

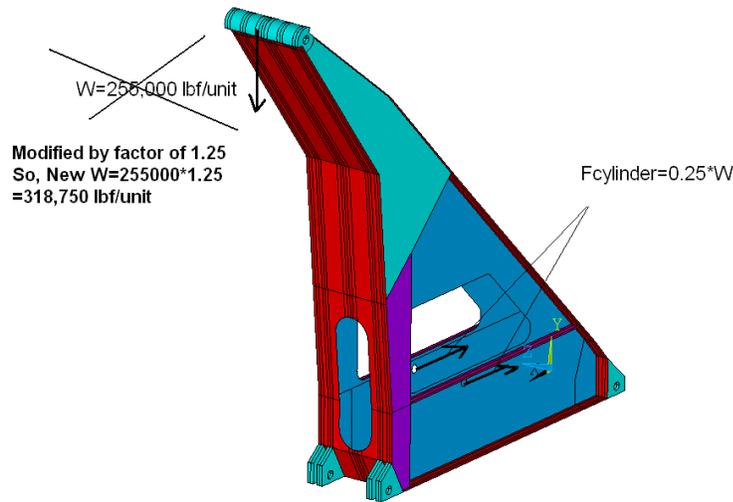
An Updated Analysis for the Upper Arm based on a Heavier Table and Extrusion

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Introduction

A steel upper arm, used for Nova pivot table assembly, is designed by D. Pushka as shown in Fig 1. This note is to update the calculation ⁽¹⁾ to reflect the latest loading change as indicated by reference 2. The structure is made of A-36 steel with an allowable of ~21.6 ksi.



upper_arm_4 shell element

Fig 1 The Upper Arm Structure with a heavier load

Modeling

One-half structure is modeled by a shell element (shell 181) in Ansys as shown in Fig 2 with a following condition:

- a) The gravity load from the table is applied on the top housing area as $W/2=255,000*1.25/2=159,375$ lb.
- b) The cylinder reaction (F_{cylin}) is estimated based on the earlier study ⁽³⁾. It is ~25% of the vertical load W.
- c) The constraints, for both front and back housing, are shown in Fig 2. For the front one, top half is constrained along the radial direction only with free rotation along the tangential direction. The back housing is constrained in a similar fashion, except it is on the lower half.

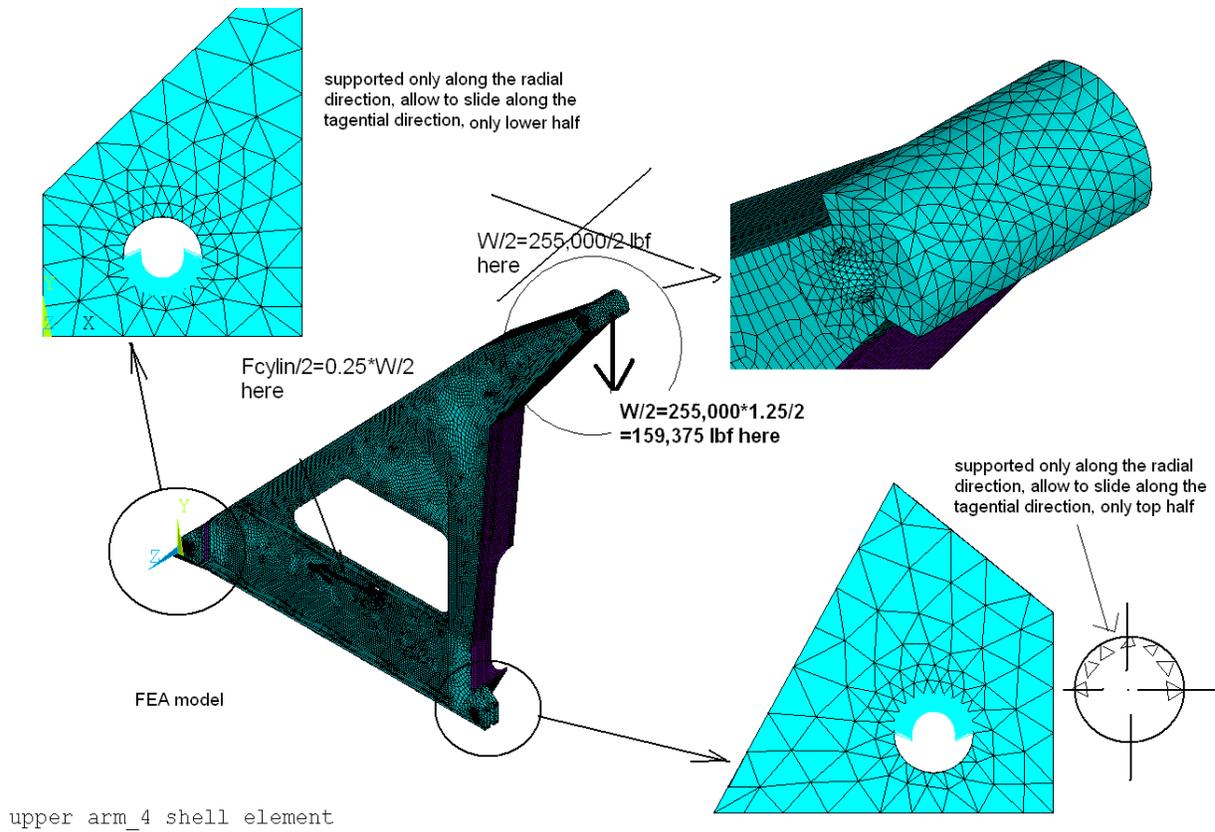


Fig 2 FEA model

Result and Discussion

a) Structure member

The calculation result is summarized in Table 1. The structure member seems adequate for a given loading case.

Table 1 Stress for the upper arm

Parts	#1_ upper reinforcement	#2_ lower reinforcement	#3_top flange	#4_web section	# 5_ mid reinforcement	#6_back bracket	#7_ the front bracket	#8_top housing
Plate Thickness (inch)	2"	1"	2"	1"	0.5"	Solid block	Solid block	Solid block
Stress (ksi)	12.2	8.1	20.2	16.75	14.7	12.25	20.25	14.8
SF for the buckling	SF=17/1.25=13.6*							

*Note: For the buckling calculation, we simply just scale the load by using the earlier result ⁽¹⁾.

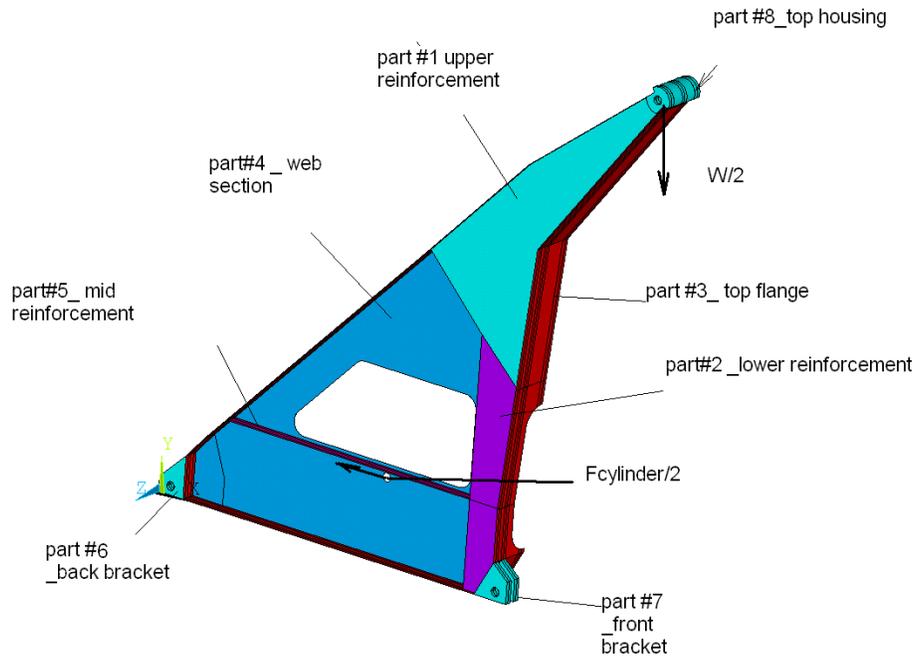


Fig 3 The description of the part

b) Weld stress

Most of welds are full size weld per weld drawing (3). We'll check several critical welds as:

- Front bracket area: the drawing shown is single bevel joint with size of 3/16" (view F-F). The minimum size for the partial penetration of the groove well should be at least $t_e(\min) = (tp/6)^{0.5} = (1/6)^{0.5} = 0.408''$ with 1/8" additional size.--> around 0.5" It gives a 0.5" inch as min weld size. **It is suggested weld size for both forward and rear pin area should be rechecked and revised accordingly in the drawing.**

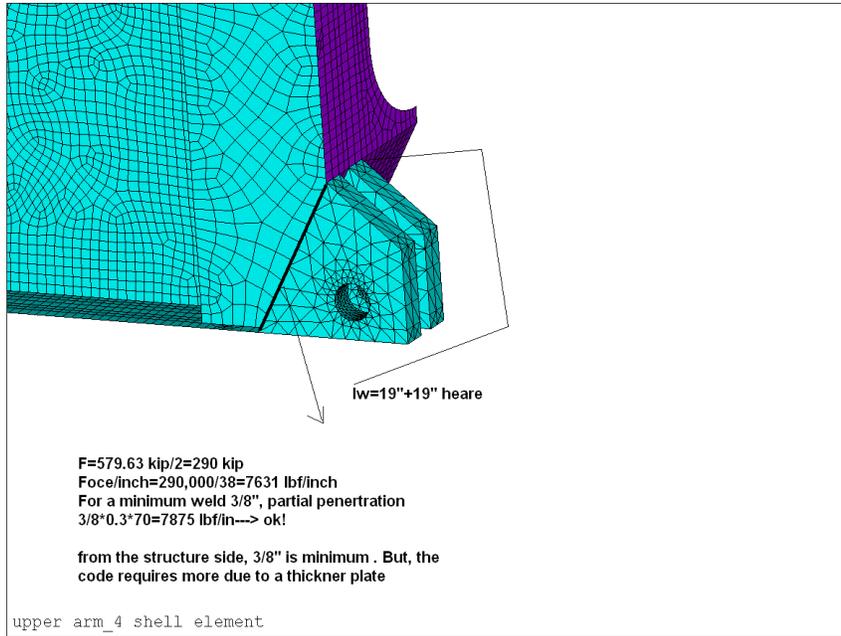


Fig 4 The weld size for forward pin area

- For the connection between Web and top flange, it is a double side, $0.5''$ continuously fillet weld (based on conversation with D Pushka). Therefore, we've scaled the shear stress of the top flange by a factor of 1.43 ($1/0.7$) to estimate the shear stress on the weld connection as shown in Fig 5. The maximum seems around 11 ksi $< 0.3 \cdot 70$. The node force summation also indicates the weld stress is fine for this region as shown in Fig 6.

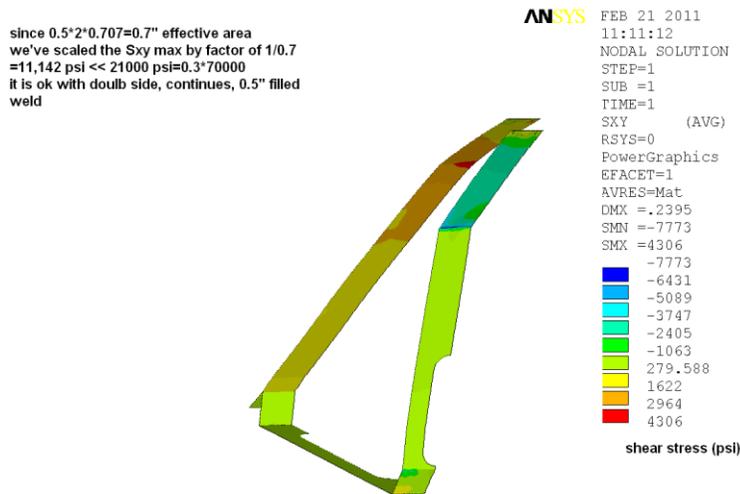


Fig 5 The shear stress plot for the top flange

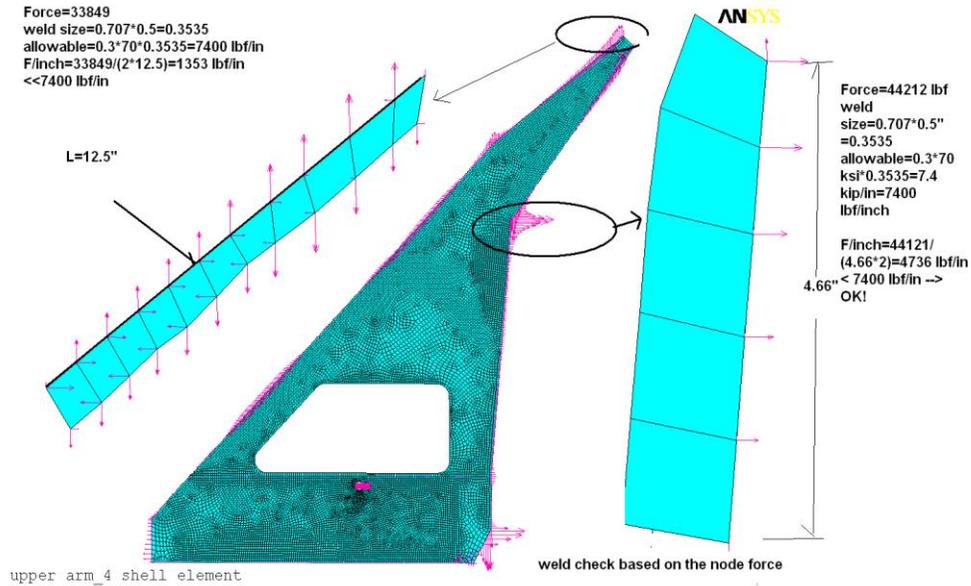


Fig 6 The node force summation result

Reference

- 1)Ang Lee," An Updated Calculation for the Upper Arm used in FHEP", Nova-doc-4217-v1,Sept 15, 2009
- 2) Dave Pushka," Evaluation of Design for Heavier Modules",MD-EBG-304, Jan 19, 2011
- 3) Ang Lee,"A Stress Analysis for the Upper Arm of the Pivot Table",Nova-doc-3666-v1, March 20, 2009
- 4)PPD_Weld Drawing," Nova FHEP PIVOTER UPPER FRAME ASSEMBLY WELDMENT",# 3929.220-ME-466549, OCT-26-2009

Appendix
Sterss plot

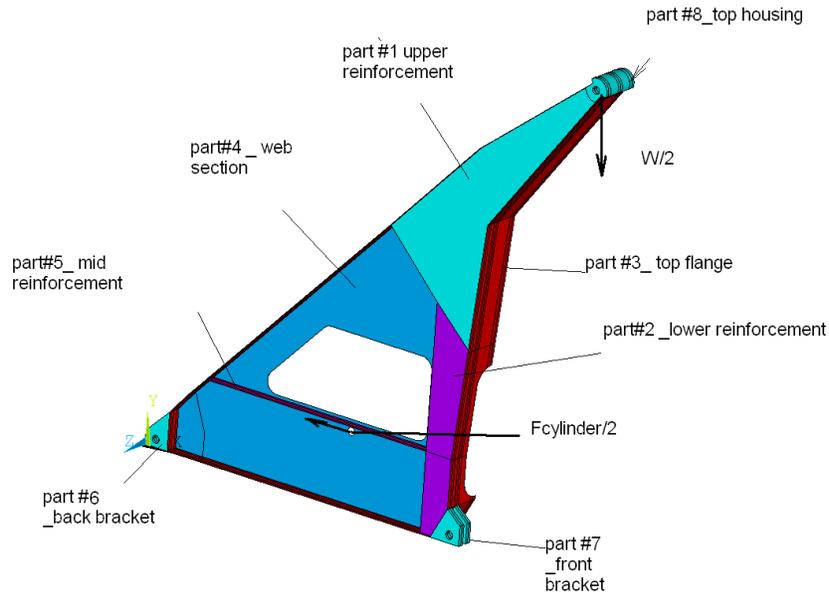


Fig A-1 The description of the parts

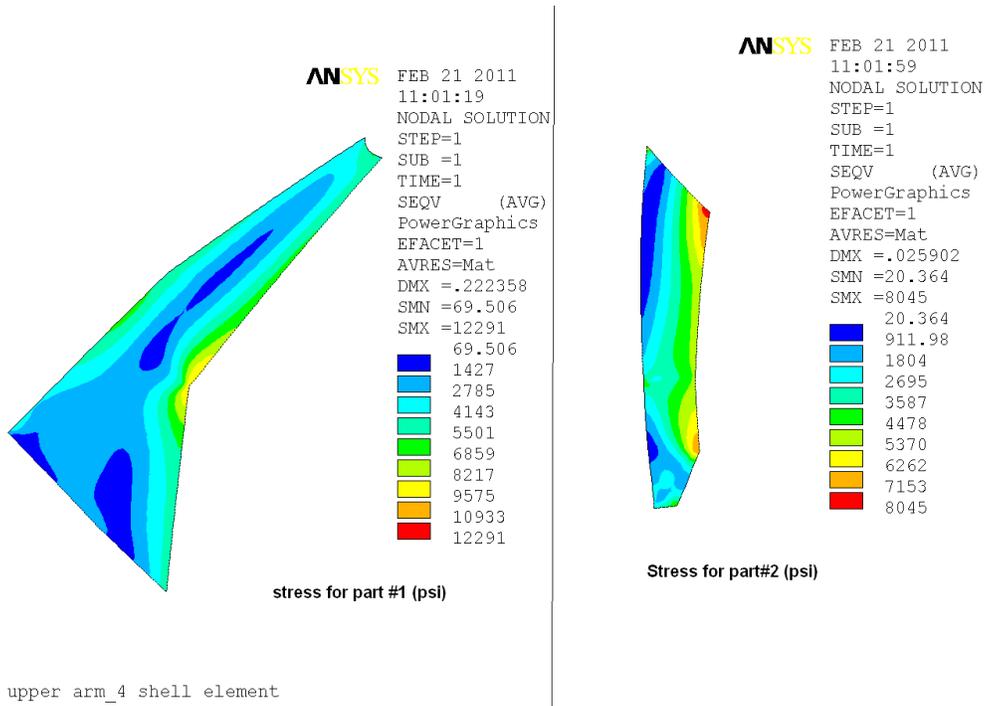
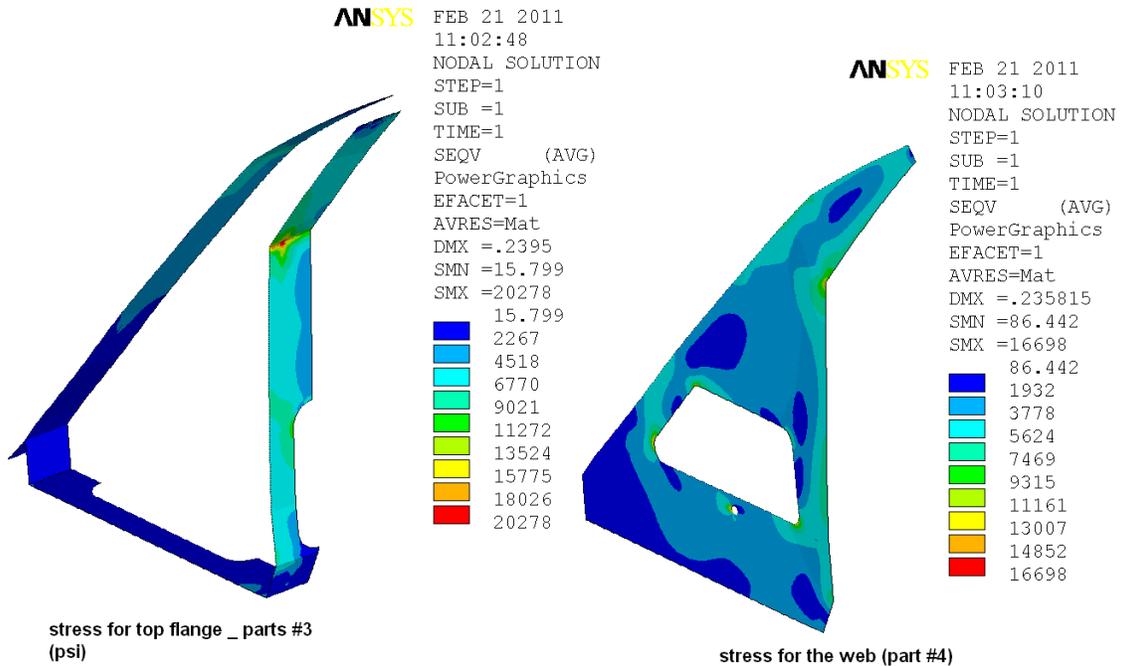


Fig A-2 Stress for part #1 and #2



upper arm_4 shell element

Fig A-3 Stress for part #3 and #4

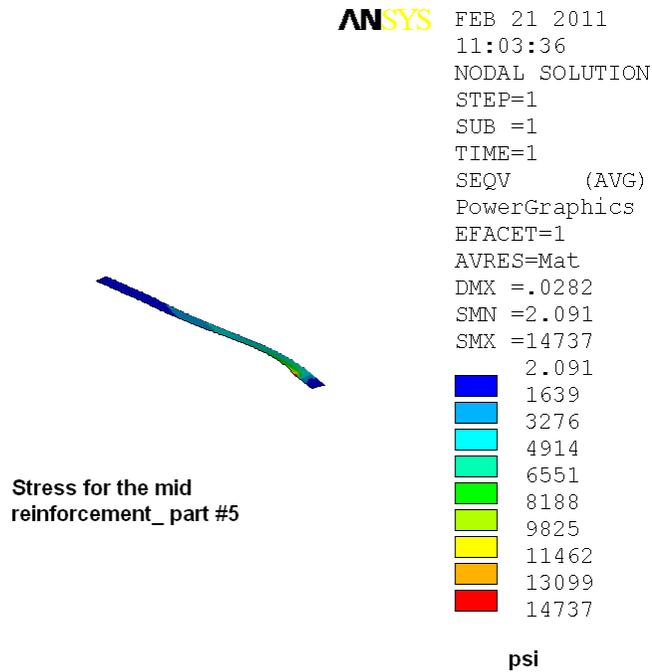
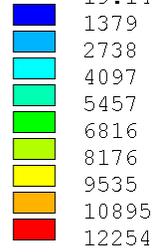
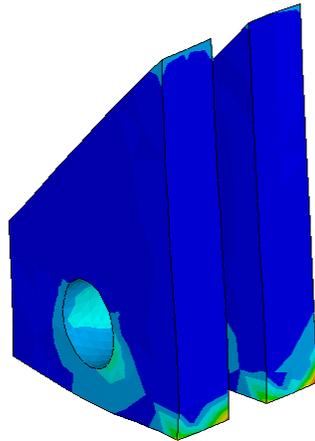


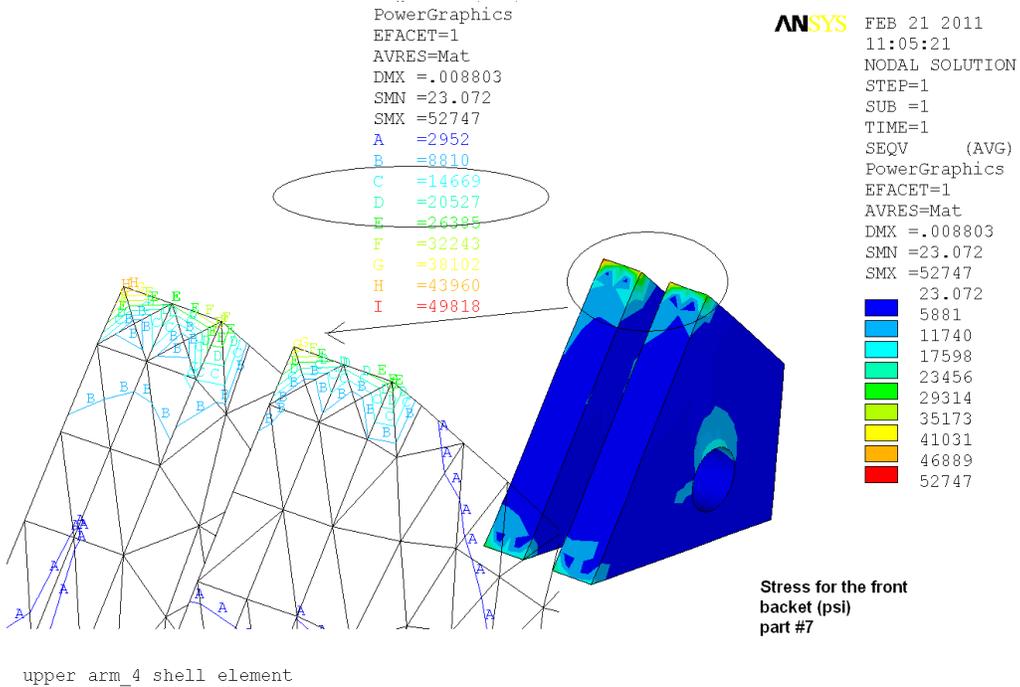
Fig A-4 Stress for part #5

ANSYS FEB 21 2011
 11:04:40
 NODAL SOLUTION
 STEP=1
 SUB =1
 TIME=1
 SEQV (AVG)
 PowerGraphics
 EFACET=1
 AVRES=Mat
 DMX =.823E-03
 SMN =19.148
 SMX =12254



stress for the back bracket
 (psi)
 part #6

Fig A-5 Stress for the back bracket



Stress for the front
 bracket (psi)
 part #7

Fig A-6 Stress for the front bracket , part #7

ANSYS FEB 21 2011
11:08:40
NODAL SOLUTION
STEP=1
SUB =1
TIME=1
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.252505
SMN =9.175
SMX =14852

9.175
1658
3308
4957
6606
8255
9904
11554
13203
14852

Stress for top housing (psi)

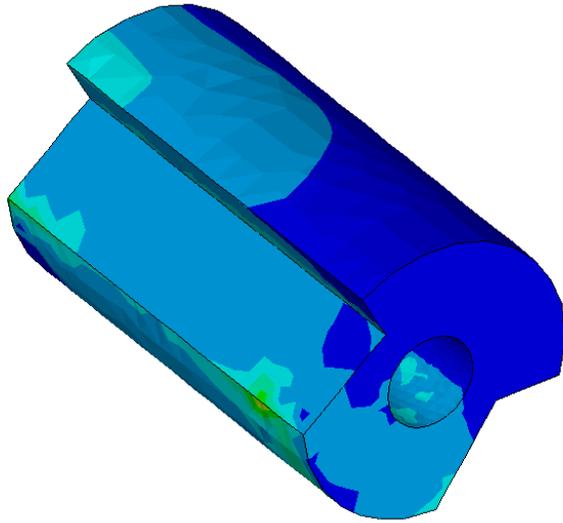


Fig A-7 Stress for the top housing

PPD weld drawing

