

BELOW-THE-HOOK LIFTING DEVICE
Engineering Note Cover Page

Lifting Device Numbers:

FNAL Site No.: _____ Div. Specific No.: 95 Asset No. _____
 if applicable if applicable if applicable

ASME B30.20 Group: _____
 (check one)

- Group I Structural and Mechanical Lifting Devices
- Group II Vacuum Lifting Devices
- Group III Magnets, Close Proximity Operated
- Group IV Magnets, Remote Operated

Device Name or Description: _____

Device was: Purchased from a Commercial Lifting Device Manufacturer
 mfg. name: _____
 (check all applicable) Designed and Built at Fermilab
 Designed by Fermilab and Built by a Vendor
 Assy drawing number: _____
 Provided by a User or Other Laboratory
 Other. Describe: _____

Engineering Note Prepared by: JAMES KILMER Date: 8/19/99Engineering Note Reviewed by: Eric D. Hynes Date: 8/20/99

Lifting Device Data:

Capacity: 220 lbs

Fixture Weight: _____

Service: normal heavy severe (refer to B30.20 for definitions)

Duty Cycle: _____ 8, 16 or 24 hour rating (applicable to groups III, and IV)

Inspections Frequency: _____

Rated Load Test by FNAL (if applicable): Date: _____ Load: 275 lbs Check if Load Test was by Vendor and attach the certificate.Satisfactory Load Test Witnessed by: Charles D. Paul

Signature (of Load Test Witness): _____

Notes or Special Information:



SUBJECT

KEK SPREADER BAR

NAME

JIM KILMER

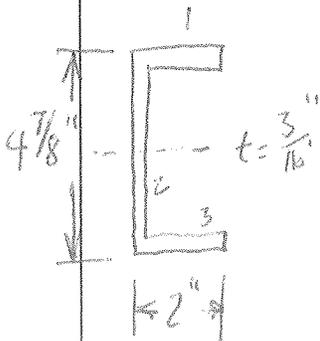
DATE

8/19/99

REVISION DATE

THIS FIXTURE WAS MADE IN JAPAN AT THE KEK LAB TO ASSEMBLE A HANGING FILE TYPE CALORIMETER FOR THE TEST BEAM IN MESON LAB. THE MATERIAL IS ALUMINUM AND APPEARS TO BE A STANDARD CHANNEL. ASSUME THE ALUMINUM TO BE 6061-T6

CALCULATE I_x



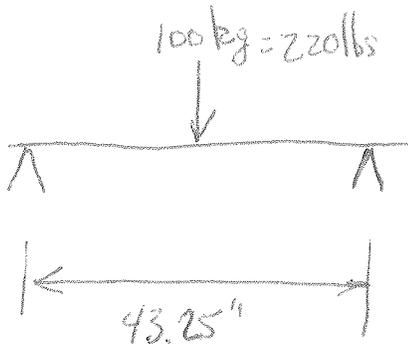
SHAPE 1	\bar{I}	A	d	Ad^2
1	$\frac{1}{12}(2)(.1875)^3$	$(2)(.1875)$	2.34	
2	1.1×10^{-3}	.375		2.05
3	$\frac{1}{12}(.1875)(4.5)^3$	$(4.5)(.1875)$	0	0
3	1.42	.844		
3	$\frac{1}{12}(2)(.1875)^3$	$(2)(.1875)$	2.34	2.05
	1.1×10^{-3}	.375		

$\Sigma \bar{I} = 1.42$

$\Sigma Ad^2 = 4.1$

$I_x = \Sigma \bar{I} + \Sigma Ad^2$

$= 1.42 + 4.1 = 5.52 \text{ in}^4$



USE SIMPLY SUPPORTED BEAM FORMULA

$$M = \frac{PL}{4} = \frac{(220 \text{ lbs}) \left(\frac{43.25 \text{ in}}{2} \right)}{4} = 1190 \text{ lb-in}$$

JV



SUBJECT

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$$\sigma = \frac{M_e}{I}$$

$$= \frac{(1190 \text{ lb in})(2.34")}{5.52 \text{ in}^4}$$

$$= 504 \text{ PSI}$$

$$c = d = 2.34"$$

$$I = 5.52 \text{ in}^4$$

Ø061 ALUMINUM YIELD = 35 KSI

ALLOWABLE FOR LIFTING FIXTURES = 11.7 KSI

⇒ BENDING IS OK

LOOK AT BEARING STRESS ON END BOLTS

BOLTS ARE 5/16" Ø

$$\text{LOAD AREA IS THEN } \frac{5}{16}" \times \frac{3}{16}" = .313 \text{ in} \times .1875 \text{ in}$$

$$= .0586 \text{ in}^2$$

$$\text{LOAD} = 110 \text{ lbs}$$

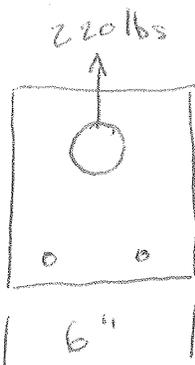
$$\sigma = \frac{\text{LOAD}}{\text{AREA}} = \frac{110 \text{ lbs}}{.0586 \text{ in}^2}$$

$$= 1880 \text{ PSI}$$

⇒ BEARING LOAD IS OK

BOLTS AT PICK POINT ARE 3/8" (LARGER) SO STRESS IS EVEN LESS

TENSION ON PICK POINT BAR



$$\sigma = \frac{\text{LOAD}}{\text{AREA}} = \frac{220 \text{ lbs}}{6" \times \frac{3}{8}"}$$

$$= 97.8 \text{ PSI}$$



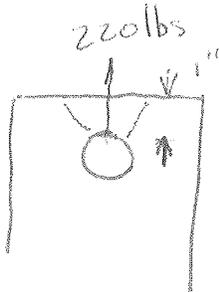
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~~DEL~~ BLOCK SHEAR ON PICK POINT



$$\sigma = \frac{\text{LOAD}}{\text{AREA}}$$

$$= \frac{220 \text{ lbs}}{1" \times \frac{3}{8}" \times 2}$$

$$= 293 \text{ PSI IN SHEAR}$$

BOLT SHEAR YIELD STRENGTH = 20 KSI

ALLOWABLE SHEAR ON LIFTING FIXTURE = 6.67 KSI

⇒ BLOCK SHEAR IS OK

PICKING EARS ARE STAINLESS STEEL 2" X 3/8"

$$\text{STRESS} = \frac{220 \text{ lbs} / 2}{2" \times \frac{3}{8}"} = 147 \text{ PSI}$$

⇒ OK

3/8" STAINLESS BOLTS ARE USED AS A HOOK ON EACH PICKING EAR

LOOK AT LOAD AS SHEAR

$$A = \frac{\pi}{4} d^2 = \frac{\pi}{4} (.294 \text{ in})^2 = .068 \text{ in}^2$$

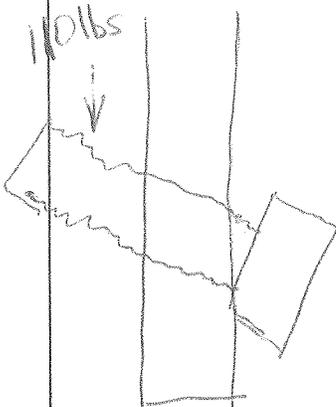
$$\sigma = \frac{F}{A}$$

$$\sigma = \frac{110 \text{ lbs}}{.068 \text{ in}^2}$$

$$= 1620 \text{ PSI}$$

$$\text{STAINLESS ALLOWABLE} = \frac{F_y}{3} = \frac{30 \text{ KSI}}{3} = 10 \text{ KSI}$$

⇒ BOLT SHEAR OK





ENGINEERING NOTE

SECTION

PROJECT

SERIAL-CATEGORY

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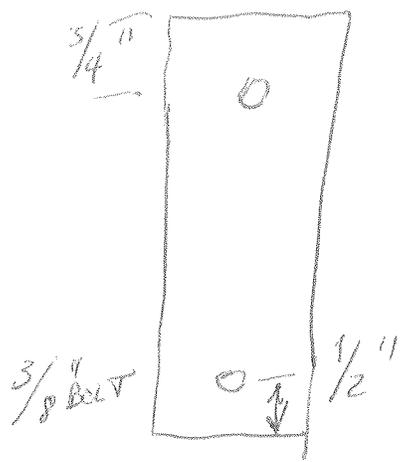
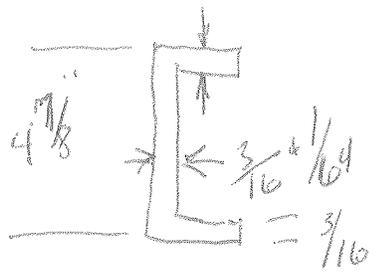
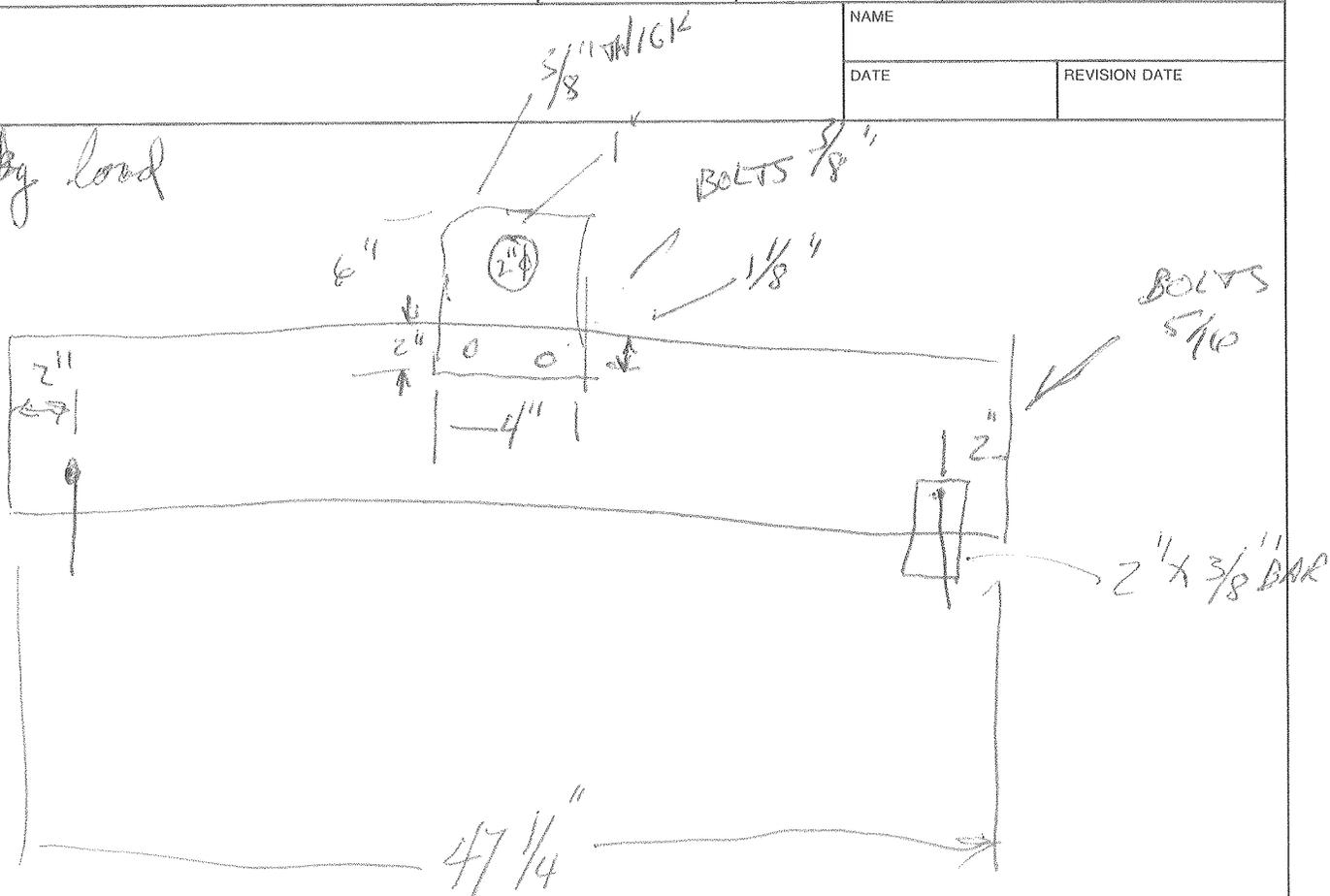
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NO by load



Mr. Fujii
RESPONSIBLE FOR
FIXTURE

