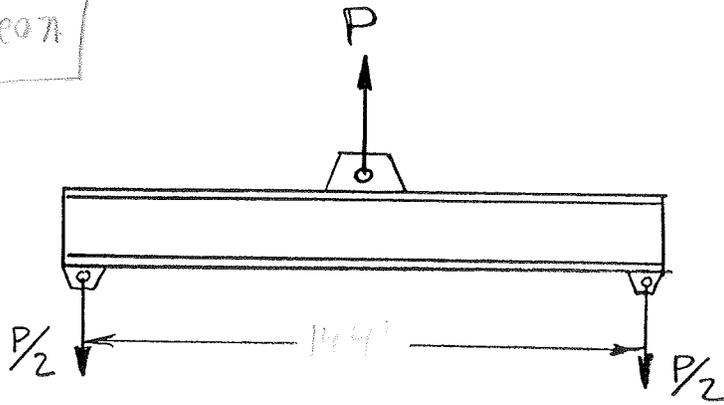
$$S = \frac{I}{c} = \frac{1160}{7} = \underline{165.7 \text{ in}^3}$$

$$\frac{d}{A_F} = \frac{14}{12} = \underline{1.167 \text{ in}^{-1}}$$

SPREADER BAR N<sup>o</sup> 10

PAINT COLOR PRIMER

LEON



BEAM SIZE SPECIAL

$$d = \underline{14 \text{ in}}$$

$$A_w = d \cdot t_w = \underline{14 \text{ in}^2}$$

$$L = \underline{144 \text{ in}}$$

$$d/A_f = \underline{1.167}$$

$$M = \frac{PL}{4} = \underline{36P}$$

$$S_x = \underline{1657 \text{ in}^3}$$

$$V = \frac{P}{2}$$

$$t_w = \underline{1 \text{ in}}$$

BENDING STRESS :

$$F_b \text{ ALLOW} = 12,000 \text{ psi} \checkmark$$

$$\text{OR } F_b \text{ ALLOW} = \frac{12 \times 10^6}{L \cdot d/A_f} = \frac{12 \times 10^6}{(144)(1.167)} = \underline{71,000 \text{ psi}}$$

USE THE LEAST

$$\therefore f_b \text{ MAX} = \frac{M}{S_x} = \frac{36P}{1657} = 12,000 \quad \therefore P = \underline{5,233 \text{ lbs}}$$

SHEAR STRESS :

$$F_v \text{ ALLOW} = \frac{.4 F_y}{3} = 4800 \text{ psi}$$

$$\therefore f_v \text{ MAX} = \frac{V}{A_w} = \frac{P}{2(14)} = 4800 \quad \therefore P = \underline{134,400 \text{ lbs}} = \underline{67.2 \text{ tons}}$$

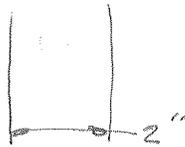
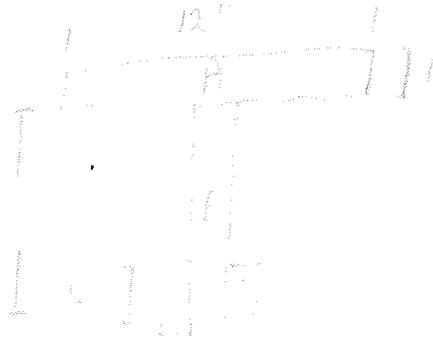
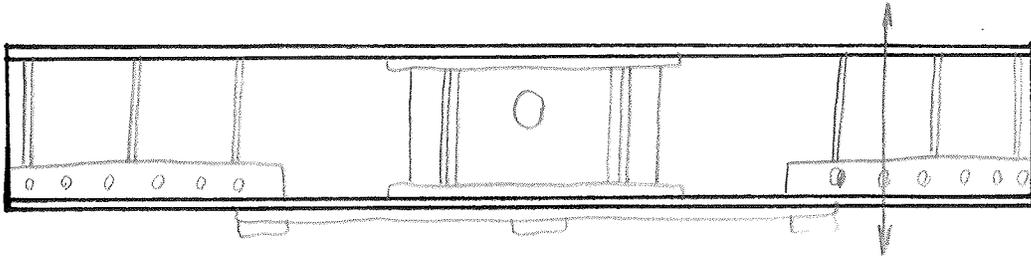
SUMMARY :

$$\therefore P = \underline{27.6 \text{ TONS}}$$

SPREADER BAR No 10

Legs

PAINT Color PRIMER



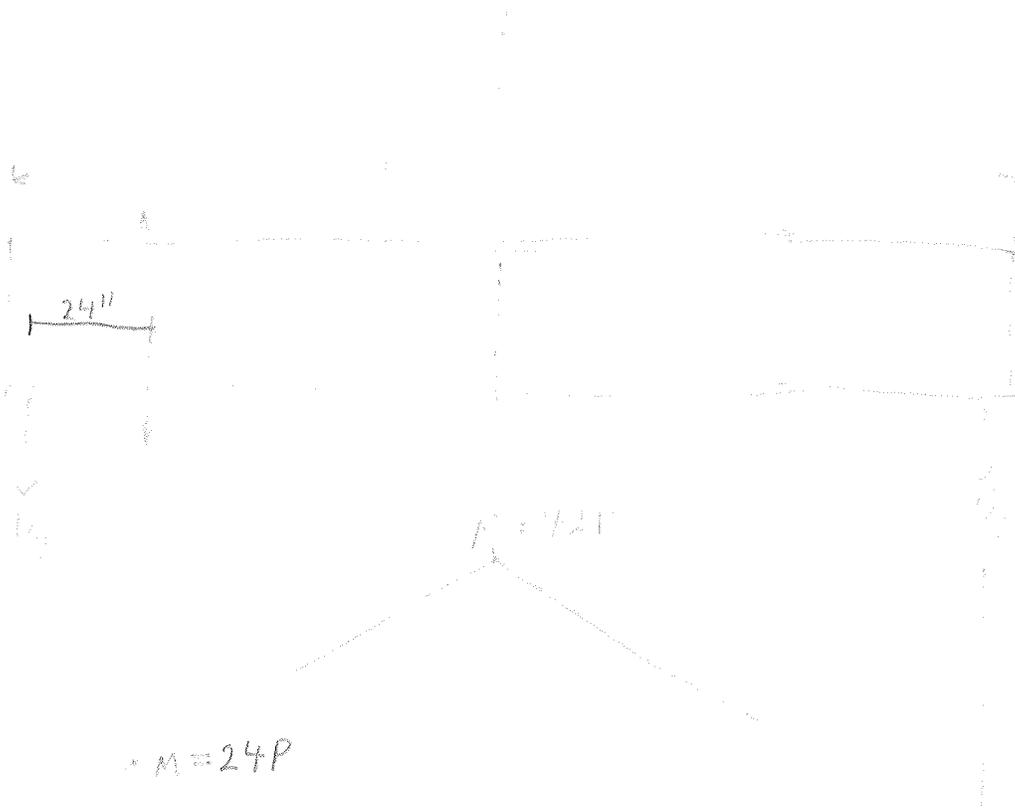
Section	Base (in)	Height (in)	I (in <sup>4</sup> )	Area (in <sup>2</sup> )	r (in)	r' (in)	Ar' <sup>2</sup> (in <sup>2</sup> )
A							
B							
C							
D							
E							

$c = 12.5 \text{ in}$

$I_{xx} = \dots$

$S_{xx} = \dots$

Handwritten notes or scribbles at the bottom right of the page.



24P

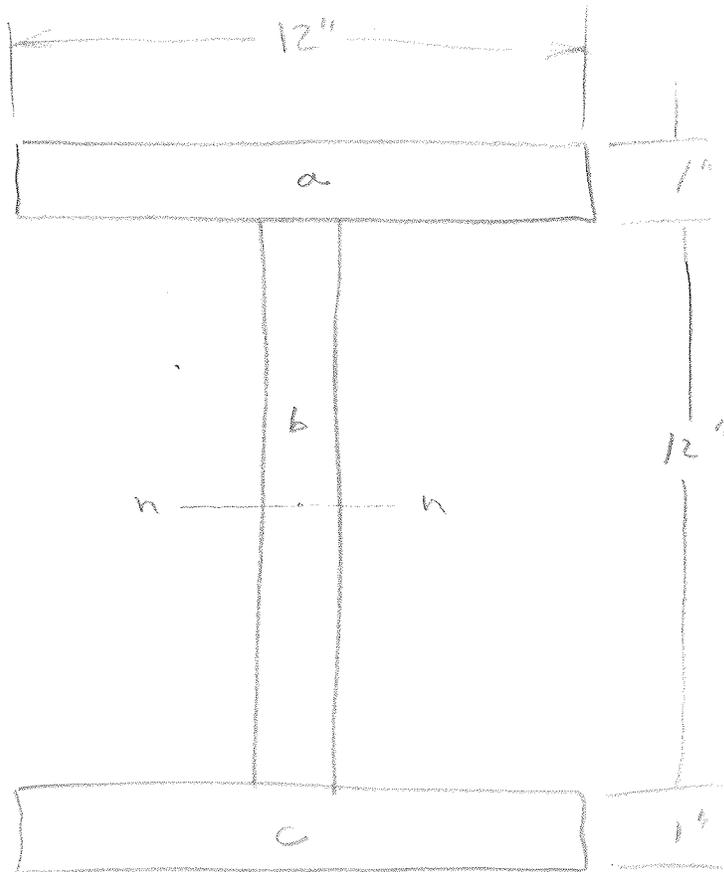
0.3333

X → tonnage adjusted from 27.6 tons  
to 22.24 tons.

SPREADER BAR #10

N. BOSEK

6-28-84



$$I_a = \frac{bh^3}{12} = \frac{12 \times 1^3}{12} = 1$$

$$I_c = 1$$

$$I_b = \frac{1 \times 12^3}{12} = 144$$

$$A_a = A_c = 12$$

$$r_a = r_c = 6.5''$$

$$I_{nn} = I_a + A_a r_a^2 + I_b + I_c + A_c r_c^2$$

$$= 1 + 12(42.25) + 144 + 1 + 12(42.25)$$

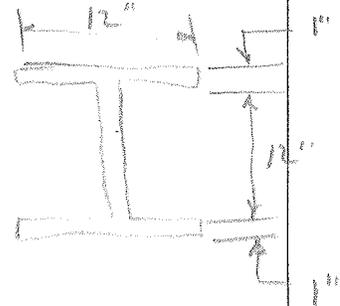
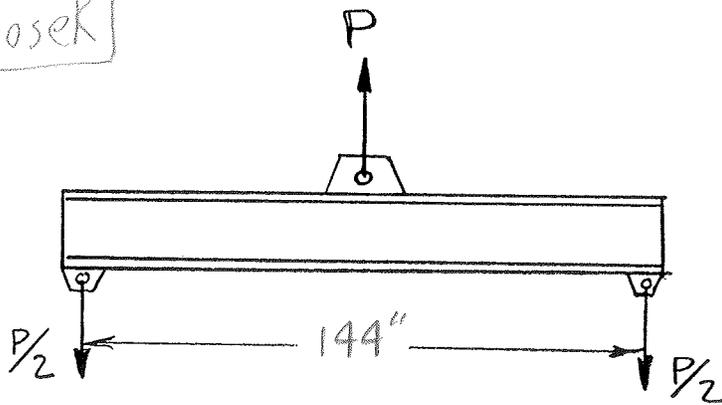
$$I_{nn} = 1160 \text{ IN}^4$$

$$S = \frac{I}{c} = \frac{1160}{7} = 165.714 \text{ IN}^3$$

$$\frac{d}{A_s} = \frac{14}{12} = 1.166$$

SPREADER BAR N<sup>o</sup> 10 PAINT COLOR RED

Bosek



BEAM SIZE SPECIAL

$d = \underline{14''}$

$A_w = d \cdot t_w = \underline{14}$

$L = \underline{144}$

$d/A_f = \underline{1.167}$

$M = \frac{PL}{4} = \underline{36P}$

$S_x = \underline{165.714 \text{ in}^3}$

$V = \frac{P}{2}$

$t_w = \underline{1}$

BENDING STRESS :

$F_{b \text{ ALLOW}} = 12,000 \text{ psi}$

OR  $F_{b \text{ ALLOW}} = \frac{12 \times 10^6}{L \cdot d/A_f} = \frac{12 \times 10^6}{144 \times 1.167} = \underline{71908 \text{ psi}}$

USE THE LEAST

$\therefore f_{b \text{ MAX}} = \frac{M}{S_x} = \frac{36P}{165.714} = 12,000$

$P = 55238 \text{ lb}$   
 $= 27.6 \text{ TONS}$

SHEAR STRESS :

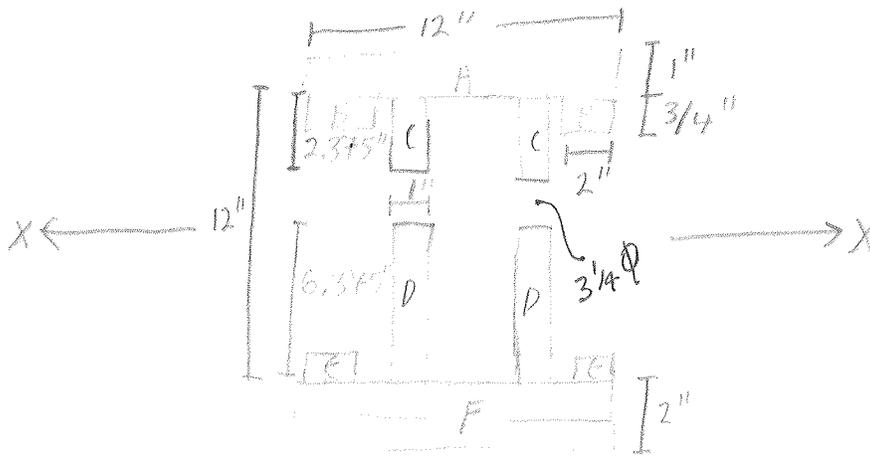
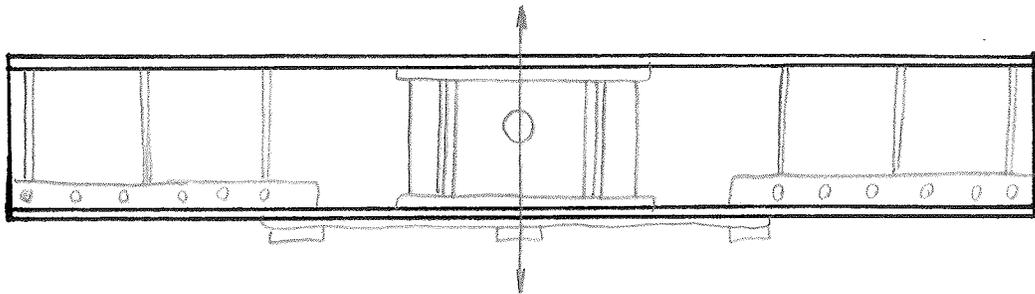
$F_{V \text{ ALLOW}} = \frac{.4 F_y}{3} = 4800 \text{ psi}$

$\therefore f_{V \text{ MAX}} = \frac{V}{A_w} = \frac{P}{2 \times 14} = 4800$

$P = 134400 \text{ LB.}$

SUMMARY :

$\therefore P = \underline{27.6 \text{ TONS}}$



$h = 6.269 \text{ in}$

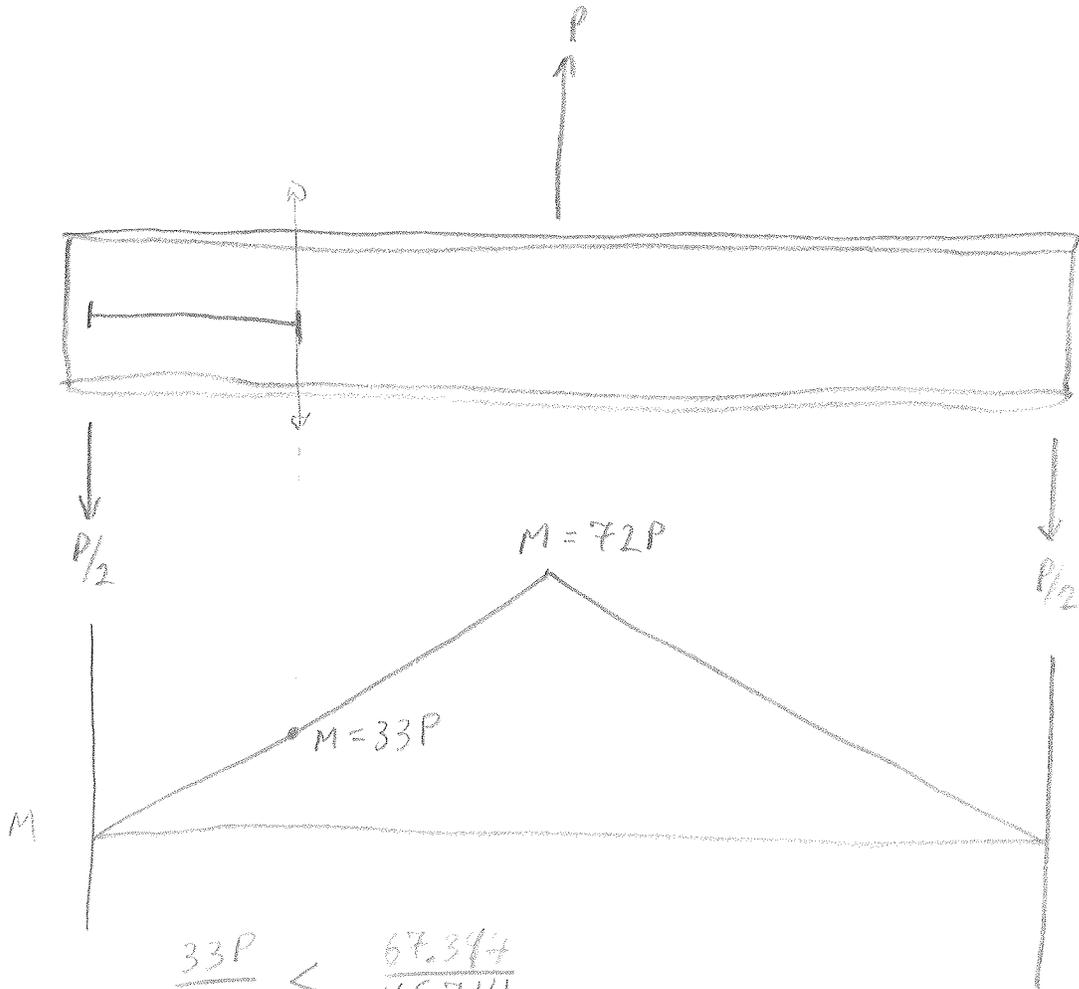
Section	Base (in)	Height (in)	I (in <sup>4</sup> )	Area (in <sup>2</sup> )	r (in)	r' (in)	Ar' <sup>2</sup> (in <sup>2</sup> )
A	12	1	1	12	14.5	8.231	812.992
B	4	0.75	0.141	3	13.625	14.335	162.132
C	2	2.375	2.233	4.75	12.613	6.537	203.414
D	2	6.375	43.101	12.75	5.158	1.081	14.899
E	4	0.75	0.141	3	2.375	3.894	45.49
F	12	2	8	24	1	6.269	666.297

$c = 8.731 \text{ in}$

$I_{xx} = 1960.12 \text{ in}^4$

$S_{xx} = 244.501 \text{ in}^3 > 165.714 \text{ in}^3$





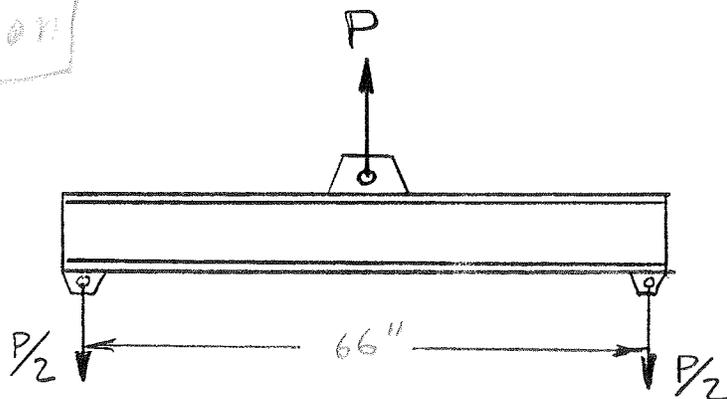
$$\frac{33P}{72P} < \frac{67.397}{165.714}$$

$$.4583 < .4067 \quad X$$

Tonnage adjusted from 24.6 tons  
to 24.5 tons.

SPREADER BAR N<sup>o</sup> 10 PAINT COLOR PRIMER

LEON



BEAM SIZE SPECIAL

$$d = \underline{14}$$

$$A_w = d \cdot t_w = \underline{14}$$

$$L = \underline{66 \text{ in}}$$

$$d/A_f = \underline{1.167}$$

$$M = \frac{PL}{4} = \underline{16.5P}$$

$$S_x = \underline{67.394 \cdot \text{in}^3}$$

$$V = \frac{P}{2}$$

$$t_w = \underline{1}$$

### BENDING STRESS :

$$F_b \text{ ALLOW} = 12,000 \text{ psi} \checkmark$$

$$\text{OR } F_b \text{ ALLOW} = \frac{12 \times 10^6}{L \cdot d/A_f} = \frac{12 \times 10^6}{(66)(1.167)} = \underline{155,949.6}$$

USE THE  
LEAST

$$\therefore f_b \text{ MAX} = \frac{M}{S_x} = \frac{16.5P}{67.394} = 12,000$$

$$\therefore P = \frac{49,014 \text{ lbs}}{2} = \underline{24,507 \text{ tons}}$$

### SHEAR STRESS :

$$F_v \text{ ALLOW} = \frac{0.4 F_y}{3} = 4800 \text{ psi}$$

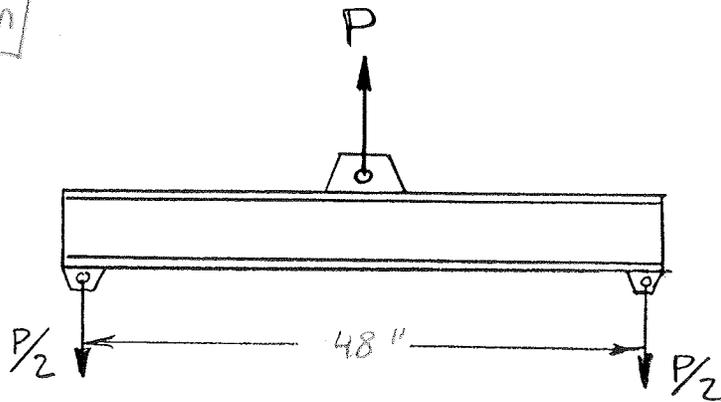
$$\therefore f_v \text{ MAX} = \frac{V}{A_w} = \frac{P}{2 \cdot 14} = 4800 = \underline{134,400 \text{ lbs}}$$

### SUMMARY :

$$\therefore P = \underline{24.5 \text{ TONS}}$$

SPREADER BAR N<sup>o</sup> 10 PAINT COLOR Red

Lean



Adjusted

BEAM SIZE SPECIAL

$$d = \underline{14''}$$

$$A_w = d \cdot t_w = \underline{14}$$

$$L = \underline{48''}$$

$$d/A_f = \underline{1.167}$$

$$M = \frac{PL}{4} = \underline{12P}$$

$$S_x = \underline{44.48 \text{ in}^3}$$

$$V = \frac{P}{2}$$

$$t_w = \underline{1}$$

BENDING STRESS :

$$F_b \text{ ALLOW} = 12,000 \text{ psi } \checkmark$$

$$\text{OR } F_b \text{ ALLOW} = \frac{12 \times 10^6}{L \cdot d/A_f} = \frac{12 \times 10^6}{(48)(1.167)} = \underline{214,224.5}$$

USE THE  
LEAST

$$\therefore f_b \text{ MAX} = \frac{M}{S_x} = \frac{12P}{44.48} = 12,000 \quad \therefore P = \underline{44,480 \text{ lbs}}$$

$$= \underline{22.24 \text{ TONS}}$$

SHEAR STRESS :

$$F_v \text{ ALLOW} = \frac{.4 F_y}{3} = 4800 \text{ psi}$$

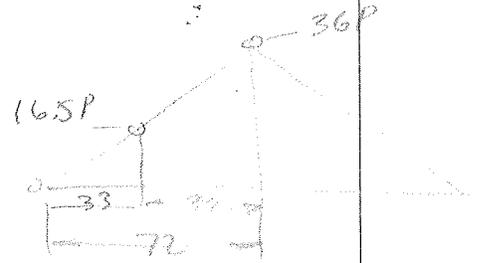
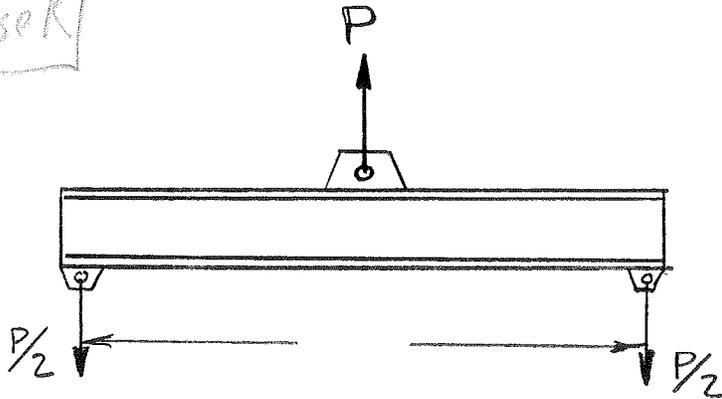
$$\therefore f_v \text{ MAX} = \frac{V}{A_w} = \frac{P}{2 \times 14} = 4800$$

$$\therefore P = \underline{134,400 \text{ lbs}}$$

SUMMARY :  $\therefore P = \underline{22.24 \text{ TONS}}$

SPREADER BAR N<sup>o</sup> 10 PAINT COLOR PRIMER

Bosek



BEAM SIZE \_\_\_\_\_

$d =$  \_\_\_\_\_

$A_w = 4 \cdot t_w =$  \_\_\_\_\_

$L =$  \_\_\_\_\_

$d/A_f =$  \_\_\_\_\_

$M = \frac{PL}{4} = \underline{16.5P}$

$S_x = \underline{67.395}$

$V = \frac{P}{2}$

$t_w =$  \_\_\_\_\_

BENDING STRESS :

$F_b \text{ ALLOW} = 12,000 \text{ psi}$

OR  $F_b \text{ ALLOW} = \frac{12 \times 10^6}{L \cdot d/A_f} = \frac{12 \times 10^6}{\quad} =$  \_\_\_\_\_

} USE THE LEAST

$\therefore f_{b \text{ MAX}} = \frac{M}{S_x} = \frac{16.5P}{67.395} = 12,000$

$P = 49019.5 \text{ lb}$   
 $P = 24.5 \text{ TON.}$

SHEAR STRESS :

$F_v \text{ ALLOW} = \frac{.4 F_y}{3} = 4800 \text{ psi}$

$\therefore f_{v \text{ MAX}} = \frac{V}{A_w} =$  \_\_\_\_\_

SUMMARY :  $\therefore P =$  \_\_\_\_\_ TONS

#10

Bill  
3PR  
STRICKLAN

