

SPREADER BAR

I.D. N^o 2

COLOR OF BAR :

Yellow

LOAD CAPACITY PAINTED

ON BAR 33 TONS.

DATE CAP. & I.D. N^o PAINTED

ON BAR July 1988

DATE OF LAST LOAD

TEST. August 8, 1988

TEST LOAD WEIGHT 41.16 TONS

TEST LOAD % 124.7%

STRESS CALCULATIONS :

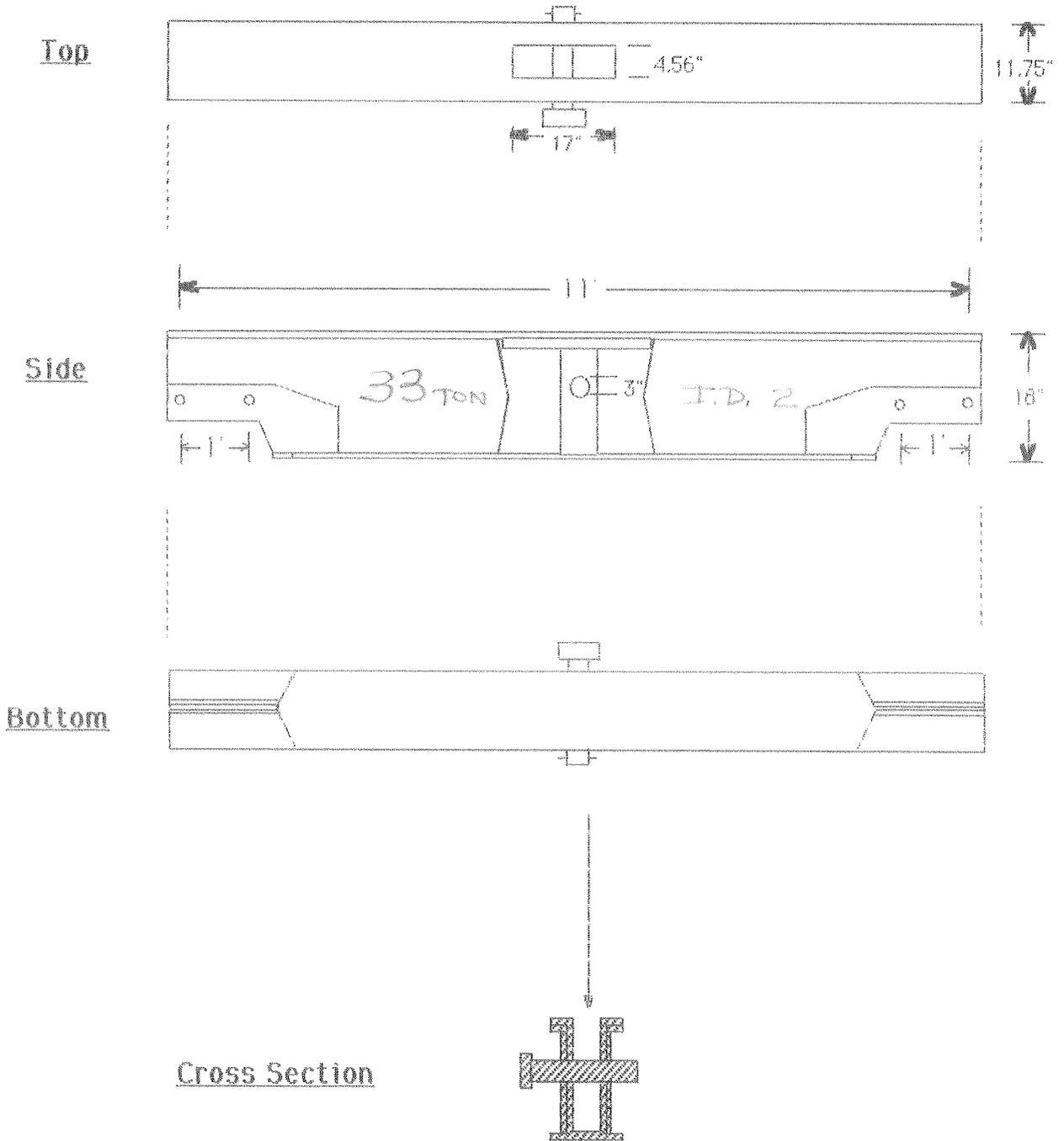
DONE BY Bosek + Miranda

DATE June 1988

REMARKS : Test was perfect



Yellow #2



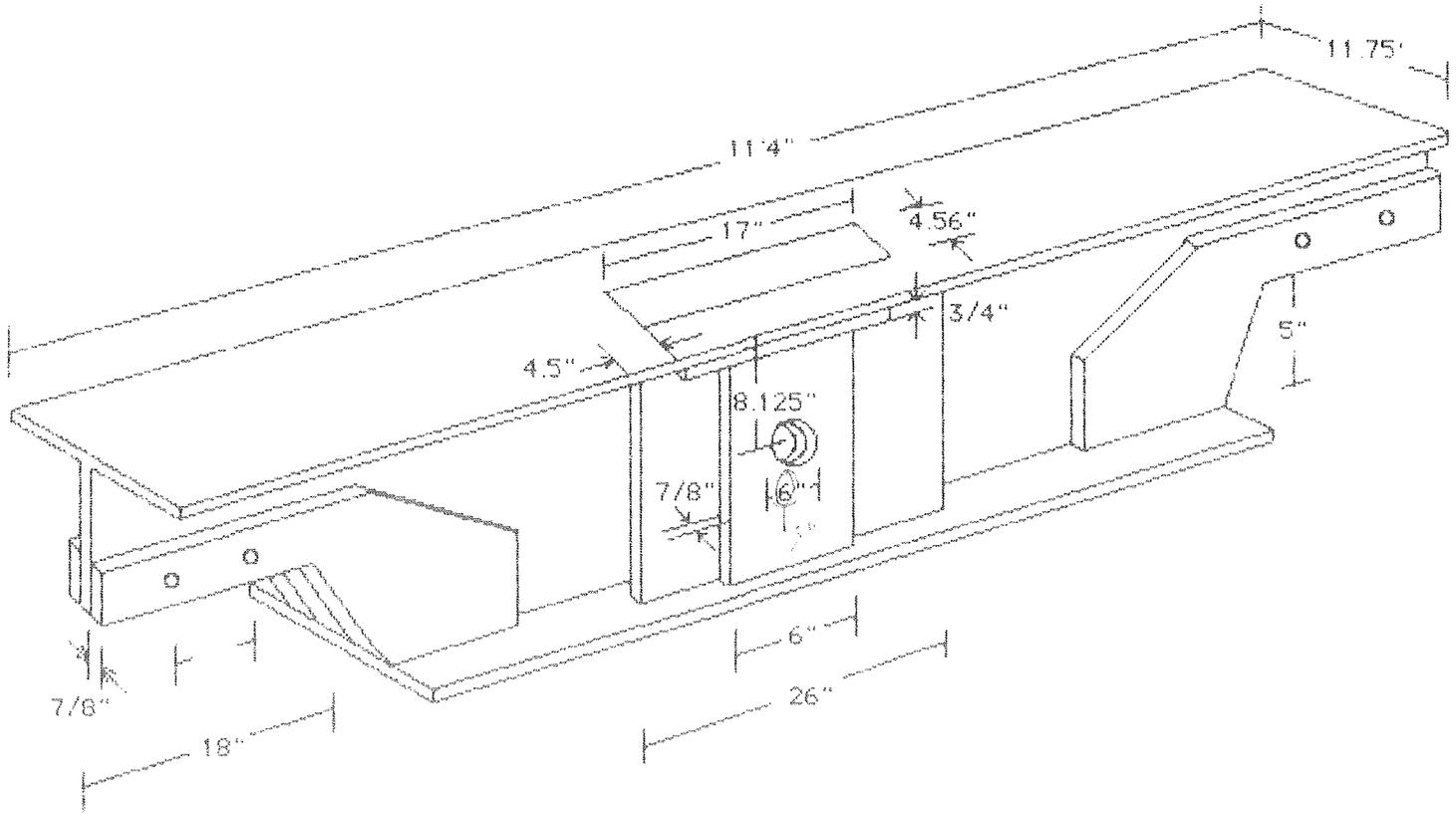
0 1 ft 2 ft 3 ft



scale: 1/2" = 1'

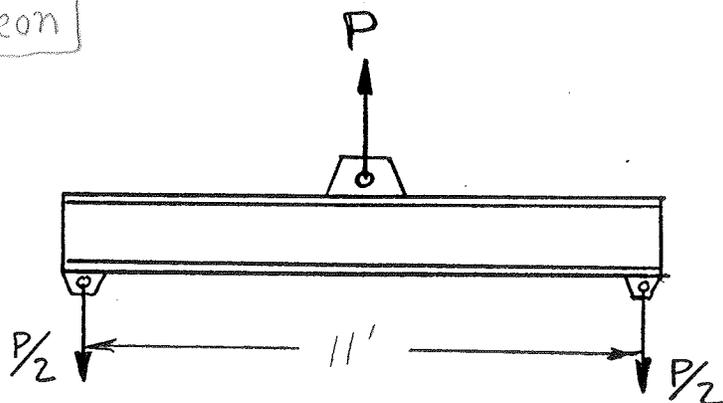
~ 1 hr 30 min

not to scale



SPREADER BAR N^o 2PAINT COLOR Yellow

Leon

BEAM SIZE W18 X 96

$$d = \underline{18 \text{ in}}$$

$$A_w = d \cdot t_w = \underline{9.216 \text{ in}^2}$$

$$L = \underline{132 \text{ in}}$$

$$d/A_f = \underline{1.86}$$

$$M = \frac{PL}{4} = \underline{33P}$$

$$S_x = \underline{185 \text{ in}^3}$$

$$V = \frac{P}{2}$$

$$t_w = \underline{.512 \text{ in}}$$

BENDING STRESS :

$$F_b \text{ ALLOW} = 12,000 \text{ psi}$$

$$\text{OR } F_b \text{ ALLOW} = \frac{12 \times 10^6}{L \cdot d/A_f} = \frac{12 \times 10^6}{(132)(1.86)} = \underline{48,876 \text{ psi}}$$

} USE THE
LEAST

$$\therefore f_b \text{ MAX} = \frac{M}{S_x} = \frac{33P}{185} = 178.4P = 12,000 \text{ psi}$$

$$\therefore P = 67,265 \text{ lb} = \underline{33.6 \text{ TONS}}$$

SHEAR STRESS :

$$F_v \text{ ALLOW} = \frac{.4 F_y}{3} = 4800 \text{ psi}$$

$$\therefore f_v \text{ MAX} = \frac{V}{A_w} = \frac{P}{2(9.216)} = \frac{P}{18.432} = 4,800 \text{ psi}$$

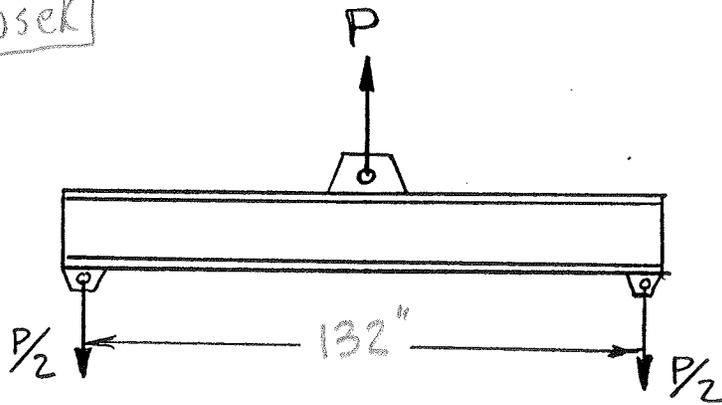
$$\therefore P = 88,474 \text{ lb} = \underline{44.2 \text{ TONS}}$$

SUMMARY :

$$\therefore P = \underline{33.6 \text{ TONS}}$$

SPREADER BAR N^o 2 PAINT COLOR YELLOW

Bosek



PAINTED ON
"33 TONS"

BEAM SIZE W 18 x 96

$$d = \underline{18.16}$$

$$A_w = d \cdot t_w = \underline{9.30}$$

$$L = \underline{132}$$

$$d/A_f = \underline{1.86}$$

$$M = \frac{PL}{4} = \underline{33P}$$

$$S_x = \underline{185}$$

$$V = \frac{P}{2}$$

$$t_w = \underline{.512}$$

BENDING STRESS :

$$F_b \text{ ALLOW} = 12,000 \text{ psi}$$

$$\text{OR } F_b \text{ ALLOW} = \frac{12 \times 10^6}{L \cdot d/A_f} = \frac{12 \times 10^6}{132 \times 1.86} = \underline{48876 \text{ psi}}$$

USE THE
LEAST

$$\therefore f_b \text{ MAX} = \frac{M}{S_x} = \frac{33P}{185} = 12000 \quad P = 67273 \text{ lb}$$

$$= 33.6 \text{ TONS}$$

SHEAR STRESS :

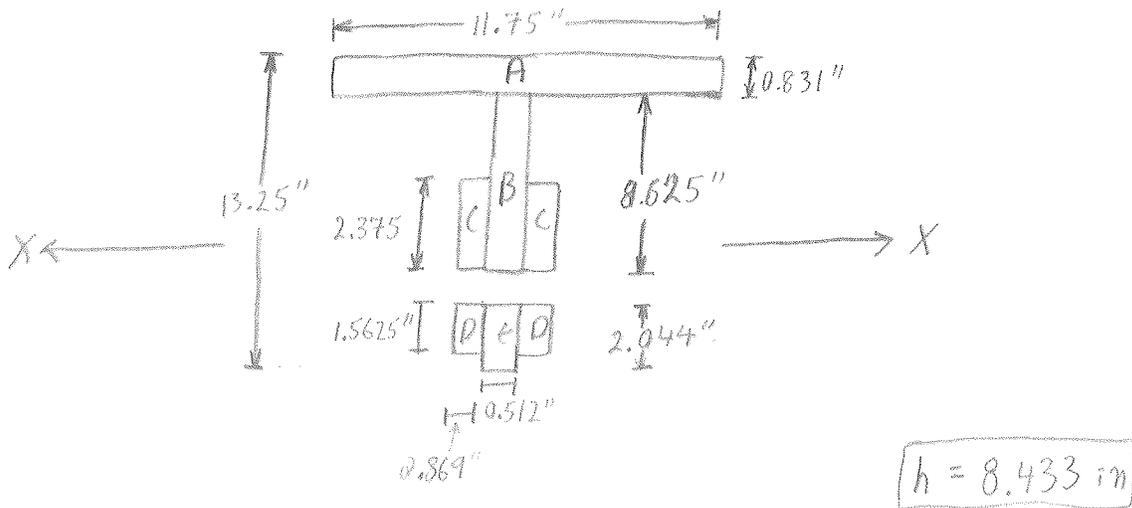
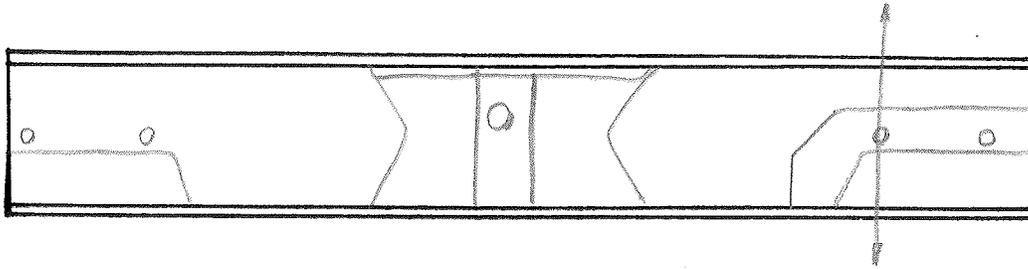
$$F_v \text{ ALLOW} = \frac{.4 F_y}{3} = 4800 \text{ psi}$$

$$\therefore f_v \text{ MAX} = \frac{V}{A_w} = \frac{P}{2 \times 9.3} = 4800 \quad P = 89280 \text{ lbs.}$$

$$= 44.6 \text{ TONS}$$

SUMMARY :

$$\therefore P = \underline{33.6 \text{ TONS}}$$



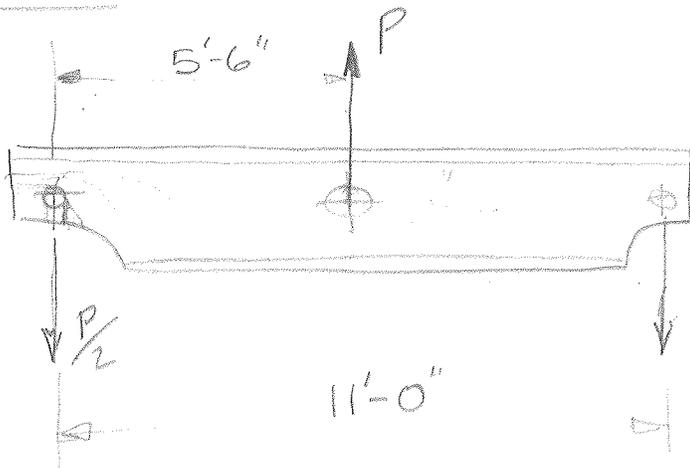
Section	Base (in)	Height (in)	I (in ⁴)	Area (in ²)	r (in)	r' (in)	Ar ² (in ²)
A	11.75	0.831	0.562	9.764	12.835	4.402	189.203
B	0.512	8.625	27.376	4.416	8.107	0.326	0.469
C	1.738	2.375	1.940	4.128	4.982	3.451	49.162
D	1.738	1.563	0.553	2.716	1.236	7.197	140.680
E	0.512	2.044	0.364	1.047	1.022	7.411	57.504

$c = 8.433 \text{ in}$

$I_{xx} = 467.813 \text{ in}^4$

$S_{xx} = 55.474 \text{ in}^3 < 185 \text{ in}^3 \implies \text{see back}$

BENDING:



I-BEAM

W-18x96

(Steel Man. PP 1-32)

$$S_{max} = 185 \text{ in}^3$$

$$\frac{d}{A_f} = 1.86$$

A_f

$$r_T = 3.19$$

$$l = 132''$$

Steel Man pp 5-19

$$F_b \text{ ALLOWABLE} = \frac{12 \times 10^6}{l d / A_f}$$

$$F_{b \text{ allow}} = \frac{12 \times 10^6}{132 \times 1.86} = 48,876 \text{ psi}$$

OR

Steel Man pp 5-19

$$F_{b \text{ allow}} = \frac{170 \times 10^6}{\left(\frac{l}{r_T}\right)^2} = 99,285 \text{ psi}$$

OR

$$F_{b \text{ max}} = 21,600 \text{ psi} \quad 12,000 \text{ psi max}$$

$$F_b = \frac{M}{S} \quad \frac{12,000}{21,600} = \frac{M}{185} \quad M = 2,220,000 \text{ in. lb.}$$

Steel Man pp. 3-200
CASE 7.

$$M_{MAX} = \frac{P}{2} \times 66 = \frac{2,220,000}{2} = 1,110,000$$

$$P = \frac{1,110,000 \text{ lb.}}{67.273 \text{ lb}} \approx 60 \text{ TONS}$$

Bosch
Not
paid

BEARING ON CENTER PIN:

STEEL MAN
11.5-19

$$F_{ALLOWABLE} = .9 (36,000) = 32,400 \text{ psi}$$

but
CHECK
SHAFTS

$$3" \text{ DIA. } \left\{ \left(\frac{7}{8} + 1 + 1 \times \frac{7}{8} \right) = 3 \frac{3}{4} \text{ " length OF CONTACT} \right.$$

$$\text{LOAD} = \frac{34.5 \text{ TONS}}{60 \text{ TONS}}$$

17,420 lbs

$$P = \frac{lb}{IN} = \frac{60 \times 2000}{3.75} = 32,000 \text{ lb/IN.}$$

ROARK pp 320 CASE 6

$$S_c = .591 \sqrt{p E \frac{(D_1 - D_2)}{D_1 D_2}}$$

E = 29 x 10⁶

D₁ = 3.062

D₂ = 3.000

$$S_c = 46773 \text{ psi} < 32,400 \text{ psi}$$

TRY LOAD = 40 TONS

$$P = \frac{40 \times 2000}{3.75} = 21333 \text{ lb/IN.}$$

$$S_c = .591 \sqrt{p E \frac{(D_1 - D_2)}{D_1 D_2}}$$

$$S_c = 38190 \text{ psi} < 32400 \text{ psi}$$

TRY LOAD = 25 TONS

$$P = \frac{25 \times 2000}{3.75} = 13333 \text{ lb/IN.}$$

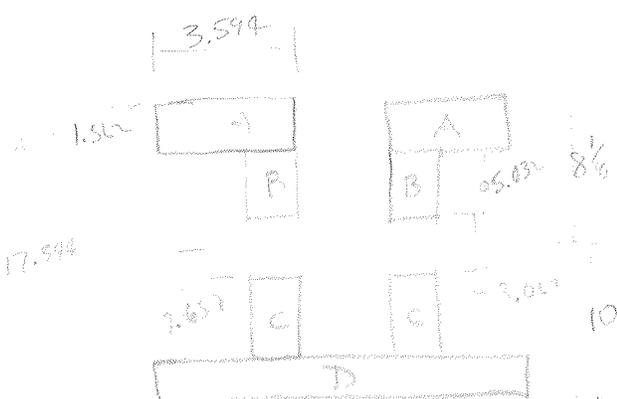
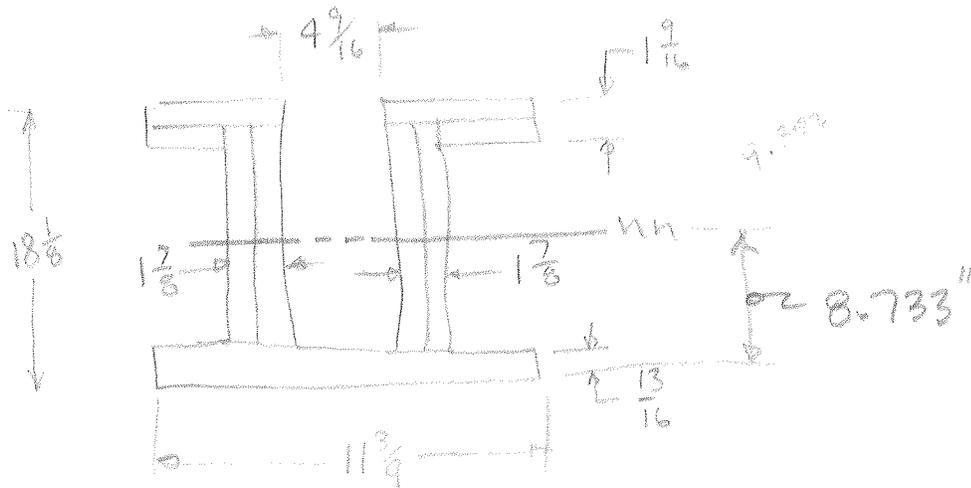
$$S_c = .591 \sqrt{p E \frac{(D_1 - D_2)}{D_1 D_2}}$$

$$S_c = 30192 \text{ psi} < 32400 \text{ psi}$$

∴ ≈ 26 TON IS MAX BEARING LOAD ON CENTER PIN.

SECTION MODULAS AT CENTER

S FOR $W18 \times 96 = 185 \text{ in}^3 \leq S$ AT BEAM CENTER



Find h

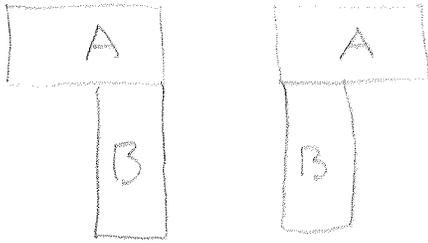
$$h = \frac{\sum M}{\sum A}$$

Deck Welding
PP 2.3-2

$$h = \frac{300.3959}{38.9467} = 8.733''$$

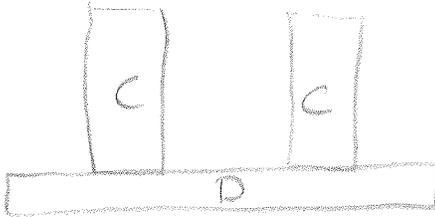
SECTION	AREA in^2	DIST. TO REF LINE	M
A	$5.6138 \times (2)$	17.344	$97.3657 \times (2)$
B	$9.435 \times (2)$	14.097	$132.5334 \times (2)$
C	$14.3569 \times (2)$	4.6405	$66.6232 \times (2)$
D	9.541	4.04	3.8736

$\sum A = 68.3524$ $\sum M = 596.9182$



$$I_{nn} = \sum I_a + \sum r^2 A_a$$

$$I_c = \frac{bh^3}{12}$$



<u>SECTION</u>	<u>$I_{a,b,c,d}$</u>	<u>r</u>	<u>A in²</u>	<u>$r^2 A$</u>
A	1.1414 x 2	2.611	11.2276	832.5189
B	19.9087 x 2	5.314	18.87	532.8623
C	70.1449 x 1	4.0925	28.7138	480.9147
D	.5242	8.327	9.541	661.5627
	<u><u>$\sum I_{a,b,c,d}$</u></u>			<u><u>$\sum r^2 A = 2507.8586$</u></u>
	$\sum I_{a,b,c,d} = 182.9142$			

$$I_{nn} = 2690.7728 \text{ in}^4$$

$$S = \frac{I}{c} = 308.1155 \text{ in}^3 > 185 \text{ in}^3$$

HORIZONTAL SHEAR AT NEUTRAL AXIS:

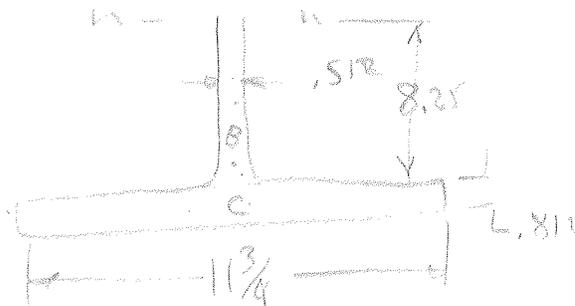
$$F_s = \frac{VAy}{I \cdot t}$$

$$V = 33600 \text{ lb.}$$

$$A = \frac{28.2}{2} = 14.1 \text{ IN}^2$$

$$I = 1680 \text{ IN}^4$$

$$t = .512 \text{ IN}$$

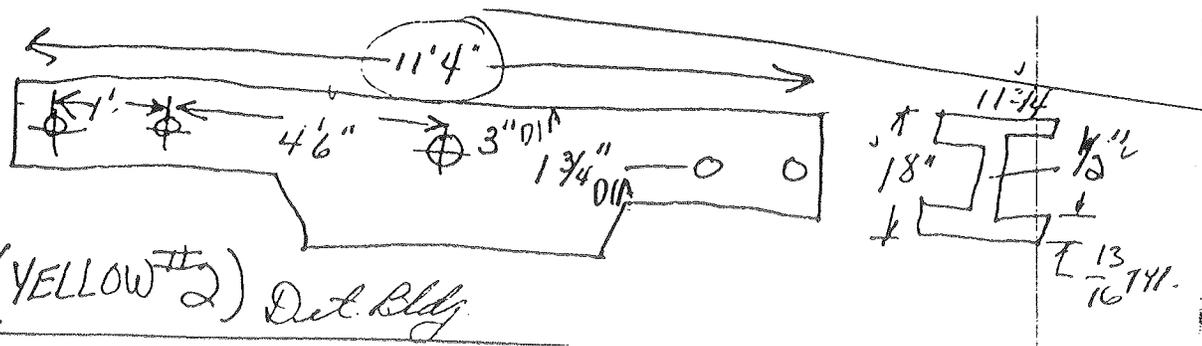


SECTION	AREA	dist to top	MOMENT
B	4.234	4.125	17.474
C	9.541	8.656	82.5869
ΣA	13.765	ΣMA	100.0109

$$Y = \frac{\Sigma MA}{\Sigma A} = 7.2656 \text{ ''}$$

$$F_s = \frac{33600 \times 14.1 \times 7.2656}{1680 \times .512} = 4002 \text{ psi}$$

Field Data



RATING (YELLOW #2) Det. Bldg.

Yellow #2

Field Data

Leon

7-18-88

