

**LIFTING DEVICE**

DEVICE NAME: Lab E Chamber Lifting Fixture

ENGINEERING NOTE NUMBER: #49

DRAWING NUMBER: \_\_\_\_\_

APPLICABLE STANDARD: Specifications for Aluminum Structures

RATED LOAD: 1120 lbs

TEST LOAD: 1400 lbs

TEST LOAD PERCENT: 125%

LAST LOAD TEST DATE: 7/29/92

COLOR: Aluminaum

**STRESS CALCULATIONS:**

Done by: Donald V. Mitchell

Date: 7-28-92

Reviewed by: Zhiying Tang

Date: 9-1-92

**REMARKS:**

**IDENTIFICATION:**

Engineering Note Number & Rated Load Must be Clearly Marked On a Conspicuous Surface.



Lab E: Chamber lifting fixture  
Rated for 1120 lbs  
Load test 7-29-92 @ 1400 lbs

*Don Mitchell*

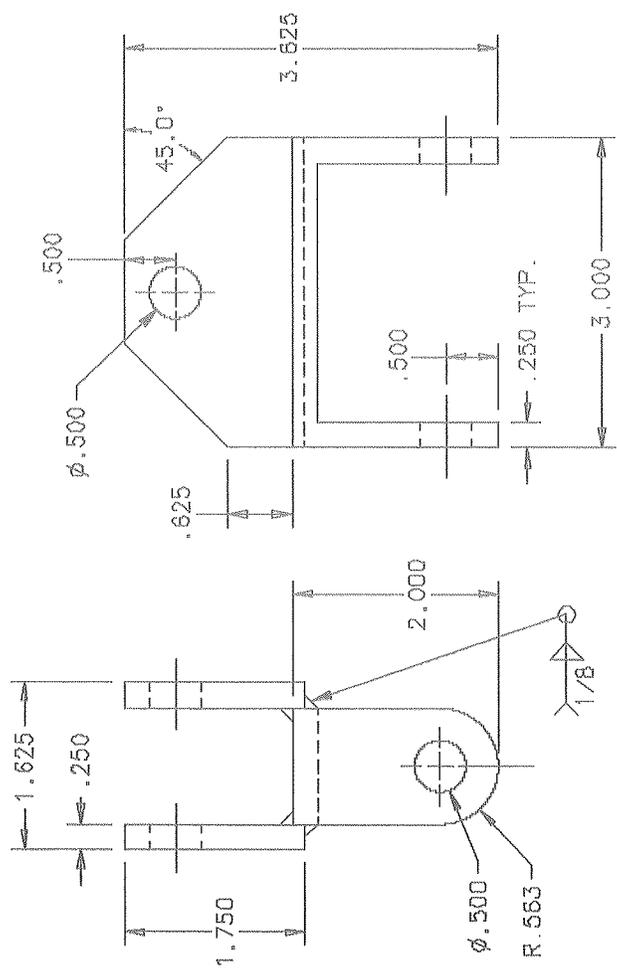


Lab E: Chamber Lifting fixture  
Rated for 1120 lbs  
Load test 7-29-92 @ 1400 lbs

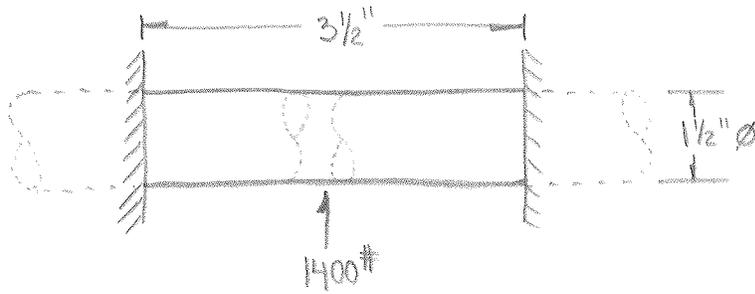
*Don Mitchell*



REV.	DESCRIPTION	DRAWN	DATE
		APPD.	DATE



ITEM NO.	PART NO.	DESCRIPTION OR SIZE	QTY.	REV.
		PARTS LIST		
UNLESS OTHERWISE SPECIFIED		ORIGINATOR		
FRACTIONS	DECIMAL	ANGLES	DRAWN	
±	±	±	CHECKED	
			APPROVED	
1. BREAK ALL SHARP EDGES 1/64 MAX.		USED ON		
2. DO NOT SCALE DRG.		MATERIAL - A36 Steel		
3. DIMENSIONING IS ACCORD TO THE AMERICAN STANDARD MAX. ALL MACHINED SURFACES		FERMI NATIONAL ACCELERATOR LABORATORY UNITED STATES DEPARTMENT OF ENERGY		
SCALE 1:1		Lab E Lifting Fixture		
DRAWING SIZE B		Pick Point Pin Weldment		
DRAWING NUMBER		REV.		
IDEAS LEVEL 8, D		USERNAME: DMITCHEL		
CADD FILE:				



Aluminum T6061-T6

From "Specifications for Aluminum Structures":

allowable stress,  $F_b = 24,000$  psi

$$I = \frac{1}{4}\pi r^4 = \frac{1}{4}\pi (.75)^4 = .2485 \text{ in}^4$$

$$c = .75 \text{ in}$$

$$M_x = \frac{FL}{8} = \left(\frac{1400\#}{8}\right)(3.5 \text{ in}) = 612.5 \text{ lb-in}$$

$$\sigma_{\max} = \frac{M_x c}{I} = \frac{(612.5 \text{ in-lb})(.75 \text{ in})}{.2485 \text{ in}^4} = 1,848 \text{ psi} \quad \underline{\text{OK}}$$

$$\sigma_{\max} = 1848 \text{ psi}$$

$$\text{Shear Stress} = \frac{F}{A} = \frac{1400\#}{1.767 \text{ in}^2} = 792.2 \text{ psi} \quad \underline{\text{OK}}$$

$$\tau = 792 \text{ psi}$$

Find  $S_{\min}$ :

With  $S_{\min}$  known, the smallest aluminum member able to withstand this load without being overstressed can be determined. A comparison between this beam and the actual lifting fixture beam can then be made.

Cantilevered end load:

$$M_{\max} = (34.25 \text{ in})(700\#) = 23,975 \text{ in-lb}$$

$$\sigma_{\text{allowable}} = F_b = 19,000 \text{ psi}$$

$$\sigma_{\max} = \frac{M_{\max}}{S_{\min}} \Rightarrow S_{\min} = \frac{M_{\max}}{\sigma_{\max}} = \frac{23,975 \text{ in-lb}}{19,000 \text{ psi}}$$

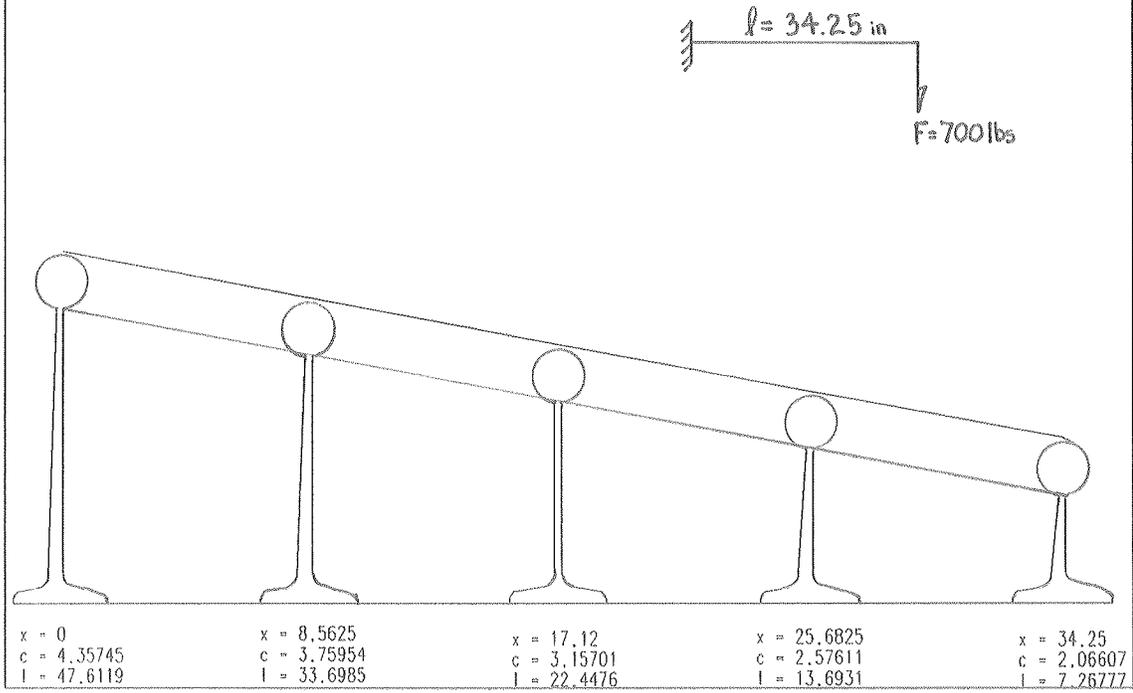
$$S_{\min} = 1.26 \text{ in}^3$$

The smallest American Standard I-beam that can be used is a  $3\frac{1}{2}$ " x  $2.33_{bf}$  x  $1.96\#/\text{ft}$  w/

$$S = 1.68 \text{ in}^3, I = 2.52 \text{ in}^4$$

LAB E Lifting Fixture

LAB E CHAMBER LIFTING FIXTURE ID # 49



junk.mcs

```

i := 1 .. 34.25 * 4          Load and length of tapered beam:
x := .25 * i                F := 700 Lbs
i
l := 34.25 in
M := F * [ x - l ]
i
    
```

Curve fitted equation to determine distance from neutral axis to extreme fiber:

$$c_i := 4.357461 - .06918622 \cdot x_i - .00007126 \cdot x_i^2 - .000002047 \cdot x_i^3 + .000000177 \cdot x_i^4$$

Curve fitted equation to determine the Moment of Inertia for the tapered beam:

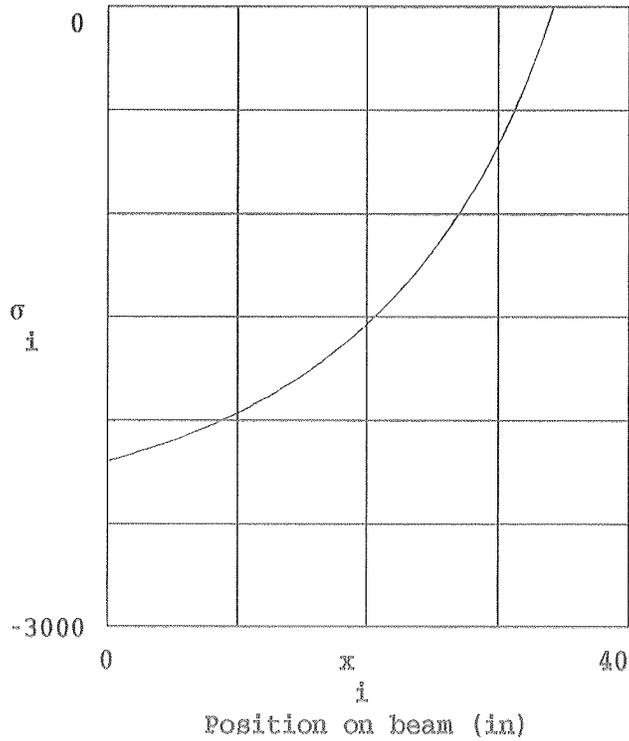
$$I_i := 47.61201 - 1.785776 \cdot x_i + .01909183 \cdot x_i^2 - .00003540131 \cdot x_i^3 - .0000001126073 \cdot x_i^4$$

Stress Equation:

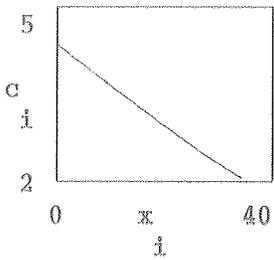
$$\sigma_i := \frac{M_i \cdot c_i}{I_i}$$

STRESS (psi)

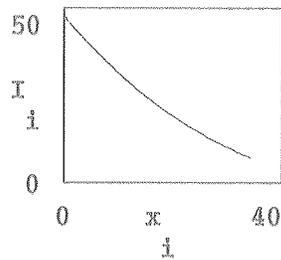
Stress (psi) vs. Position along beam



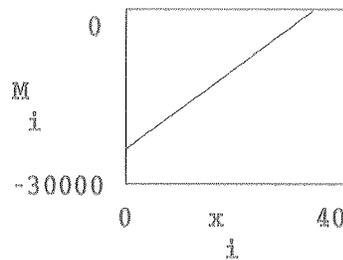
c value



moment of inertia



Moments



$$\sigma_{max} = |-2,190 \text{ psi}|$$

DATA CURVE FOLDING RESULTS

X-Values: X position (length)  
 Y-Values: Moment of Inertia about the X-Y axis

Input Data:

	<u>X</u>	<u>Y</u>
Data point # 1 :	0	47.6119
Data point # 2 :	6.5625	33.5935
Data point # 3 :	17.12	22.4476
Data point # 4 :	29.6875	13.6931
Data point # 5 :	34.25	7.26777

Results:

	Equation	Average % Deviation	Maximum % Deviation
Exponential:	$Y = 51.95314 * \text{EXP}(-5.442561E-02 * X^2)$	7.66	10.66
Square Root:	$Y = 49.89095 + 6.935931 * \text{SQRT}(X)$	11.63	27.95
Logarithmic:	$Y = 75.1312 * (-13.99659 * \text{LN}(X))$	4.87	10.60
Power:	Not applicable (req. of 10 X or Y values)	---	---
Inverse:	$Y = 2.129107 + 281.6705 / X$	14.56	42.93
Linear:	$Y = 45.0609 * (-1.176628 * X)$	11.89	33.92
Polynomial:	Constant coefficient: 47.61191 1 Degree coefficient: -1.285726 2 Degree coefficient: -1.905193E-02 3 Degree coefficient: -3.540131E-05 4 Degree coefficient: 1.325070E-07	0.00	0.00

NON-LINEAR LEAST SQUARES (NLSQ) RESULTS

X-Values: Z position (inches)  
 Y-Values: C (distance from neutral axis to extreme fiber)

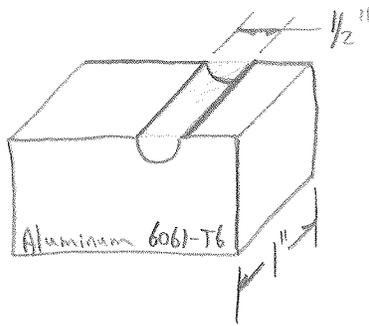
Input Data:

	(X)	(Y)
Data point # 1 :	0	4.35745
Data point # 2 :	6.5625	3.75954
Data point # 3 :	17.12	3.15701
Data point # 4 :	25.6825	2.57611
Data point # 5 :	34.25	2.06607

Results:

	Equation	Average % Deviation	Maximum % Deviation
Exponential:	$Y = 4.471975 * \text{EXP}(-2.194671E-02 * X)$	1.99	2.60
Square Root:	$Y = 4.564344 + (-.3959337 * \text{SQRT}(X))$	5.59	12.15
Logarithmic:	$Y = 6.419071 + (-1.200016 * \text{LN}(X))$	3.58	9.49
Power:	Not applicable (neg. or 0) X or Y values	-	-
Inverse:	$Y = 1.873152 + (-17.33197 / X)$	6.09	14.01
Polynomial:	$Y = 4.346579 + (-.077459 * X)$	1.25	1.75
Polynomial:	constant coefficient: 0.357163 1 Degree coefficient: 6.218625E-02 2 Degree coefficient: 3.137025E-04 3 Degree coefficient: -2.047274E-06 4 Degree coefficient: 1.773909E-07	0.00	0.00

Reference: Specifications for Aluminum Structures



$$\text{Bearing Area} = \left(\frac{1}{2}\text{''}\right)(1\text{''}) = \frac{1}{2}\text{ in}^2$$

$$\text{Load on Pin} = 700 \#$$

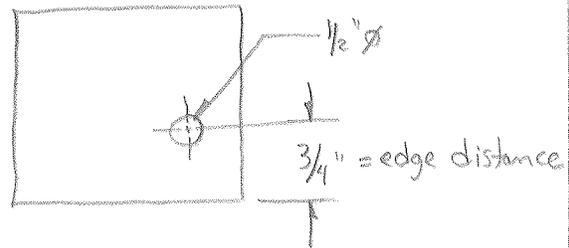
$$\text{Bearing stress} = \frac{700 \#}{\frac{1}{2}\text{ in}^2} = 1400 \text{ psi}$$

### Allowable Bearing Stress:

Minimum edge distance should be:

$$e.d = 2 \times \text{Nominal diameter}$$

$$e.d = 2 \times \frac{1}{2}\text{''} = 1\text{''}$$



Allowable bearing stress for standard edge distance = 35,000 psi

$$\text{reduction factor} = \frac{3/4\text{''}}{1\text{''}} = .75$$

$$\text{Allowable bearing stress} = (35,000 \text{ psi})(.75) = 26,250 \text{ psi}$$

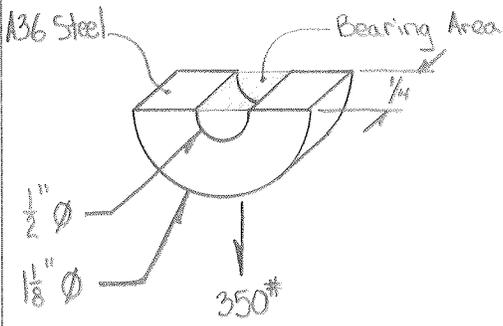
$$\text{actual bearing stress} = 1400 \text{ psi} \therefore \underline{\underline{OK}}$$

$$\begin{aligned} \text{Absolute Minimum edge distance} &= (1.5)(\text{hole diameter}) \\ &= (1.5)(.5) \\ &= .75\text{''}, \frac{3}{4}\text{''} \end{aligned}$$

$$\text{Shear area of block} = (.56\text{ in})(1\text{ in}) = .56\text{ in}^2$$

$$\text{Shear stress}_{\text{Block}} = \frac{700 \#}{.56\text{ in}^2} = 1250 \text{ psi}$$

$$\text{allowable shear stress} = 11,000 \text{ psi}$$



$$\text{Bearing Area} = \left(\frac{1}{4}\right) \left(\frac{1}{2}\right) = .125 \text{ in}^2$$

$$\text{Bearing Stress} = \frac{F}{A_b} = \frac{350\#}{.125 \text{ in}^2} = 2800 \text{ psi}$$

From AISC 9th edition:

$$\text{Allowable Bearing Stress} = \frac{L_e F_u}{2d}$$

$$\sigma_b = \frac{(.5)(58 \text{ ksi})}{(2)(.5" \text{ } \phi)}$$

$$\sigma_b = 29,000 \text{ psi} \quad \underline{\underline{\text{OK}}}$$

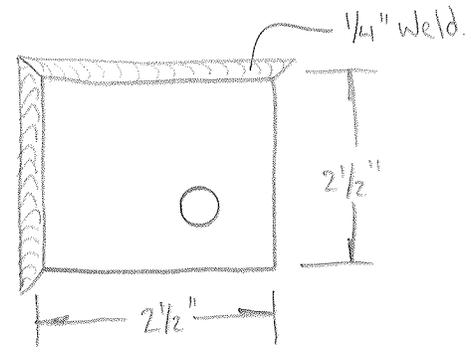
Allowable, Minimum Edge distance: (AISC)

$$L_e = \frac{2P}{F_u t} = \frac{2(350\#)}{(58,000 \text{ psi})(.25 \text{ in})} = .048 \text{ in}$$

For an edge distance of 1/2" (as in this case), the maximum load allowable is 3,625 lbs.

WELDS:

A 2 1/2" x 2 1/2" x 1" Aluminum block is mounted at each end of the beam. Ten inches of 1/4" deep weld is used to mount each block. With only 700 lbs supported, 70 lbs/inch of weld is well below the allowable.



**BELOW-THE-HOOK LIFTING DEVICE**  
**Engineering Note Cover Page**

Lifting Device Numbers:

FNAL Site No.: \_\_\_\_\_ Div. Specific No.: #49 Asset No. \_\_\_\_\_  
 if applicable if applicable if applicable

ASME B30.20 Group:  
 (check one)

**Group I** Structural and Mechanical Lifting Devices  
 **Group II** Vacuum Lifting Devices  
 **Group III** Magnets, Close Proximity Operated  
 **Group IV** Magnets, Remote Operated

Device Name or Description: SPREADER BAR

Device was: Purchased from a Commercial Lifting Device Manufacturer  
 mfg. name: \_\_\_\_\_

(check all applicable)  Designed and Built at Fermilab  
 Designed by Fermilab and Built by a Vendor  
 Assy drawing number: \_\_\_\_\_  
 Provided by a User or Other Laboratory  
 Other. Describe: \_\_\_\_\_

Engineering Note Prepared by: Don Mitchell Date: 7-23-92

Engineering Note Reviewed by: Zhu Jing Date: 3-3-2000

Lifting Device Data:

Capacity: 1400 lbs

Fixture Weight: 34 lbs

Service:  normal  heavy  severe (refer to B30.20 for definitions)

Duty Cycle: \_\_\_\_\_ 8, 16 or 24 hour rating (applicable to groups III, and IV)

Inspections Frequency: \_\_\_\_\_

Rated Load Test by FNAL (if applicable): Date: 3/14/00 Load: 1680 lbs

Check if Load Test was by Vendor and attach the certificate.

Satisfactory Load Test Witnessed by: JAMES FAGAN 6475

Signature (of Load Test Witness): James Fagan

Notes or Special Information:

Spreader bar to 13 ft HDT Drill fixture weight = 1250 lbs  
 original calculations used 1400 lbs load. Device to be  
 re-rated to 1400 lbs by testing to 1680 lbs.