

Fermilab

**Particle Physics Division
Mechanical Department Engineering Note**

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Project: NuMI / MINOS

Title: ODH Analysis for NuMI Below Ground Spaces

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Key Words: ODH Analysis,

Abstract Summary: Analysis of the effects of various quantities of inert gas used in the underground spaces of NuMI and MINOS. Result is that under all conditions, these spaces with the quantities of gas used or stored below ground, remain ODH classification 0.

Analysis considers:

- Inert Argon CO₂ (80/20) for the Total Loss Monitor.
- Helium used for the target.
- Nitrogen used for the head spaces on the expansion tanks for the RAW systems in the mechanical support room under MI-65
- Inert gas used in the Muon and Hadron monitors in the muon alcove and absorber enclosure. Gas is either Helium or Argon (depending on the run conditions) per Sacha Kopp.

Applicable Codes: FESHM 5064

Discussion:

NuMI will have four systems located underground which will use inert gas. These systems include:

- 1) The nitrogen blanket used on the Target, Horn 1, Horn 2 and Decay pipe cooling RAW systems located in the target hall mechanical support room (THSR).
- 2) A helium gas pressure applied to the target in the target hall.
- 3) A total Loss Monitor which is fed gas from a bottle located underground in the electrical support room.
- 4) The gas system used at the downstream (MINOS) end of the project for the Muon Monitors and the Hadron Monitor. Both the Muon Monitors and the Hadron Monitor systems are fed gas from the same gas system. This system uses either Helium or Argon depending on the run conditions.

This analysis does not attempt to quantify an ODH analysis for any of the above ground service buildings (MI-60, MI-62). GN2 will be used in MI-62. GN2 will flow through MI-60. Additional ODH analysis will have to be addressed separately.

Ventilation details for the underground spaces are documented in FESS drawings for project 6-7-6 (NuMI Outfitting). See Drawings M-3, M-4 and M-5 attached.

The Nitrogen Blanket for the RAW systems in the Target Hall Mechanical Support Room (THSR)

This system will be fed GN2 from a Dewar located outside of MI-60. The lines have been run through MI-60 (pump room, north power supply room) down into the tunnel, to MI-62, with a branch line going down the NuMI stub, the stub extension, the RCP (round concrete pipe) carrier pipe, the drill and blast (D&B) portion of the carrier pipe, the pre-target, thru the labyrinth pipe chase (a non-habitable area), and into the target hall mechanical support room. The only place along this route where GN2 will be used in the THSR. Here, a small amount of GN2 (1 scfh) will be bled through each of four expansion tanks and vented into the room.

Three of the four expansion tanks are 100 gallon capacity, code stamped vessels. Each will be half filled with water and half filled with gas at less than 10 psig. The forth vessel is approximately 30 gallon capacity, also code stamped and also planned to operate half filled with water, half filled with gas at about 10 psig.

The Dewar has a MAWP of 250 psig but is currently labeled to operate the pressure between 30 and 50 psig. For NuMI needs, the Dewar does not need to operate above 100 psig, so a pressure of 100 psig is used to calculate the flow rate out of the copper tubing should it be severed in each area. Obviously, the flow rate out of the end of the severed tubing increases as the location of the sever gets closer to the gas source. The equation 3-20 from Crane Technical Paper 410 was used to calculate the flow rates.

Details on the MI-60 Dewar are not set. The responsibility for installing and commissioning this Dewar and performing the ODH analysis for MI-60 rests on the shoulders of Maurice Ball and the Accelerator Division Mechanical Department. As of the date that this engineering note has been written, the MI-60 Nitrogen Dewar is locked out. The Dewar does not appear to meet the current FESHM Dewar installation rules. Should the final Dewar installation not match the values assumed in this engineering note, this note will require a revision.

Initial operation of these systems will likely used compressed air in lieu of GN2 or will use one GN2 cylinder to provide a pressurized gas source. The analysis included for using a single GN2 or argon cylinder.

Target Helium

The target will be pressurized with helium from a gas bottle. The bottle will be located in the electrical support room next to the target hall. There helium is not planned to be purged through the target.

Total Loss Monitor

The total loss monitor will use Argon/ CO2 from a bottle in the electrical support room next to the target hall. The Ar/CO2 will be piped to the pre-target beam line and then all along the beam line, through the carrier tunnel, into the NuMI Stub, and to the inlet of the total loss monitor (TLM) at the upstream end of the NuMI stub. Then the TLM will carry the gas back down steam through four sections of TLM. The gas output will be routed back to the electrical support room next to the target hall where it will vent through a bubble. See the schematic on drawing 8875.117-MB-433163.

Muon and Hadron Monitors

The muon hadron monitors will be located in the muon alcoves (muon monitors) and in the absorber enclosure (hadron monitor). The gas will originate from a gas cylinder manifold near the bottom of the MINOS shaft. Gas will vent from each monitor and will be routed to the exhaust line (see FESS drawings for project 6-7-6 (NuMI Outfitting). Drawing M-5). This exhaust line will transport the gas to the suction of the exhaust fan located near the center of the decay pipe passage. Gas will either be Helium or Argon, depending on the run conditions.

General Notes Applicable to all Areas:

All ventilation rates listed are the ventilation rates of fresh, conditioned, make-up air. Mechanical HVAC drawings for these areas have been attached to this engineering note. Little air is re-circulated (refer to the drawings) and the re-circulated air is not considered in the ventilation rates.

All gas cylinders are planned to be 200 cubic feet. 230 cubic feet is used in the calculations in the spread sheets to account for cylinders filled to 110%.

ODH Calculations for the NuMI Underground Mechanical Support Room which uses GN2 from MI-60 for the RAW system expansion tanks head space. Considers each area that the GN2 line goes thru. Areas which intentionally bleed GN2 have a normal bleed rate. Others just have a leak based on a failure.

Complete rupture of the Nitrogen feed line into the NuMI Underground Mechanical Support Room:

Nitrogen comes from a dewar located near MI-60. 3/4 inch nominal size, type L copper lines bring the GN2 to this area

The calculated flow rate of gas out of this line if it were to be severed is:

95.5 cfm

Based on an outlet of 0 psig, and an inlet of :

100 psig

and a tubing length of:

1400 feet

Normal Ventilation Rate is :

440 cfm for this area

With the normal ventilation operating, the concentration of O2 would fall to : 0.1725515 % O2

However, the probability of having a brazed joint fail or of having one of the lines

rupture is sufficiently low that the fatality rate would only get to:

9.34E-10

Which results in an ODH classification of:

0

Refer to the table below:

Elevation 626 feet

Pressure 743.6 torr

| Item | Type | Number | Failure Rate | Group Failure Rate | Leak Rate (SCFM) | fO2 Fraction O2 | Fatality Factor | Fatality Rate | ODH Class |
|----------------------|-------------|--------|--------------|--------------------|------------------|-----------------|-----------------|---------------|-----------|
| Pipes < 3" | Sections | 70 | 1.00E-09 | 7.00E-08 | 95.5 | 0.1725515 | 4.67E-07 | 3.27E-14 | 0 |
| valve (MOV) | rupture | 2 | 1.00E-08 | 2.00E-08 | 80 | 0.1776923 | 1.94E-07 | 3.87E-15 | 0 |
| valve (AOV) | rupture | 2 | 1.00E-09 | 2.00E-09 | 80 | 0.1776923 | 1.94E-07 | 3.87E-16 | 0 |
| brazed joint | leak | 71 | 1.00E-09 | 7.10E-08 | 95.5 | 0.1725515 | 4.67E-07 | 3.31E-14 | 0 |
| partial ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 95.5 | 0.1725515 | 4.67E-07 | 4.67E-10 | 0 |
| complete ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 95.5 | 0.1725515 | 4.67E-07 | 4.67E-10 | 0 |
| Total | | | | | 9.34E-10 | | | 0 | |

ODH Calculations for the NuMI Underground Mechanical Support Room - Helium for Target

| Elevation Pressure Item | 626 feet 743.6 torr | | Type | Number | Failure Rate | Group Failure Rate | Leak Rate (SCFM) | fO2 Fraction O2 | Fatality Factor | Fatality Rate | ODH Class |
|-------------------------------|------------------------|----------|------|--------|--------------|--------------------|------------------|-----------------|-----------------|---------------|-----------|
| Pipes < 3" | in THSR | Sections | | 20 | 1.00E-09 | 2.00E-08 | 230 | 0.205863 | 1.55616E-09 | 3.11E-17 | 0 |
| Pipes < 3" | in Target hall | Sections | | 20 | 1.00E-09 | 2.00E-08 | 230 | 0.209639 | 8.15177E-10 | 1.63E-17 | 0 |
| valve (MOV) | in THSR | rupture | | 2 | 1.00E-08 | 2.00E-08 | 230 | 0.205863 | 1.55616E-09 | 3.11E-17 | 0 |
| valve (MOV) | in Target hall | rupture | | 2 | 1.00E-08 | 2.00E-08 | 230 | 0.209639 | 8.15177E-10 | 1.63E-17 | 0 |
| valve (AOV) | in THSR | rupture | | 2 | 1.00E-09 | 2.00E-09 | 230 | 0.205863 | 1.55616E-09 | 3.11E-18 | 0 |
| valve (AOV) | in Target hall | rupture | | 2 | 1.00E-09 | 2.00E-09 | 230 | 0.209639 | 8.15177E-10 | 1.63E-18 | 0 |
| brazed joint | in THSR | rupture | | 50 | 1.00E-09 | 5.00E-08 | 230 | 0.205863 | 1.55616E-09 | 7.78E-17 | 0 |
| brazed joint | in Target hall | rupture | | 50 | 1.00E-09 | 5.00E-08 | 230 | 0.209639 | 8.15177E-10 | 4.08E-17 | 0 |
| Total | | | | | | | | | | 1.77E-16 | 0 |

Complete rupture of the Helium feed line into the NuMI Underground Mechanical Support Room:

Helium from a 200 cubic foot gas cylinder supplies helium to the target. This gas isn't purged.

The maximum loss of helium is 230 cubic feet. This can occur in either the electrical room or the target hall

The volume of the room housing the helium cylinder is: 11445 cubic feet

The volume of the target hall is: 133650 cubic feet

Oxygen concentration assuming no ventilation and a sudden 200 cubic foot gas release in each volume is:

Target Hall Support room (THSR): 0.205863 fraction O2

Target Hall : 0.209639 fraction O2

In both areas, the O2 concentration does not fall below 18% considering an instantaneous loss of the cylinder contents and no ventilation. No further analysis is required.

Complete rupture of the Nitrogen feed line into the NuMI Underground Pre-Target Area:

The volume of this tunnel is conservatively 20,800 cubic feet (13 feet wide by 10 feet tall by 160 feet long). Actual volume is much bigger.

Nitrogen comes from a dewar located near MI-60. 3/4 inch nominal size, type L copper lines bring the GN2 to this area

The calculated flow rate of gas out of this line if it were to be severed is: 111.9 cfm

Based on an outlet of 0 psig, and an inlet of : 100 psig

and a tubing length of: 1019 feet

Normal Ventilation Rate is : 900 cfm for this area

With the normal ventilation operating, the concentration of O₂ would fall to : 0.1867719 % O₂

However, the probability of having a brazed joint fail or of having one of the lines

rupture is sufficiently low that the fatality rate would only get to: 8.18E-11

Which results in an ODH classification of: 0

Refer to the table below:

Elevation 626 feet

Pressure 743.6 torr

| Item | Type | Number | Failure Rate | Group Failure Rate | Leak Rate (SCFM) | fO ₂ O ₂ | Fatality Fraction | Fatality Factor | Fatality Rate | ODH Class |
|----------------------|-------------|--------|--------------|--------------------|------------------|--------------------------------|-------------------|-----------------|---------------|-----------|
| Pipes < 3" | Sections | 70 | 1.00E-09 | 7.00E-08 | 111.9 | 0.1867719 | 4.09E-08 | 2.86E-15 | 0 | |
| brazed joint | leak | 71 | 1.00E-09 | 7.10E-08 | 111.9 | 0.1867719 | 4.09E-08 | 2.90E-15 | 0 | |
| partial ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 111.9 | 0.1867719 | 4.09E-08 | 4.09E-11 | 0 | |
| complete ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 111.9 | 0.1867719 | 4.09E-08 | 4.09E-11 | 0 | |
| Total | | | | | 8.18E-11 | | | | 0 | |

Complete rupture of the Nitrogen feed line in the Drill and Blast portion of the Carrier Tunnel.

The volume of this tunnel is conservatively 12000 cubic feet (10 feet wide by 6 feet tall by 200 feet long).

Nitrogen comes from a dewar located near MI-60. 3/4 inch nominal size, type L copper lines bring the GN2 to this area

The calculated flow rate of gas out of this line if it were to be severed is: 126.7 cfm

Based on an outlet of 0 psig, and an inlet of : 100 psig

and a tubing length of: 795 feet

Normal Ventilation Rate is : 1000 cfm for this area

With the normal ventilation operating, the concentration of O₂ would fall to : 0.1863815 % O₂

However, the probability of having a brazed joint fail or of having one of the lines

rupture is sufficiently low that the fatality rate would only get to: 8.74E-11

Which results in an ODH classification of: 0

Refer to the table below:

Elevation 626 feet

Pressure 743.6 torr

| Item | Type | Number | Failure Rate | Group Failure Rate | Leak Rate (SCFM) | fO ₂ O ₂ | Fatality Fraction | Fatality Factor | Fatality Rate | ODH Class |
|----------------------|-------------|--------|--------------|--------------------|------------------|--------------------------------|-------------------|-----------------|---------------|-----------|
| Pipes < 3" | Sections | 70 | 1.00E-09 | 7.00E-08 | 126.7 | 0.1863815 | 4.37E-08 | 3.06E-15 | 0 | |
| brazed joint | leak | 71 | 1.00E-09 | 7.10E-08 | 126.7 | 0.1863815 | 4.37E-08 | 3.10E-15 | 0 | |
| partial ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 126.7 | 0.1863815 | 4.37E-08 | 4.37E-11 | 0 | |
| complete ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 126.7 | 0.1863815 | 4.37E-08 | 4.37E-11 | 0 | |
| Total | | | | | 8.74E-11 | | | | 0 | |

Complete rupture of the Nitrogen feed line in the Round Concrete Pre-Cast Lined portion of the Carrier Tunnel.

The volume of this tunnel is conservatively 6107 cubic feet (6 feet diameter by 216 feet long).

Nitrogen comes from a dewar located near MI-60. 3/4 inch nominal size, type L copper lines bring the GN2 to this area

The calculated flow rate of gas out of this line if it were to be severed is: 151.7 cfm

Based on an outlet of 0 psig, and an inlet of : 100 psig

and a tubing length of: 555 feet

Normal Ventilation Rate is : 1000 cfm for this area

With the normal ventilation operating, the concentration of O2 would fall to : 0.1823446 % O2

However, the probability of having a brazed joint fail or of having one of the lines

rupture is sufficiently low that the fatality rate would only get to: 1.75E-10

Which results in an ODH classification of: 0

Refer to the table below:

Elevation 626 feet

Pressure 743.6 torr

| Item | Type | Number | Failure Rate | Group Failure Rate | Leak Rate (SCFM) | fO2 Fraction O2 | Fatality Factor | Fatality Rate | ODH Class |
|----------------------|-------------|--------|--------------|--------------------|------------------|-----------------|-----------------|---------------|-----------|
| Pipes < 3" | Sections | 70 | 1.00E-09 | 7.00E-08 | 151.7 | 0.1823446 | 8.73E-08 | 6.11E-15 | 0 |
| brazed joint | leak | 71 | 1.00E-09 | 7.10E-08 | 151.7 | 0.1823446 | 8.73E-08 | 6.20E-15 | 0 |
| partial ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 151.7 | 0.1823446 | 8.73E-08 | 8.73E-11 | 0 |
| complete ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 151.7 | 0.1823446 | 8.73E-08 | 8.73E-11 | 0 |
| Total | | | | | | | 1.75E-10 | 0 | |

Complete rupture of the Nitrogen feed line in the NumI Stub and Stub Extension

The volume of this enclosure is conservatively 20000 cubic feet (10 feet wide, 10 feet tall by 200 feet long). Actual volume larger due to higher ceilings.

Nitrogen comes from a dewar located near MI-60. 3/4 inch nominal size, type L copper lines bring the GN2 to this area

The calculated flow rate of gas out of this line if it were to be severed is: 188.3 cfm

Based on an outlet of 0 psig, and an inlet of : 100 psig

and a tubing length of: 360 feet

Normal Ventilation Rate is : 1000 cfm for this area

With the normal ventilation operating, the concentration of O2 would fall to : 0.176721 % O2

However, the probability of having a brazed joint fail or of having one of the lines

rupture is sufficiently low that the fatality rate would only get to: 4.57E-10

Which results in an ODH classification of: 0

Refer to the table below:

Elevation 626 feet

Pressure 743.6 torr

| Item | Type | Number | Failure Rate | Group Failure Rate | Leak Rate (SCFM) | fO2 Fraction O2 | Fatality Factor | Fatality Rate | ODH Class |
|----------------------|-------------|--------|--------------|--------------------|------------------|-----------------|-----------------|---------------|-----------|
| Pipes < 3" | Sections | 70 | 1.00E-09 | 7.00E-08 | 188.3 | 0.176721 | 2.29E-07 | 1.60E-14 | 0 |
| brazed joint | leak | 71 | 1.00E-09 | 7.10E-08 | 188.3 | 0.176721 | 2.29E-07 | 1.62E-14 | 0 |
| partial ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 188.3 | 0.176721 | 2.29E-07 | 2.29E-10 | 0 |
| complete ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 188.3 | 0.176721 | 2.29E-07 | 2.29E-10 | 0 |
| Total | | | | | | | 4.57E-10 | 0 | |

Concentration of O₂ in the Mechanical Support Room as a function of time for normal ventilation and loss of ventilation conditions with the 'Normal' GN2 bleed rate into this space:

This area is ventilated by the main air handling equipment located in the MI-65 service building. The MI-65 equipment moves 440 cfm through this room. There is also a fan located at EAV-2 which draws air from the target hall and upstream spaces. The HVAC drawings indicate that EAV-2 should provide 26 cfm moving thru the mechanical support room. The volume is based on a room 12' tall, 35 feet long and 21.5 feet wide. There are four expansion tanks, each will get a little N2 bled thru it to remove any hydrogen. Bleed rate will be about 1 standard cubic feet per hour (scfh). This is 1/60 scfm. Therefore, bleed into the room will be $4 \cdot 1/60 = 0.066667$ cfm.

$$f_{O_2}(t) = \frac{0.21}{Q + R} \cdot (Q + R \cdot \exp(-\frac{(Q + R)}{V} \cdot t)) \cdot 100\%$$

VERY (!) Simple O₂ concentration Calculations

Normal Ventilation:

| Room | Normal | Room |
|-----------|------------|--------|
| Vent rate | Spill Rate | Volume |
| Q, cfm | R, cfm | V, cfm |
| 440 | 0.066667 | 9030 |

Just enter Q, R, V and see the O₂(t)

Concentration, O₂ % at (time = 10 days) = 20.9968

This does not cause an ODH condition since the oxygen concentration remains above 18%

* O₂ as a f(t) for the normal case of NuMI Mechanical Support Room

| t, min | t, hrs | t, days | C, % |
|--------|--------|---------|-------|
| 0 | 0 | 0 | 21.00 |
| 30 | 0.5 | 0.02 | 21.00 |
| 60 | 1 | 0.04 | 21.00 |
| 90 | 1.5 | 0.06 | 21.00 |
| 120 | 2 | 0.08 | 21.00 |
| 150 | 2.5 | 0.10 | 21.00 |
| 180 | 3 | 0.13 | 21.00 |
| 210 | 3.5 | 0.15 | 21.00 |
| 240 | 4 | 0.17 | 21.00 |
| 14400 | 240 | 10.00 | 21.00 |

Complete Loss of Ventilation:

| Room | Normal | Room |
|-----------|------------|--------|
| Vent rate | Spill Rate | Volume |
| Q, cfm | R, cfm | V, cfm |
| 0 | 0.066667 | 9030 |

Just enter Q, R, V and see the O₂(t)

Concentration, O₂ % at (time = 10 days) = 18.8820

This does not cause an ODH condition since the oxygen concentration remains above 18%

* O₂ as a f(t) for the worst case ventilation loss of NuMI Mechanical Support Room.

| t, min | t, hrs | t, days | C, % |
|--------|--------|---------|---------|
| 0 | 0 | 0 | 21.0000 |
| 30 | 0.5 | 0.02 | 20.9953 |
| 60 | 1 | 0.04 | 20.9907 |
| 90 | 1.5 | 0.06 | 20.9861 |
| 120 | 2 | 0.08 | 20.9814 |
| 150 | 2.5 | 0.10 | 20.9768 |
| 180 | 3 | 0.13 | 20.9721 |
| 210 | 3.5 | 0.15 | 20.9675 |
| 240 | 4 | 0.17 | 20.9628 |
| 14400 | 240 | 10.00 | 18.8820 |

Partial Loss of Ventilation:

| Room | Normal | Room |
|-----------|------------|--------|
| Vent rate | Spill Rate | Volume |
| Q, cfm | R, cfm | V, cfm |
| 26 | 0.066667 | 9030 |

Just enter Q, R, V and see the O₂(t)

Concentration, O₂ % at (time = 10 days) = 20.9463

This does not cause an ODH condition since the oxygen concentration remains above 18%

* O₂ as a f(t) for the worst case ventilation loss of NuMI Mechanical Support Room.

| t, min | t, hrs | t, days | C, % |
|--------|--------|---------|---------|
| 0 | 0 | 0 | 21.0000 |
| 30 | 0.5 | 0.02 | 20.9955 |
| 60 | 1 | 0.04 | 20.9915 |
| 90 | 1.5 | 0.06 | 20.9877 |
| 120 | 2 | 0.08 | 20.9843 |
| 150 | 2.5 | 0.10 | 20.9811 |
| 180 | 3 | 0.13 | 20.9782 |
| 210 | 3.5 | 0.15 | 20.9756 |
| 240 | 4 | 0.17 | 20.9732 |
| 14400 | 240 | 10.00 | 20.9463 |

**ODH Calculations for the NuMI Underground Mechanical Support Room - GN2 gas Cylinder used for initial commissioning
(gas used in the four expansion tanks)**

| Elevation | 626 feet | | | | | | | | |
|--------------------------|------------|--------|--------------|--------------------|------------------|----------|-----------------|---------------|-----------|
| Pressure | 743.6 torr | | | | | | | | |
| Item | Type | Number | Failure Rate | Group Failure Rate | Leak Rate (SCFM) | fO2 O2 | Fatality Factor | Fatality Rate | ODH Class |
| Pipes < 3" in THSR | Sections | 20 | 1.00E-09 | 2.00E-08 | 230 | 0.204784 | 3162278 | 6.32E-02 | 0 |
| Pipes < 3" in Target h: | Sections | 20 | 1.00E-09 | 2.00E-08 | 230 | 0.204784 | 3162278 | 6.32E-02 | 0 |
| valve (MOV) in THSR | rupture | 2 | 1.00E-08 | 2.00E-08 | 230 | 0.204784 | 3162278 | 6.32E-02 | 0 |
| valve (MOV) in Target h: | rupture | 2 | 1.00E-08 | 2.00E-08 | 230 | 0.204784 | 3162278 | 6.32E-02 | 0 |
| valve (AOV) in THSR | rupture | 2 | 1.00E-09 | 2.00E-09 | 230 | 0.204784 | 3162278 | 6.32E-03 | 0 |
| valve (AOV) in Target h: | rupture | 2 | 1.00E-09 | 2.00E-09 | 230 | 0.204784 | 3162278 | 6.32E-03 | 0 |
| brazed join in THSR | rupture | 50 | 1.00E-09 | 5.00E-08 | 230 | 0.204784 | 3162278 | 1.58E-01 | 0 |
| brazed join in Target h: | rupture | 50 | 1.00E-09 | 5.00E-08 | 230 | 0.204784 | 3162278 | 1.58E-01 | 0 |
| Total | | | | | | | | 4.24E-01 | 0 |

Complete rupture of the GN2 from a cylinder and the expansion tanks into the NuMI Underground Mechanical Support Room:

GN2 from a 200 cubic foot (230 used in the calculation) gas cylinder supplies GN2 to the water expansion tanks.
The maximum loss of helium is 230 cubic feet. This can occur in the mechanical room

The volume of the expansion tanks (3 @ 100 gallons + 1 at 30 gallons) half full 165 gallons
 The volume of the expansion tanks (3 @ 100 gallons + 1 at 30 gallons) half full 22.058824 cubic feet
 Capacity of the expansion tanks half filled with gas at 15 psig 44.117647 scf
 The volume of the room housing the gas cylinder is: 9030 cubic feet

Oxygen concentration assuming no ventilation and a sudden 200 cubic foot gas release in the room is:
 Target Hall Support room (THSR): 0.204784 fraction O2

Oxygen concentration assuming no ventilation and a sudden 275 cubic foot (230 + 45 cubic feet) gas release in the room is:
 Target Hall Support room (THSR): 0.203794 fraction O2
 Note, this analysis is applicable if the gas is changed from GN2 to argon.
 In both areas, the O2 concentration does not fall below 18% considering an instantaneous loss of the cylinder contents
 and no ventilation. No further analysis is required.

ODH Calculations for the NuMI Muon Alcoves Room with the inert gas mixture used in the muon detectors and the hadron monitor:

Complete Loss of Gas Bottle Contents at the Gas Rack below ground at MINOS Shaft bottom:

Muon Monitor and the Hadron gas system will use eight (8) two hundred (200) cubic foot bottles of inert gas connected to a manifold. This bottle manifold will be in the underground near the MINOS shaft (not in the fire escape egress passage).

The volume in the area of the MINOS shaft is not less than : 69272.12 cubic feet

based on a tunnel cross section of 21 feet diameter extending 100 feet towards MINOS and 100 feet up the shaft

Should this manifold suddenly loose 100% of all eight bottle inert contents into this space, the oxygen concentration (assuming no ventilation) will drop to:

Concentration, O₂ %= 20.52591 This does not cause an ODH condition since the oxygen concentration remains above 18%
 One does not need to go any further and consider the probability if this failure occurring since even if the bottle was breached, the oxygen concentration stays above 18%

Complete Loss of Gas Bottle Contents at the Gas Rack below ground in a Muon Alcove:

Muon Monitor and the Hadron gas system will use eight (8) two hundred (200) cubic foot bottles of inert gas connected to a manifold.

This bottle manifold will be in the underground near the MINOS shaft (not in the fire escape egress passage) and piped to the alcoves.

The volume in the muon alcove is not less than : 3016 cubic feet

based on a space 9'-10" deep, 12 feet tall and 12 feet across and a hallway 8' wide, by 8' tall by 25 feet long

Should this manifold suddenly loose 100% of all eight bottle inert contents into this space, the oxygen concentration (assuming no ventilation) will drop to:

Concentration, O₂ %= 13.72097 This would be an ODH condition since the oxygen concentration falls below 18%
 One needs to consider the probability of the valves failing and causing the entire contents of the gas rack to dump into one muon alcove.

ODH Calculations for the NuMI Muon Alcoves Room with the inert gas mixture used in the muon detectors and the hadron monitor considering the probability of a failure of each component. Assumes the entire contents of the gas rack discharge into one Muon Alcove in 1 minute time:

| Elevation | 430 feet | Pressure | 748.7 torr | Item | Type | Number | Failure Rate | Group Failure | Leak Rate | fO ₂ Fraction | Fatality Factor | Fatality Rate | ODH Class |
|----------------------|-------------|----------|------------|----------|---------|--------|--------------|---------------|-------------|--------------------------|-----------------|---------------|-----------|
| | | | | | | | | | Rate (SCFM) | O ₂ | | | |
| Pipes < 3" | Sections | 200 | 1.00E-09 | 2.00E-07 | | 1840 | | 0.04832636 | | 1 | 2.00E-07 | | 0 |
| valve (MOV) | rupture | 2 | 1.00E-08 | 2.00E-08 | | 1840 | | 0.04832636 | | 1 | 2.00E-08 | | 0 |
| valve (AOV) | rupture | 2 | 1.00E-09 | 2.00E-09 | | 1840 | | 0.04832636 | | 1 | 2.00E-09 | | 0 |
| brazed joint | leak | 10 | 1.00E-09 | 1.00E-08 | | 1840 | | 0.04832636 | | 1 | 1.00E-08 | | 0 |
| partial ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 0.03532 | | 0.209986515 | | 5.99233E-10 | | 5.99E-13 | | 0 |
| complete ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 0.03532 | | 0.209986515 | | 5.99233E-10 | | 5.99E-13 | | 0 |
| Total | | | | | | | | | 2.32E-07 | | | | 0 |

Conclusion: The ODH classification remains 0 because of the probability of the failures remains sufficiently low.

Complete Loss of Gas Bottle Contents at the Gas Rack below ground in the Absorber Enclosure:

Muon Monitor and the Hadron gas system will use eight (8) two hundred (200) cubic foot bottles of inert gas connected to a manifold.

This bottle manifold will be in the underground near the MINOS shaft (not in the fire escape egress passage) and piped to the alcoves.

The volume in the absorber enclosure is not less than : 15820 cubic feet

based on a space 40 feet long, 20 feet high and 27 feet wide minus the 17' by 17' by 20' absorber volume. This includes the first muon counter location.

Should this manifold suddenly loose 100% of all eight bottle inert contents into this space, the oxygen concentration (assuming no ventilation) will drop to:

Concentration, O₂ % = 19.07118

This would not be an ODH condition since the oxygen concentration remains above 18%

One does not need to go any further and consider the probability if this failure occurring since even if the bottle was breached, the oxygen concentration stays above 18%

Concentration of O₂ in the Muon Alcoves as a function of time for normal ventilation and loss of ventilation conditions:

There are two ventilation fans in this area. One fan exchanges air with the absorber access tunnel at 495 cfm. The other fan is the exhaust fan which draws air out of each alcove (and the vacuum pump exhaust) at a rate of approximately 55 cfm and transports this air to the suction of EAV-3 near the middle of the decay pipe.

Each of these fans provide air exchange for the alcoves. One case considers the loss of the both fans while the other considers the loss of the large fan. Muon Alcove Volume is approximately 9'-10" in z, 12'-0" tall and 12'-0" wide. The hallway entry is about 8'-0" wide, 8'-0" tall and about 25'-0" long. The hallway volume is ignored below.

$$f_{O_2}(t) = \frac{0.21}{Q + R} \cdot (Q + R \cdot \exp(-\frac{(Q + R)}{V} \cdot t)) \cdot 100\%$$

VERY (!) Simple O₂ concentration Calculations

Normal Ventilation:

| Room | Normal | Room |
|-----------|------------|--------|
| Vent rate | Spill Rate | Volume |
| Q, cfm | R, cfm | V, cf |
| 550 | 0.03532 | 3016 |

Just enter Q, R, V and see the O₂(t)

Per Sacha Kopp, the anticipated gas usage thru the detector is .60 liters per hour which equates to 0.03532 cfm

Concentration, O₂ % at (time = 10 days) = 20.9987

This does not cause an ODH condition since the oxygen concentration remains above 18%

Complete Loss of Ventilation:

| Room | Normal | Room |
|-----------|------------|--------|
| Vent rate | Spill Rate | Volume |
| Q, cfm | R, cfm | V, cf |
| 0 | 0.03532 | 3016 |

Just enter Q, R, V and see the O₂(t)

Concentration, O₂ % at (time = 10 days) = 17.7411

This does cause an ODH condition after two days of ventilation loss since the oxygen concentration falls below 18%
However, because the probability of both fans failing is low (see the table below), the ODH class remains at 0

Partial Loss of Ventilation:

| Room | Normal | Room |
|-----------|------------|--------|
| Vent rate | Spill Rate | Volume |
| Q, cfm | R, cfm | V, cf |
| 55 | 0.03532 | 3016 |

Just enter Q, R, V and see the O₂(t)

Concentration, O₂ % at (time = 10 days) = 20.9865

This does not cause an ODH condition since the oxygen concentration remains above 18%

* O₂ as a f(t) for the normal case of NuMI Muon Alcoves

| t, min | t, hrs | t, days | C, % |
|--------|--------|---------|---------|
| 0 | 0 | 0 | 21.0000 |
| 30 | 0.5 | 0.02 | 20.9987 |
| 60 | 1 | 0.04 | 20.9987 |
| 90 | 1.5 | 0.06 | 20.9987 |
| 120 | 2 | 0.08 | 20.9987 |
| 150 | 2.5 | 0.10 | 20.9987 |
| 180 | 3 | 0.13 | 20.9987 |
| 210 | 3.5 | 0.15 | 20.9987 |
| 240 | 4 | 0.17 | 20.9987 |
| 14400 | 240 | 10.00 | 20.9987 |

* O₂ as a f(t) for the worst case ventilation loss of NuMI Muon Alcoves

| t, min | t, hrs | t, days | C, % |
|--------|--------|---------|---------|
| 0 | 0 | 0 | 21.0000 |
| 30 | 0.5 | 0.02 | 20.9926 |
| 60 | 1 | 0.04 | 20.9852 |
| 90 | 1.5 | 0.06 | 20.9779 |
| 120 | 2 | 0.08 | 20.9705 |
| 150 | 2.5 | 0.10 | 20.9631 |
| 180 | 3 | 0.13 | 20.9558 |
| 210 | 3.5 | 0.15 | 20.9484 |
| 240 | 4 | 0.17 | 20.9411 |
| 14400 | 240 | 10.00 | 17.7411 |

* O₂ as a f(t) for another case of ventilation loss for the NuMI Muon Alcoves

| t, min | t, hrs | t, days | C, % |
|--------|--------|---------|---------|
| 0 | 0 | 0 | 21.0000 |
| 30 | 0.5 | 0.02 | 20.9943 |
| 60 | 1 | 0.04 | 20.9910 |
| 90 | 1.5 | 0.06 | 20.9891 |
| 120 | 2 | 0.08 | 20.9880 |
| 150 | 2.5 | 0.10 | 20.9874 |
| 180 | 3 | 0.13 | 20.9870 |
| 210 | 3.5 | 0.15 | 20.9868 |
| 240 | 4 | 0.17 | 20.9867 |
| 14400 | 240 | 10.00 | 20.9865 |

ODH Calculations for the NuMI Muon Alcoves Room with the inert gas mixture used in the muon detectors and the hadron monitor considering the probability of a failure of each component. Assumes steady leak rate and a fan failure:

| Elevation | 430 feet | Pressure | 748.7 torr | Item | Type | Number | Failure Rate | Group Failure Rate | Leak Rate (SCFM) | fO2 Fraction O2 | Fatality Factor | Fatality Rate | ODH Class |
|----------------------|-------------|----------|------------|----------|---------|-------------|--------------|--------------------|------------------|-----------------|-----------------|---------------|-----------|
| Steady Vent | | 1 | 1.00E+00 | 1.00E+00 | 0.03532 | 0.209986515 | 5.99233E-10 | 5.99E-10 | 0 | | | | |
| partial ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 0.03532 | 0.209865228 | 6.11895E-10 | 6.12E-13 | 0 | | | | |
| complete ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 0.03532 | 0.177411328 | 1.64669E-07 | 1.65E-10 | 0 | | | | |
| Total | | | | | | | | | 7.65E-10 | | | | 0 |

Conclusion: The ODH classification remains 0 because of the probability of the failures remains sufficiently low.

ODH Calculations for the NuMI Electrical Support Room with the 80-20 Argon and CO₂ mixture used in the Total loss monitor (TLM):

| Elevation | 626 feet | Pressure | 743.6 torr | Item | Type | Number | Failure Rate | Group Failure Rate | Leak Rate (SCFM) | IO ₂ Fraction O ₂ | Fatality Factor | Fatality Rate | ODH Class |
|----------------------|-------------|----------|------------|----------|----------|----------|--------------|--------------------|------------------|---|-----------------|---------------|-----------|
| Pipes < 3" | Sections | 20 | 1.00E-09 | 2.00E-08 | 200 | 0.144375 | 5.81E-05 | 1.16E-12 | 0 | | | | |
| valve (MOV) | rupture | 2 | 1.00E-08 | 2.00E-08 | 200 | 0.144375 | 5.81E-05 | 1.16E-12 | 0 | | | | |
| valve (AOV) | rupture | 2 | 1.00E-09 | 2.00E-09 | 200 | 0.144375 | 5.81E-05 | 1.16E-13 | 0 | | | | |
| brazed joint | leak | 100 | 1.00E-09 | 1.00E-07 | 200 | 0.144375 | 5.81E-05 | 5.81E-12 | 0 | | | | |
| partial ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 0.002111 | 0.209999 | 7.66E-10 | 7.66E-13 | 0 | | | | |
| complete ventilation | fail to run | 1 | 1.00E-03 | 1.00E-03 | 0.002111 | 0.209999 | 7.66E-10 | 7.66E-13 | 0 | | | | |
| Total | | | | | | | 9.79E-12 | | 0 | | | | |

Complete Loss of Gas Bottle Contents at the Gas Rack below ground In the Electrical Support Room (location of gas bottle rack and the bubbler):

Loss Monitor (TLM) gas system will use one (1) two hundred (200) cubic foot bottle of Argon (80%) and CO₂ (20%) (230 cubic feet used below)

This bottle will be in the electrical support room underground. The volume of this area is 11,445 cubic feet.

Should this bottle suddenly loose 100% of its inert contents into this room, the oxygen concentration (assuming no ventilation) will drop to:

Concentration, O₂ % = 20.5863 This does not cause an ODH condition since the oxygen concentration remains above 18%
 One does not need to go any further and consider the probability if this failure occurring since even if
 the bottle was breached, the oxygen concentration stays above 18%

Complete Loss of Gas Bottle Contents in the Pretarget Tunnel.

Loss Monitor (TLM) gas system will use one (1) two hundred (200) cubic foot bottle of Argon (80%) and CO₂ (20%) (230 cubic feet used below)

The volume of this tunnel is conservatively 20,800 cubic feet (13 feet wide by 10 feet tall by 160 feet long). Actual volume is much bigger.

Should this bottle suddenly loose 100% of its inert contents into this room, the oxygen concentration (assuming no ventilation) will drop to:

Concentration, O₂ % = 20.77033 This does not cause an ODH condition since the oxygen concentration remains above 18%
 One does not need to go any further and consider the probability if this failure occurring since even if
 the bottle was breached, the oxygen concentration stays above 18%

Complete Loss of Gas Bottle Contents in the Drill and Blast portion of the Carrier Tunnel.

Loss Monitor (TLM) gas system will use one (1) two hundred (200) cubic foot bottle of Argon (80%) and CO₂ (20%) (230 cubic feet used below)

The volume of this tunnel is conservatively 12000 cubic feet (10 feet wide by 6 feet tall by 200 feet long).

Should this bottle suddenly loose 100% of its inert contents into this room, the oxygen concentration (assuming no ventilation) will drop to:

Concentration, O₂ % = 20.60507 This does not cause an ODH condition since the oxygen concentration remains above 18%
 One does not need to go any further and consider the probability if this failure occurring since even if
 the bottle was breached, the oxygen concentration stays above 18%

Complete Loss of Gas Bottle Contents in the Round Concrete Pre-Cast Lined portion of the Carrier Tunnel.

Loss Monitor (TLM) gas system will use one (1) two hundred (200) cubic foot bottle of Argon (80%) and CO₂ (20%) (230 cubic feet used below)

The volume of this tunnel is conservatively 6107 cubic feet (6 feet diameter by 216 feet long).

Should this bottle suddenly loose 100% of its inert contents into this room, the oxygen concentration (assuming no ventilation) will drop to:

Concentration, O₂ % = 20.23781 This does not cause an ODH condition since the oxygen concentration remains above 18%
 One does not need to go any further and consider the probability if this failure occurring since even if
 the bottle was breached, the oxygen concentration stays above 18%

Complete Loss of Gas Bottle Contents in the NuMI Stub and Stub Extension

Loss Monitor (TLM) gas system will use one (1) two hundred (200) cubic foot bottle of Argon (80%) and CO₂ (20%) (230 cubic feet used below)

The volume of this enclosure is conservatively 20000 cubic feet (10 feet wide, 10 feet tall by 200 feet long). Actual volume larger due to higher ceilings.

Should this bottle suddenly loose 100% of its inert contents into this room, the oxygen concentration (assuming no ventilation) will drop to:

Concentration, O₂ % = 20.76125 This does not cause an ODH condition since the oxygen concentration remains above 18%
 One does not need to go any further and consider the probability if this failure occurring since even if
 the bottle was breached, the oxygen concentration stays above 18%

Concentration of O₂ In the NuMI Electrical Support Room as a function of time for normal ventilation and loss of ventilation conditions:

This area is ventilated by the main air handling equipment located in the MI-65 service building. The MI-65 equipment moves 440 cfm through this room. There is also a fan located at EAV-2 which draws air from the target hall and upstream spaces. The HVAC drawings indicate that EAV-2 should provide 26 cfm moving thru the electrical support room. This area is also ventilated by the penetration strip line fan, which has a capacity larger than 26 cfm.

$$f_{O_2}(t) = \frac{0.21}{Q + R} \cdot (Q + R \cdot \exp(-\frac{(Q + R)}{V} \cdot t)) \cdot 100\%$$

VERY (I) Simple O₂ concentration Calculations

Normal Ventilation:

| Room | Normal | Room |
|-----------|-----------|--------|
| Vent rate | Leak Rate | Volume |
| Q, cfm | R, cfm | V, cf |
| 440 | 0.002111 | 11445 |

Just enter Q, R, V and see the O₂(t)

Per Dan Schoo, the anticipated gas usage thru the detector is 86 liters per day which equates to 0.00211 cfm

Concentration, O₂ % at (time = 10 days) = 20.9999

This does not cause an ODH condition since the oxygen concentration remains above 18%

* O₂ as a f(t) for the normal case of NuMI electrical Support Room

| t, min | t, hrs | t, days | O ₂ % |
|--------|--------|---------|------------------|
| 0 | 0 | 0 | 21.0000 |
| 30 | 0.5 | 0.02 | 20.9999 |
| 60 | 1 | 0.04 | 20.9999 |
| 90 | 1.5 | 0.06 | 20.9999 |
| 120 | 2 | 0.08 | 20.9999 |
| 14400 | 240 | 10.00 | 20.9999 |

Complete Loss of Ventilation:

| Room | Normal | Room |
|-----------|------------|--------|
| Vent rate | Spill Rate | Volume |
| Q, cfm | R, cfm | V, cf |
| 0 | 0.002111 | 11445 |

Just enter Q, R, V and see the O₂(t)

Partial Loss of Ventilation:

| Room | Normal | Room |
|-----------|-----------|--------|
| Vent rate | Leak Rate | Volume |
| Q, cfm | R, cfm | V, cf |
| 26 | 0.002111 | 11445 |

Just enter Q, R, V and see the O₂(t)

Concentration, O₂ % at (time = 10 days) = 20.9983

This does not cause an ODH condition since the oxygen concentration remains above 18%

* O₂ as a f(t) for the worst case ventilation loss of NuMI electrical support room

| t, min | t, hrs | t, days | O ₂ % |
|--------|--------|---------|------------------|
| 0 | 0 | 0 | 21.0000 |
| 30 | 0.5 | 0.02 | 20.9999 |
| 60 | 1 | 0.04 | 20.9998 |
| 90 | 1.5 | 0.06 | 20.9997 |
| 120 | 2 | 0.08 | 20.9995 |
| 14400 | 240 | 10.00 | 20.9943 |

Concentration of O₂ In the NuMI Pre-Target Tunnel as a function of time for normal ventilation and loss of ventilation conditions:

This area is ventilated by the main air handling equipment located in the MI-65 service building. The MI-65 equipment moves about 900 cfm through this tunnel. There is also a fan located at EAV-1 which draws air out of this tunnel and exhausts at a rate of 900 cfm. The volume of this tunnel is conservatively 20,800 cubic feet (13 feet wide by 10 feet tall by 160 feet long). Actual volume is much bigger.

$$f_{O_2}(t) = \frac{0.21}{Q + R} \cdot (Q + R \cdot \exp(-\frac{(Q + R)}{V} \cdot t)) \cdot 100\%$$

VERY (I) Simple O₂ concentration Calculations

Normal Ventilation:

| Room | Normal | Room |
|-----------|-----------|--------|
| Vent rate | Leak Rate | Volume |
| Q, cfm | R, cfm | V, cf |
| 900 | 0.002111 | 20800 |

Just enter Q, R, V and see the O₂(t)

Per Dan Schoo, the anticipated gas usage thru the detector is 86 liters per day which equates to 0.00211 cfm

Concentration, O₂ % at (time = 10 days) = 21.0000

This does not cause an ODH condition since the oxygen concentration remains above 18%

* O₂ as a f(t) for the normal case of NuMI electrical Support Room

| t, min | t, hrs | t, days | O ₂ % |
|--------|--------|---------|------------------|
| 0 | 0 | 0 | 21.0000 |
| 30 | 0.5 | 0.02 | 21.0000 |
| 60 | 1 | 0.04 | 21.0000 |
| 90 | 1.5 | 0.06 | 21.0000 |
| 120 | 2 | 0.08 | 21.0000 |
| 14400 | 240 | 10.00 | 21.0000 |

Complete Loss of Ventilation:

| Room | Normal | Room |
|-----------|------------|--------|
| Vent rate | Spill Rate | Volume |
| Q, cfm | R, cfm | V, cf |
| 0 | 0.002111 | 20800 |

Just enter Q, R, V and see the O₂(t)

Partial Loss of Ventilation:

| Room | Normal | Room |
|-----------|-----------|--------|
| Vent rate | Leak Rate | Volume |
| Q, cfm | R, cfm | V, cf |
| 26 | 0.002111 | 20800 |

Just enter Q, R, V and see the O₂(t)

Concentration, O₂ % at (time = 10 days) = 20.9983

This does not cause an ODH condition since the oxygen concentration remains above 18%

* O₂ as a f(t) for the worst case ventilation loss of NuMI electrical support room

| t, min | t, hrs | t, days | O ₂ % |
|--------|--------|---------|------------------|
| 0 | 0 | 0 | 21.0000 |
| 30 | 0.5 | 0.02 | 20.9999 |
| 60 | 1 | 0.04 | 20.9999 |
| 90 | 1.5 | 0.06 | 20.9998 |
| 120 | 2 | 0.08 | 20.9997 |
| 14400 | 240 | 10.00 | 20.9693 |

Concentration of O₂ In the NuMI RCP Carrier Tunnel as a function of time for normal ventilation and loss of ventilation conditions:

This area is ventilated by two 1000 cfm fans. One fan pressurizes the area, the other draws air out of the area and into the pre-target tunnel. The volume of this space is about 12000 cubic feet. This assumes that the TLM bleeds 86 liters per day into this volume as a result of a pipe or tube failure and that there is a problem with the ventilation.

$$f_{O_2}(t) = \frac{0.21}{Q + R} \cdot (Q + R \cdot \exp(-\frac{(Q + R)}{V} \cdot t)) \cdot 100\%$$

VERY (I) Simple O₂ concentration Calculations

Normal Ventilation:

| Room | Normal | Room |
|-----------|-----------|--------|
| Vent rate | Leak Rate | Volume |
| Q, cfm | R, cfm | V, cf |
| 1000 | 0.002111 | 12000 |

Just enter Q, R, V and see the O₂(t)

Per Dan Schoo, the anticipated gas usage thru the detector is 86 liters per day which equates to 0.00211 cfm

Concentration, O₂ % at (time =
10 days) = 21.0000

This does not cause an ODH condition since
the oxygen concentration remains above
18%

* O₂ as a f(t) for the normal case of NuMI
electrical Support Room

| t, min | t, hrs | t, days | O ₂ % |
|--------|--------|---------|------------------|
| 0 | 0 | 0 | 21.0000 |
| 30 | 0.5 | 0.02 | 21.0000 |
| 60 | 1 | 0.04 | 21.0000 |
| 90 | 1.5 | 0.06 | 21.0000 |
| 120 | 2 | 0.08 | 21.0000 |
| 14400 | 240 | 10.00 | 21.0000 |

Complete Loss of Ventilation:

| Room | Normal | Room |
|-----------|------------|--------|
| Vent rate | Spill Rate | Volume |
| Q, cfm | R, cfm | V, cf |
| 0 | 0.002111 | 12000 |

Just enter Q, R, V and see the O₂(t)

Concentration, O₂ % at (time =
10 days) = 20.9469

This does not cause an ODH condition since
the oxygen concentration remains above
18%

* O₂ as a f(t) for the worst case ventilation
loss of NuMI electrical support room

| t, min | t, hrs | t, days | O ₂ % |
|--------|--------|---------|------------------|
| 0 | 0 | 0 | 21.0000 |
| 30 | 0.5 | 0.02 | 20.9999 |
| 60 | 1 | 0.04 | 20.9998 |
| 90 | 1.5 | 0.06 | 20.9997 |
| 120 | 2 | 0.08 | 20.9996 |
| 14400 | 240 | 10.00 | 20.9469 |

Partial Loss of Ventilation:

| Room | Normal | Room |
|-----------|-----------|--------|
| Vent rate | Leak Rate | Volume |
| Q, cfm | R, cfm | V, cf |
| 500 | 0.002111 | 12000 |

Just enter Q, R, V and see the O₂(t)

Concentration, O₂ % at (time =
10 days) = 20.9999

This does not cause an ODH condition since
the oxygen concentration remains above
18%

* O₂ as a f(t) for another case of ventilation
loss for the NuMI electrical support room

| t, min | t, hrs | t, days | O ₂ % |
|--------|--------|---------|------------------|
| 0 | 0 | 0 | 21.0000 |
| 30 | 0.5 | 0.02 | 20.9999 |
| 60 | 1 | 0.04 | 20.9999 |
| 90 | 1.5 | 0.06 | 20.9999 |
| 120 | 2 | 0.08 | 20.9999 |
| 14400 | 240 | 10.00 | 20.9999 |

| Measured Distances in the MI Enclosure | | |
|--|---|-------------------------|
| Downstream from Q608 Quad | Reference Point | Upstream from Q624 Quad |
| -0.50 | MI-60 Equipment Gallery RF19 Penetration | 770.75 |
| 0.00 | Q608 Center | 770.25 |
| 0.50 | MI-60 Equipment Gallery RF18 Penetration | 769.75 |
| 50.00 | Downstream Wall of Q609 Alcove | 720.25 |
| 58.00 | Q609 Center | 712.25 |
| 77.75 | Barrier Gate | 692.50 |
| 99.92 | Q610 Center | 670.33 |
| 142.67 | Q611 Center | 627.58 |
| 185.50 | Q612 Center | 584.75 |
| 188.25 | Exit Door Center Line | 582.00 |
| 227.33 | Q613 Center | 542.92 |
| 244.00 | Dual LCW Headers From MI-62 Transition Over Aisle | 526.25 |
| 264.42 | Edge of Wall Dividing A150 Line and Main Injector | 505.83 |
| 285.00 | Q614 Center | 485.25 |
| 343.00 | Q615 Center | 427.25 |
| 359.17 | Edge of Wall Dividing NuMI Stub and Main Injector | 411.08 |
| 372.58 | Enclosure Takes a Step Change in Width | 397.67 |
| 385.17 | Q616 Center | 385.08 |
| 400.33 | Level of Dual 18 Inch Tray Moves 10 Feet Toward S | 369.92 |
| 427.92 | Q617 Center | 342.33 |
| 432.83 | Enclosure Takes a Step Change in Width | 337.42 |
| 436.67 | Center Line of Passage to NuMI Stub Access | 333.58 |
| 470.75 | Q618 Centerline | 299.50 |
| 504.92 | Center Line of Penetrations to NuMI Stub | 265.33 |
| 512.75 | Q619 Center | 257.50 |
| 513.50 | Center Line of Exhaust Pipe from NuMI Stub | 256.75 |
| 570.50 | Q620 Center | 199.75 |
| 583.33 | End of 2nd Level of Dual 18 Inch Cable Tray | 186.92 |
| 627.50 | Q621 Center | 142.75 |
| 685.42 | Q622 Center | 84.83 |
| 727.58 | Q623 Center | 42.67 |
| 744.83 | MI-62 Controls/Kicker Room K1 Penetration | 25.42 |
| 758.17 | MI-62 Controls/Kicker Room K12 Penetration | 12.08 |
| 762.42 | Upstream Wall of MI-62 Alcove | 7.83 |
| 763.25 | MI-62 Power Supply Room Penetrations 1 and 11 | 7.00 |
| 767.33 | Ceiling LCW Penetrations | 2.92 |
| 770.25 | Q624 Center | 0.00 |
| 771.33 | MI-62 Power Supply Room Penetrations 10 and 20 | -1.08 |
| 778.33 | Downstream Wall of MI-62 Alcove | -8.08 |

(4) Q108

| line | location | typ_code | distance | x | y | z | brng | pitch |
|------|----------|----------|-----------|------------|------------|-----------|-----------|---------|
| | [ft] | [ft] | [ft] | [ft] | [deg] | [deg] | [deg] | |
| 0 | S1_BML | marker | -56.88634 | 101383.293 | 97215.3773 | 715.72409 | 148.73096 | 0.10571 |
| 1 | LAM60 | MI_LAM | -56.88634 | 101383.293 | 97215.3773 | 715.72409 | 148.73096 | 0.10571 |
| 2 | LAMEND | DRIFT | -47.7 | 101375.48 | 97220.2106 | 715.74102 | 148.69343 | 0.21142 |
| 3 | QSPPOOL | drift | -46.94423 | 101374.835 | 97220.6033 | 715.74381 | 148.69343 | 0.21142 |
| 4 | QENDU | drift | -46.52756 | 101374.479 | 97220.8198 | 715.74535 | 148.69343 | 0.21142 |
| 5 | HQ608 | 3Q84/2 | -46.40256 | 101374.372 | 97220.8848 | 715.74581 | 148.72552 | 0.22202 |
| 6 | HQ608 | 3Q84/2 | -42.90257 | 101371.38 | 97222.7018 | 715.7593 | 148.78998 | 0.24866 |
| 7 | QENDD | drift | -39.40258 | 101368.387 | 97224.5154 | 715.77442 | 148.82235 | 0.26471 |
| 8 | BPM | MI_BPM | -39.21006 | 101368.222 | 97224.6151 | 715.77531 | 148.82235 | 0.26471 |
| 9 | D3IN | drift | -38.54339 | 101367.652 | 97224.9602 | 715.77839 | 148.82235 | 0.26471 |
| 10 | LAMEND | DRIFT | -38.29339 | 101367.438 | 97225.0896 | 715.77954 | 148.82235 | 0.26471 |
| 11 | LAM61A | MI_LAM | -37.53762 | 101366.791 | 97225.4809 | 715.78302 | 148.81805 | 0.47957 |
| 12 | LAMEND | DRIFT | -28.35129 | 101358.932 | 97230.2372 | 715.85992 | 148.81376 | 0.69442 |
| 13 | LSPOOL | drift | -27.59552 | 101358.286 | 97230.6285 | 715.86907 | 148.81376 | 0.69442 |
| 14 | LAMEND | DRIFT | -27.09552 | 101357.858 | 97230.8874 | 715.87514 | 148.81376 | 0.69442 |
| 15 | LAM61B | MI_LAM | -26.33974 | 101357.211 | 97231.2788 | 715.8843 | 148.81376 | 0.90957 |
| 16 | LAMEND | DRIFT | -17.15341 | 101349.353 | 97236.0357 | 716.03016 | 148.81376 | 1.12472 |
| 17 | VALVE | VALVE | -16.3976 | 101348.706 | 97236.4271 | 716.04502 | 148.81376 | 1.12472 |
| 18 | LCSPOO | drift | -15.89761 | 101348.278 | 97236.6859 | 716.05483 | 148.81376 | 1.12472 |
| 19 | CMGEND | DRIFT | -15.42198 | 101347.872 | 97236.9322 | 716.06418 | 148.81376 | 1.12472 |
| 20 | V100 | MI_CMG | -14.75532 | 101347.301 | 97237.2773 | 716.07724 | 148.81376 | 1.36536 |
| 21 | CMGEND | DRIFT | -3.75531 | 101337.894 | 97242.9718 | 716.33935 | 148.81376 | 1.606 |
| 22 | NOVALV | drift | -3.08864 | 101337.324 | 97243.3168 | 716.35805 | 148.81376 | 1.606 |
| 23 | Q12_UP | DRIFT | -2.58864 | 101336.896 | 97243.5756 | 716.37206 | 148.81376 | 1.606 |
| 24 | HQD101 | 3Q120/2 | -2.01571 | 101336.406 | 97243.8722 | 716.3881 | 148.81376 | 1.606 |
| 25 | HQD101 | 3Q120/2 | 2.98428 | 101332.13 | 97246.4603 | 716.52826 | 148.81376 | 1.606 |
| 26 | Q101DN | drift | 7.98427 | 101327.855 | 97249.0484 | 716.66838 | 148.81376 | 1.606 |
| 27 | IP101A | ionpump | 8.8905 | 101327.08 | 97249.5175 | 716.69378 | 148.81376 | 1.606 |
| 28 | P101SE | drift | 9.3905 | 101326.652 | 97249.7763 | 716.70779 | 148.81376 | 1.606 |
| 29 | IP101B | ionpump | 15.6481 | 101321.301 | 97253.0153 | 716.88318 | 148.81376 | 1.606 |
| 30 | V101UP | drift | 16.1481 | 101320.873 | 97253.2741 | 716.89719 | 148.81376 | 1.606 |
| 31 | VP101 | BPM | 16.78766 | 101320.326 | 97253.6052 | 716.9151 | 148.81376 | 1.606 |
| 32 | BPM_DN | DRIFT | 17.321 | 101319.87 | 97253.8813 | 716.93006 | 148.81376 | 1.606 |
| 33 | BPM_UP | DRIFT | 17.42933 | 101319.778 | 97253.9374 | 716.93308 | 148.81376 | 1.606 |
| 34 | HP101 | BPM | 17.70433 | 101319.542 | 97254.0797 | 716.94079 | 148.81376 | 1.606 |
| 35 | H101DN | drift | 18.23766 | 101319.086 | 97254.3558 | 716.95575 | 148.81376 | 1.606 |
| 36 | PM101 | MUWIRE | 19.22982 | 101318.238 | 97254.8693 | 716.98357 | 148.81376 | 1.606 |
| 37 | DUP4 | drift | 20.04648 | 101317.539 | 97255.292 | 717.00644 | 148.81376 | 1.606 |
| 38 | IP101C | ionpump | 22.53299 | 101315.413 | 97256.5791 | 717.07612 | 148.81376 | 1.606 |
| 39 | RWMUPS | drift | 23.03299 | 101314.986 | 97256.8379 | 717.09013 | 148.81376 | 1.606 |
| 40 | RWCM01 | REWAMON | 23.50172 | 101314.585 | 97257.0805 | 717.10329 | 148.81376 | 1.606 |
| 41 | RWMDNS | drift | 24.09549 | 101314.077 | 97257.3879 | 717.11992 | 148.81376 | 1.606 |
| 42 | TOR1UP | DRIFT | 24.35933 | 101313.851 | 97257.5245 | 717.12731 | 148.81376 | 1.606 |
| 43 | TOR101 | TOROID | 24.57042 | 101313.671 | 97257.6337 | 717.13324 | 148.81376 | 1.606 |
| 44 | TOR1DN | DRIFT | 25.28919 | 101313.056 | 97258.0058 | 717.15339 | 148.81376 | 1.606 |
| 45 | MIC2UP | DRIFT | 25.35169 | 101313.003 | 97258.0381 | 717.15513 | 148.81376 | 1.606 |
| 46 | HT102 | MIHC | 25.69234 | 101312.711 | 97258.2144 | 717.16467 | 148.81376 | 1.606 |

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|----|--------|---------|-----------|------------|------------|-----------|-----------|----------|
| 47 | MICR_D | DRIFT | 26.69234 | 101311.856 | 97258.7321 | 717.19269 | 148.81376 | 1.606 |
| 48 | EPB_UP | DRIFT | 26.99443 | 101311.598 | 97258.8884 | 717.20116 | 148.81376 | 1.606 |
| 49 | HV01_1 | EPB | 27.5465 | 101311.126 | 97259.1742 | 717.21664 | 149.14292 | 1.606 |
| 50 | EPB_DN | DRIFT | 37.54655 | 101302.545 | 97264.3011 | 717.49689 | 149.47208 | 1.606 |
| 51 | EPB_UP | DRIFT | 37.99445 | 101302.159 | 97264.5286 | 717.50946 | 149.47208 | 1.606 |
| 52 | HV01_2 | EPB | 38.54654 | 101301.684 | 97264.8089 | 717.52494 | 149.80067 | 1.58451 |
| 53 | EPB_DN | DRIFT | 48.54656 | 101293.044 | 97269.8371 | 717.80142 | 150.12927 | 1.56303 |
| 54 | Q12_UP | DRIFT | 48.99449 | 101292.656 | 97270.0601 | 717.81362 | 150.12927 | 1.56303 |
| 55 | HQF102 | 3Q120/2 | 49.56742 | 101292.159 | 97270.3453 | 717.82927 | 150.12927 | 1.56303 |
| 56 | HQF102 | 3Q120/2 | 54.56741 | 101287.825 | 97272.8347 | 717.96562 | 150.12927 | 1.56303 |
| 57 | Q12_DN | DRIFT | 59.5674 | 101283.491 | 97275.324 | 718.10198 | 150.12927 | 1.56303 |
| 58 | BPM_UP | DRIFT | 59.99447 | 101283.121 | 97275.5366 | 718.11362 | 150.12927 | 1.56303 |
| 59 | HP102 | BPM | 60.26947 | 101282.883 | 97275.6735 | 718.12114 | 150.12927 | 1.56303 |
| 60 | BPM_DN | DRIFT | 60.8028 | 101282.42 | 97275.939 | 718.13567 | 150.12927 | 1.56303 |
| 61 | PUMP | PUMP | 60.91113 | 101282.326 | 97275.993 | 718.13862 | 150.12927 | 1.56303 |
| 62 | EPB_UP | DRIFT | 61.24446 | 101282.037 | 97276.1589 | 718.14771 | 150.12927 | 1.56303 |
| 63 | HV01_3 | EPB | 61.79656 | 101281.559 | 97276.4338 | 718.16277 | 150.42921 | 1.4281 |
| 64 | EPB_DN | DRIFT | 71.79658 | 101272.864 | 97281.3672 | 718.41195 | 150.72915 | 1.29317 |
| 65 | EPB_UP | DRIFT | 72.24451 | 101272.473 | 97281.5862 | 718.42205 | 150.72915 | 1.29317 |
| 66 | HV01_4 | EPB | 72.79657 | 101271.992 | 97281.856 | 718.43452 | 150.97008 | 1.06857 |
| 67 | EPB_DN | DRIFT | 82.79662 | 101263.25 | 97286.7078 | 718.62097 | 151.21101 | 0.84397 |
| 68 | EPB_UP | DRIFT | 83.24452 | 101262.857 | 97286.9235 | 718.62757 | 151.21101 | 0.84397 |
| 69 | HV01_5 | EPB | 83.79662 | 101262.374 | 97287.1894 | 718.6357 | 151.45996 | 0.62882 |
| 70 | EPB_DN | DRIFT | 93.79666 | 101253.589 | 97291.9668 | 718.74548 | 151.70891 | 0.41368 |
| 71 | MICR_U | DRIFT | 94.24456 | 101253.195 | 97292.1791 | 718.74869 | 151.70891 | 0.41368 |
| 72 | VT103 | MIHC-R | 94.73416 | 101252.764 | 97292.4111 | 718.75224 | 151.70891 | 0.41368 |
| 73 | MICR_D | DRIFT | 95.73416 | 101251.883 | 97292.8851 | 718.75945 | 151.70891 | 0.41368 |
| 74 | Q12_UP | DRIFT | 96.03623 | 101251.617 | 97293.0282 | 718.76165 | 151.70891 | 0.41368 |
| 75 | HQD103 | 3Q120/2 | 96.60916 | 101251.113 | 97293.2998 | 718.76579 | 151.70891 | 0.41368 |
| 76 | HQD103 | 3Q120/2 | 101.60915 | 101246.71 | 97295.6695 | 718.80188 | 151.70891 | 0.41368 |
| 77 | Q12_DN | DRIFT | 106.60914 | 101242.308 | 97298.0392 | 718.838 | 151.70891 | 0.41368 |
| 78 | BPM_UP | DRIFT | 107.0362 | 101241.931 | 97298.2416 | 718.84108 | 151.70891 | 0.41368 |
| 79 | VP103 | BPM | 107.3112 | 101241.689 | 97298.3719 | 718.84305 | 151.70891 | 0.41368 |
| 80 | BPM_DN | DRIFT | 107.84453 | 101241.22 | 97298.6247 | 718.84692 | 151.70891 | 0.41368 |
| 81 | PUMP | PUMP | 107.95287 | 101241.124 | 97298.676 | 718.84768 | 151.70891 | 0.41368 |
| 82 | EPB_UP | DRIFT | 108.2862 | 101240.831 | 97298.834 | 718.8501 | 151.70891 | 0.41368 |
| 83 | HV01_6 | EPB | 108.8383 | 101240.345 | 97299.0956 | 718.85407 | 151.95786 | 0.19853 |
| 84 | EPB_DN | DRIFT | 118.83831 | 101231.519 | 97303.7968 | 718.88875 | 152.20681 | -0.01662 |
| 85 | DRC0 | drift | 119.28624 | 101231.122 | 97304.0057 | 718.88862 | 152.20681 | -0.01662 |
| 86 | DRMTDX | drift | 121.70743 | 101228.981 | 97305.1346 | 718.88793 | 152.20681 | -0.01662 |
| 87 | BPM_UP | DRIFT | 132.30456 | 101219.606 | 97310.0759 | 718.88488 | 152.20681 | -0.01662 |
| 88 | HP104 | BPM | 132.57956 | 101219.363 | 97310.2041 | 718.88478 | 152.20681 | -0.01662 |
| 89 | BPM_DN | DRIFT | 133.11289 | 101218.891 | 97310.4528 | 718.88462 | 152.20681 | -0.01662 |
| 90 | Q12_UP | DRIFT | 133.22122 | 101218.795 | 97310.5033 | 718.88459 | 152.20681 | -0.01662 |
| 91 | HQF104 | 3Q60/2 | 133.79415 | 101218.288 | 97310.7704 | 718.88442 | 152.20681 | -0.01662 |
| 92 | HQF104 | 3Q60/2 | 136.29415 | 101216.077 | 97311.9361 | 718.8837 | 152.20681 | -0.01662 |
| 93 | Q12_DN | DRIFT | 138.79414 | 101213.865 | 97313.1018 | 718.88298 | 152.20681 | -0.01662 |
| 94 | DR104D | drift | 139.22121 | 101213.487 | 97313.301 | 718.88288 | 152.20681 | -0.01662 |
| 95 | SYTR_U | DRIFT | 140.91911 | 101211.985 | 97314.0927 | 718.88239 | 152.20681 | -0.01662 |

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| 96 | H104 | SYTRIM | 141.56494 | 101211.414 | 97314.3938 | 718.88219 | 152.20681 | -0.01662 |
| 97 | SYTR_D | DRIFT | 144.48163 | 101208.834 | 97315.7538 | 718.88134 | 152.20681 | -0.01662 |
| 98 | BPM_UP | DRIFT | 144.93997 | 101208.428 | 97315.9675 | 718.88121 | 152.20681 | -0.01662 |
| 99 | HP105 | BPM | 145.21497 | 101208.185 | 97316.0957 | 718.88114 | 152.20681 | -0.01662 |
| 100 | BPM_DN | DRIFT | 145.7483 | 101207.713 | 97316.3444 | 718.88098 | 152.20681 | -0.01662 |
| 101 | SFOUR_ | adapter | 145.85663 | 101207.617 | 97316.3949 | 718.88094 | 152.20681 | -0.01662 |
| 102 | PM105 | MUWIRE | 146.00246 | 101207.488 | 97316.4629 | 718.88091 | 152.20681 | -0.01662 |
| 103 | SFOUR_ | adapter | 147.33579 | 101206.309 | 97317.0846 | 718.88052 | 152.20681 | -0.01662 |
| 104 | Q12_UP | DRIFT | 147.48163 | 101206.18 | 97317.1526 | 718.88048 | 152.20681 | -0.01662 |
| 105 | HQF105 | 3Q120/2 | 148.05453 | 101205.673 | 97317.4198 | 718.88032 | 152.20681 | -0.01662 |
| 106 | HQF105 | 3Q120/2 | 153.05452 | 101201.25 | 97319.7512 | 718.87888 | 152.20681 | -0.01662 |
| 107 | Q12_DN | DRIFT | 158.05451 | 101196.827 | 97322.0826 | 718.87743 | 152.20681 | -0.01662 |
| 108 | MICR_U | DRIFT | 158.48161 | 101196.449 | 97322.2817 | 718.8773 | 152.20681 | -0.01662 |
| 109 | HT105 | MIHC | 158.97117 | 101196.016 | 97322.51 | 718.87717 | 152.20681 | -0.01662 |
| 110 | MICR_D | DRIFT | 159.97117 | 101195.131 | 97322.9763 | 718.87688 | 152.20681 | -0.01662 |
| 111 | DRMTU1 | drift | 160.27327 | 101194.864 | 97323.1171 | 718.87681 | 152.20681 | -0.01662 |
| 112 | DRMTD | drift | 182.05597 | 101175.594 | 97333.274 | 718.87051 | 152.20681 | -0.01662 |
| 113 | BPM_UP | DRIFT | 203.1114 | 101156.968 | 97343.0917 | 718.86444 | 152.20681 | -0.01662 |
| 114 | VP106 | BPM | 203.3864 | 101156.724 | 97343.22 | 718.86434 | 152.20681 | -0.01662 |
| 115 | BPM_DN | DRIFT | 203.91974 | 101156.253 | 97343.4687 | 718.86421 | 152.20681 | -0.01662 |
| 116 | Q12_UP | DRIFT | 204.02807 | 101156.157 | 97343.5192 | 718.86418 | 152.20681 | -0.01662 |
| 117 | HQD106 | 3Q120/2 | 204.60097 | 101155.65 | 97343.7863 | 718.86402 | 152.20681 | -0.01662 |
| 118 | HQD106 | 3Q120/2 | 209.60096 | 101151.227 | 97346.1177 | 718.86257 | 152.20681 | -0.01662 |
| 119 | Q12_DN | DRIFT | 214.60098 | 101146.804 | 97348.4491 | 718.86113 | 152.20681 | -0.01662 |
| 120 | MICR_U | DRIFT | 215.02805 | 101146.426 | 97348.6483 | 718.861 | 152.20681 | -0.01662 |
| 121 | VT106 | MIHC-R | 215.51761 | 101145.993 | 97348.8765 | 718.86087 | 152.20681 | -0.01662 |
| 122 | MICR_D | DRIFT | 216.51761 | 101145.108 | 97349.3428 | 718.86057 | 152.20681 | -0.01662 |
| 123 | DRMTU | drift | 216.81971 | 101144.841 | 97349.4837 | 718.86047 | 152.20681 | -0.01662 |
| 124 | DRMTD1 | drift | 237.27098 | 101126.749 | 97359.0197 | 718.8546 | 152.20681 | -0.01662 |
| 125 | BPM_UP | DRIFT | 258.03479 | 101108.38 | 97368.7015 | 718.8486 | 152.20681 | -0.01662 |
| 126 | HP107 | BPM | 258.30979 | 101108.137 | 97368.8297 | 718.84853 | 152.20681 | -0.01662 |
| 127 | BPM_DN | DRIFT | 258.84312 | 101107.665 | 97369.0784 | 718.84837 | 152.20681 | -0.01662 |
| 128 | SFOUR_ | adapter | 258.95145 | 101107.57 | 97369.1289 | 718.84833 | 152.20681 | -0.01662 |
| 129 | PM107 | MUWIRE | 259.09728 | 101107.441 | 97369.1969 | 718.8483 | 152.20681 | -0.01662 |
| 130 | SFOUR_ | adapter | 260.43061 | 101106.261 | 97369.8186 | 718.84791 | 152.20681 | -0.01662 |
| 131 | Q12_UP | DRIFT | 260.57645 | 101106.132 | 97369.8866 | 718.84787 | 152.20681 | -0.01662 |
| 132 | HQF107 | 3Q120/2 | 261.14935 | 101105.625 | 97370.1538 | 718.84771 | 152.20681 | -0.01662 |
| 133 | HQF107 | 3Q120/2 | 266.14934 | 101101.202 | 97372.4851 | 718.84627 | 152.20681 | -0.01662 |
| 134 | Q12_DN | DRIFT | 271.14933 | 101096.779 | 97374.8165 | 718.84482 | 152.20681 | -0.01662 |
| 135 | MICR_U | DRIFT | 271.57643 | 101096.401 | 97375.0157 | 718.84469 | 152.20681 | -0.01662 |
| 136 | HT107 | MIHC | 272.06599 | 101095.968 | 97375.244 | 718.84456 | 152.20681 | -0.01662 |
| 137 | MICR_D | DRIFT | 273.06599 | 101095.083 | 97375.7102 | 718.84426 | 152.20681 | -0.01662 |
| 138 | DRMTU2 | drift | 273.36809 | 101094.816 | 97375.8511 | 718.84417 | 152.20681 | -0.01662 |
| 139 | DRMTDM | drift | 294.35066 | 101076.254 | 97385.6349 | 718.83813 | 152.20681 | -0.01662 |
| 140 | MICR_U | DRIFT | 312.87441 | 101059.867 | 97394.2721 | 718.83278 | 152.20681 | -0.01662 |
| 141 | VT108 | MIHC-R | 313.36401 | 101059.434 | 97394.5004 | 718.83262 | 152.20681 | -0.01662 |
| 142 | MICR_D | DRIFT | 314.364 | 101058.55 | 97394.9667 | 718.83235 | 152.20681 | -0.01662 |
| 143 | BPM_UP | DRIFT | 314.66607 | 101058.282 | 97395.1076 | 718.83226 | 152.20681 | -0.01662 |
| 144 | VP108 | BPM | 314.94107 | 101058.039 | 97395.2358 | 718.83219 | 152.20681 | -0.01662 |

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| 145 | BPM_DN | DRIFT | 315.4744 | 101057.567 | 97395.4845 | 718.83203 | 152.20681 | -0.01662 |
| 146 | SFOUR_ | adapter | 315.58273 | 101057.471 | 97395.535 | 718.83199 | 152.20681 | -0.01662 |
| 147 | PM108 | MUWIRE | 315.72857 | 101057.342 | 97395.603 | 718.83196 | 152.20681 | -0.01662 |
| 148 | SFOUR_ | adapter | 317.0619 | 101056.163 | 97396.2247 | 718.83157 | 152.20681 | -0.01662 |
| 149 | Q12_UP | DRIFT | 317.20773 | 101056.034 | 97396.2927 | 718.83153 | 152.20681 | -0.01662 |
| 150 | HQD108 | 3Q120/2 | 317.78066 | 101055.527 | 97396.5598 | 718.83137 | 152.20681 | -0.01662 |
| 151 | HQD108 | 3Q120/2 | 322.78065 | 101051.104 | 97398.8912 | 718.82993 | 152.20681 | -0.01662 |
| 152 | Q12_DN | DRIFT | 327.78064 | 101046.681 | 97401.2227 | 718.82848 | 152.20681 | -0.01662 |
| 153 | SMIDGE | drift | 328.20771 | 101046.303 | 97401.4218 | 718.82835 | 152.20681 | -0.01662 |
| 154 | FOUR_6 | adapter | 329.34951 | 101045.293 | 97401.9542 | 718.82802 | 152.20681 | -0.01662 |
| 155 | B2_UPS | DRIFT | 329.51617 | 101045.145 | 97402.0319 | 718.82796 | 152.20681 | -0.01662 |
| 156 | V108_1 | B2 | 330.13074 | 101044.602 | 97402.3185 | 718.82779 | 152.20681 | -0.76089 |
| 157 | B2_DNS | DRIFT | 350.04792 | 101026.984 | 97411.6044 | 718.56326 | 152.20681 | -1.50516 |
| 158 | B2_UPS | DRIFT | 350.60002 | 101026.496 | 97411.8617 | 718.54876 | 152.20681 | -1.50516 |
| 159 | V108_2 | B2 | 351.21459 | 101025.953 | 97412.1482 | 718.53262 | 152.20681 | -2.24972 |
| 160 | B2_DNS | DRIFT | 371.13177 | 101008.347 | 97421.4278 | 717.75073 | 152.20681 | -2.99428 |
| 161 | FOUR_6 | adapter | 371.68387 | 101007.859 | 97421.6849 | 717.72189 | 152.20681 | -2.99428 |
| 162 | MICR_U | DRIFT | 371.85054 | 101007.712 | 97421.7624 | 717.71316 | 152.20681 | -2.99428 |
| 163 | HT109 | MIHC | 372.3401 | 101007.28 | 97421.9904 | 717.68761 | 152.20681 | -2.99428 |
| 164 | MICR_D | DRIFT | 373.3401 | 101006.396 | 97422.4561 | 717.63538 | 152.20681 | -2.99428 |
| 165 | Q12_UP | DRIFT | 373.6422 | 101006.129 | 97422.5967 | 717.61959 | 152.20681 | -2.99428 |
| 166 | HQF109 | 3Q120/2 | 374.2151 | 101005.623 | 97422.8635 | 717.58964 | 152.20681 | -2.99428 |
| 167 | HQF109 | 3Q120/2 | 379.21509 | 101001.206 | 97425.1917 | 717.32845 | 152.20681 | -2.99428 |
| 168 | Q12_DN | DRIFT | 384.21508 | 100996.789 | 97427.5199 | 717.06727 | 152.20681 | -2.99428 |
| 169 | H109UP | drift | 384.64218 | 100996.412 | 97427.7188 | 717.04496 | 152.20681 | -2.99428 |
| 170 | HP109 | BPM | 385.04375 | 100996.057 | 97427.9058 | 717.02399 | 152.20681 | -2.99428 |
| 171 | FOUR_6 | adapter | 385.57708 | 100995.586 | 97428.1541 | 716.99611 | 152.20681 | -2.99428 |
| 172 | V183UP | drift | 385.74375 | 100995.439 | 97428.2318 | 716.98741 | 152.20681 | -2.99428 |
| 173 | V108_3 | B2 | 386.34007 | 100994.912 | 97428.5094 | 716.95628 | 152.20681 | -3.73884 |
| 174 | B2_DNS | DRIFT | 406.25729 | 100977.33 | 97437.7764 | 715.65753 | 152.20681 | -4.48339 |
| 175 | B2_UPS | DRIFT | 406.80936 | 100976.843 | 97438.033 | 715.61435 | 152.20681 | -4.48339 |
| 176 | V108_4 | B2 | 407.42392 | 100976.301 | 97438.3187 | 715.56632 | 152.20681 | -5.22795 |
| 177 | B2_DNS | DRIFT | 427.34114 | 100958.756 | 97447.5669 | 713.75159 | 152.20681 | -5.97251 |
| 178 | FOUR_6 | adapter | 427.89321 | 100958.27 | 97447.8229 | 713.69414 | 152.20681 | -5.97251 |
| 179 | MICR_U | DRIFT | 428.05987 | 100958.123 | 97447.9002 | 713.67682 | 152.20681 | -5.97251 |
| 180 | VT110 | MIHC-R | 428.54947 | 100957.693 | 97448.1272 | 713.62587 | 152.20681 | -5.97251 |
| 181 | MICR_D | DRIFT | 429.54947 | 100956.813 | 97448.591 | 713.52183 | 152.20681 | -5.97251 |
| 182 | Q60_UP | DRIFT | 429.85154 | 100956.547 | 97448.7311 | 713.4904 | 152.20681 | -5.97251 |
| 183 | HQD110 | 3Q60/2 | 430.30987 | 100956.144 | 97448.9436 | 713.4427 | 152.20681 | -5.97251 |
| 184 | HQD110 | 3Q60/2 | 432.80986 | 100953.944 | 97450.103 | 713.1826 | 152.20681 | -5.97251 |
| 185 | Q60_DN | DRIFT | 435.30986 | 100951.744 | 97451.2624 | 712.92246 | 152.20681 | -5.97251 |
| 186 | V110UP | drift | 435.85152 | 100951.268 | 97451.5136 | 712.86609 | 152.20681 | -5.97251 |
| 187 | VP110 | BPM | 436.17961 | 100950.979 | 97451.6657 | 712.83197 | 152.20681 | -5.97251 |
| 188 | V110DN | drift | 436.71294 | 100950.51 | 97451.913 | 712.77646 | 152.20681 | -5.97251 |
| 189 | FOUR_6 | adapter | 436.76819 | 100950.461 | 97451.9387 | 712.77072 | 152.20681 | -5.97251 |
| 190 | B2_UPS | DRIFT | 436.93485 | 100950.315 | 97452.016 | 712.7534 | 152.20681 | -5.97251 |
| 191 | V108_5 | B2 | 437.54945 | 100949.774 | 97452.301 | 712.68945 | 152.20681 | -6.71678 |
| 192 | B2_DNS | DRIFT | 457.46664 | 100932.276 | 97461.524 | 710.35996 | 152.20681 | -7.46106 |
| 193 | B2_UPS | DRIFT | 458.0187 | 100931.792 | 97461.7792 | 710.28828 | 152.20681 | -7.46106 |

| | | | | | | | | |
|-----|--------|---------|-----------|------------|------------|-----------|-----------|----------|
| 194 | V108_6 | B2 | 458.6333 | 100931.253 | 97462.0633 | 710.20849 | 152.20681 | -8.20562 |
| 195 | B2_DNS | DRIFT | 478.55049 | 100913.814 | 97471.255 | 707.36584 | 152.20681 | -8.95017 |
| 196 | FOUR_6 | adapter | 479.10255 | 100913.332 | 97471.5093 | 707.27995 | 152.20681 | -8.95017 |
| 197 | DV1T0 | drift | 479.26922 | 100913.186 | 97471.5861 | 707.254 | 152.20681 | -8.95017 |
| 198 | P111UP | drift | 479.43756 | 100913.039 | 97471.6636 | 707.22782 | 152.20681 | -8.95017 |
| 199 | CT111T | CALTGT | 479.7246 | 100912.788 | 97471.7958 | 707.18317 | 152.20681 | -8.95017 |
| 200 | P111DN | drift | 481.05793 | 100911.623 | 97472.4099 | 706.97572 | 152.20681 | -8.95017 |
| 201 | DV2T0A | drift | 481.06255 | 100911.619 | 97472.4121 | 706.975 | 152.20681 | -8.95017 |
| 202 | STUB_E | POINT | 482.25412 | 100910.578 | 97472.9609 | 706.78963 | 152.20681 | -8.95017 |
| 203 | DV2T0B | drift | 482.25412 | 100910.578 | 97472.9609 | 706.78963 | 152.20681 | -8.95017 |
| 204 | MICR_U | DRIFT | 484.94988 | 100908.222 | 97474.2026 | 706.37024 | 152.20681 | -8.95017 |
| 205 | VT111 | MIH-OR | 485.43945 | 100907.794 | 97474.4281 | 706.29406 | 152.20681 | -8.95017 |
| 206 | MICR_D | DRIFT | 486.43945 | 100906.92 | 97474.8887 | 706.13848 | 152.20681 | -8.95017 |
| 207 | Q12_UP | DRIFT | 486.74155 | 100906.656 | 97475.0279 | 706.0915 | 152.20681 | -8.95017 |
| 208 | HQD111 | 3Q120/2 | 487.31445 | 100906.155 | 97475.2917 | 706.00236 | 152.20681 | -8.95017 |
| 209 | HQD111 | 3Q120/2 | 492.31444 | 100901.786 | 97477.5947 | 705.22451 | 152.20681 | -8.95017 |
| 210 | Q12_DN | DRIFT | 497.31443 | 100897.417 | 97479.8978 | 704.44662 | 152.20681 | -8.95017 |
| 211 | V111UP | drift | 497.74152 | 100897.044 | 97480.0945 | 704.38019 | 152.20681 | -8.95017 |
| 212 | VP111 | BPM | 498.15822 | 100896.68 | 97480.2864 | 704.31536 | 152.20681 | -8.95017 |
| 213 | DV2TA | drift | 498.69156 | 100896.213 | 97480.5321 | 704.23238 | 152.20681 | -8.95017 |
| 214 | MICR_U | DRIFT | 499.64241 | 100895.382 | 97480.97 | 704.08445 | 152.20681 | -8.95017 |
| 215 | HT112 | MIHC-O | 500.132 | 100894.955 | 97481.1956 | 704.00827 | 152.20681 | -8.95017 |
| 216 | MICR_D | DRIFT | 501.132 | 100894.081 | 97481.6562 | 703.85269 | 152.20681 | -8.95017 |
| 217 | Q12_UP | DRIFT | 501.43407 | 100893.817 | 97481.7953 | 703.80571 | 152.20681 | -8.95017 |
| 218 | HQF112 | 3Q120/2 | 502.007 | 100893.316 | 97482.0592 | 703.71657 | 152.20681 | -8.95017 |
| 219 | HQF112 | 3Q120/2 | 507.00699 | 100888.947 | 97484.3622 | 702.93869 | 152.20681 | -8.95017 |
| 220 | Q12_DN | DRIFT | 512.00698 | 100884.578 | 97486.6652 | 702.16083 | 152.20681 | -8.95017 |
| 221 | H112UP | drift | 512.43405 | 100884.204 | 97486.8619 | 702.0944 | 152.20681 | -8.95017 |
| 222 | HP112 | BPM | 512.87732 | 100883.817 | 97487.0661 | 702.02543 | 152.20681 | -8.95017 |
| 223 | PM112U | drift | 513.41069 | 100883.351 | 97487.3118 | 701.94243 | 152.20681 | -8.95017 |
| 224 | PM112 | MUWIRE | 513.53362 | 100883.243 | 97487.3684 | 701.9233 | 152.20681 | -8.95017 |
| 225 | C_P_MK | POINT | 514.51351 | 100882.387 | 97487.8197 | 701.77087 | 152.20681 | -8.95017 |
| 226 | PM112B | MUWIRE | 514.51351 | 100882.387 | 97487.8197 | 701.77087 | 152.20681 | -8.95017 |
| 227 | PM112D | drift | 514.86695 | 100882.078 | 97487.9825 | 701.71589 | 152.20681 | -8.95017 |
| 228 | DHALFX | drift | 514.97574 | 100881.983 | 97488.0326 | 701.69896 | 152.20681 | -8.95017 |
| 229 | DHALFX | drift | 524.51739 | 100873.645 | 97492.4275 | 700.21451 | 152.20681 | -8.95017 |
| 230 | DHALFX | drift | 535.64237 | 100863.923 | 97497.5517 | 698.48374 | 152.20681 | -8.95017 |
| 231 | DHALFX | drift | 546.76734 | 100854.202 | 97502.6759 | 696.75297 | 152.20681 | -8.95017 |
| 232 | DHALFX | drift | 557.89232 | 100844.48 | 97507.8002 | 695.0222 | 152.20681 | -8.95017 |
| 233 | DHALFX | drift | 569.0173 | 100834.758 | 97512.9244 | 693.29143 | 152.20681 | -8.95017 |
| 234 | DHALFX | drift | 580.14228 | 100825.036 | 97518.0486 | 691.56066 | 152.20681 | -8.95017 |
| 235 | DHALFX | drift | 591.26726 | 100815.315 | 97523.1728 | 689.82989 | 152.20681 | -8.95017 |
| 236 | DHALFX | drift | 602.39223 | 100805.593 | 97528.297 | 688.09912 | 152.20681 | -8.95017 |
| 237 | DHALFX | drift | 613.51721 | 100795.871 | 97533.4212 | 686.36835 | 152.20681 | -8.95017 |
| 238 | DHALFX | drift | 624.64219 | 100786.15 | 97538.5454 | 684.63757 | 152.20681 | -8.95017 |
| 239 | DHALFX | drift | 635.76717 | 100776.428 | 97543.6696 | 682.9068 | 152.20681 | -8.95017 |
| 240 | DHALFX | drift | 646.89214 | 100766.706 | 97548.7938 | 681.17603 | 152.20681 | -8.95017 |
| 241 | DHALFX | drift | 658.01712 | 100756.984 | 97553.918 | 679.44526 | 152.20681 | -8.95017 |
| 242 | DHALFX | drift | 669.1421 | 100747.263 | 97559.0422 | 677.71449 | 152.20681 | -8.95017 |

RCP
START

| | | | | | | | | |
|-----|--------|---------|-----------|------------|------------|-----------|-----------|----------|
| 243 | DHALFX | drift | 680.26708 | 100737.541 | 97564.1664 | 675.98372 | 152.20681 | -8.95017 |
| 244 | DHALFX | drift | 691.39206 | 100727.819 | 97569.2906 | 674.25295 | 152.20681 | -8.95017 |
| 245 | DHALFX | drift | 702.51703 | 100718.097 | 97574.4148 | 672.52218 | 152.20681 | -8.95017 |
| 246 | DHALFX | drift | 713.64201 | 100708.376 | 97579.539 | 670.79141 | 152.20681 | -8.95017 |
| 247 | DHALFX | drift | 724.76699 | 100698.654 | 97584.6632 | 669.06064 | 152.20681 | -8.95017 |
| 248 | BPM_UP | DRIFT | 736.01693 | 100688.823 | 97589.845 | 667.31041 | 152.20681 | -8.95017 |
| 249 | VP113 | BPM | 736.29193 | 100688.583 | 97589.9717 | 667.26763 | 152.20681 | -8.95017 |
| 250 | BPM_DN | DRIFT | 736.82527 | 100688.117 | 97590.2173 | 667.18466 | 152.20681 | -8.95017 |
| 251 | Q12_UP | DRIFT | 736.9336 | 100688.022 | 97590.2672 | 667.16779 | 152.20681 | -8.95017 |
| 252 | HQD113 | 3Q120/2 | 737.50653 | 100687.521 | 97590.5311 | 667.07869 | 152.20681 | -8.95017 |
| 253 | HQD113 | 3Q120/2 | 742.50652 | 100683.152 | 97592.8341 | 666.3008 | 152.20681 | -8.95017 |
| 254 | Q12_DN | DRIFT | 747.50651 | 100678.783 | 97595.1371 | 665.52291 | 152.20681 | -8.95017 |
| 255 | MICR_U | DRIFT | 747.93358 | 100678.409 | 97595.3338 | 665.45648 | 152.20681 | -8.95017 |
| 256 | VT114 | MIH_OR | 748.42318 | 100677.982 | 97595.5593 | 665.3803 | 152.20681 | -8.95017 |
| 257 | MICR_D | DRIFT | 749.42317 | 100677.108 | 97596.0199 | 665.22475 | 152.20681 | -8.95017 |
| 258 | DV2T13 | drift | 749.72524 | 100676.844 | 97596.1591 | 665.17774 | 152.20681 | -8.95017 |
| 259 | MICR_U | DRIFT | 749.83495 | 100676.748 | 97596.2096 | 665.16068 | 152.20681 | -8.95017 |
| 260 | HT114 | MIHC_O | 750.32452 | 100676.32 | 97596.4351 | 665.0845 | 152.20681 | -8.95017 |
| 261 | MICR_D | DRIFT | 751.32451 | 100675.446 | 97596.8957 | 664.92892 | 152.20681 | -8.95017 |
| 262 | Q12_UP | DRIFT | 751.62661 | 100675.182 | 97597.0349 | 664.88194 | 152.20681 | -8.95017 |
| 263 | HQF114 | 3Q120/2 | 752.19951 | 100674.682 | 97597.2987 | 664.7928 | 152.20681 | -8.95017 |
| 264 | HQF114 | 3Q120/2 | 757.1995 | 100670.312 | 97599.6018 | 664.01494 | 152.20681 | -8.95017 |
| 265 | Q12_DN | DRIFT | 762.19949 | 100665.943 | 97601.9048 | 663.23706 | 152.20681 | -8.95017 |
| 266 | BPM_UP | DRIFT | 762.62659 | 100665.57 | 97602.1015 | 663.17062 | 152.20681 | -8.95017 |
| 267 | HP114 | BPM | 762.90159 | 100665.329 | 97602.2282 | 663.12784 | 152.20681 | -8.95017 |
| 268 | BPM_DN | DRIFT | 763.43492 | 100664.863 | 97602.4738 | 663.04487 | 152.20681 | -8.95017 |
| 269 | SFOUR_ | adapter | 763.54326 | 100664.769 | 97602.5237 | 663.028 | 152.20681 | -8.95017 |
| 270 | PM114 | MUWIRE | 763.68909 | 100664.641 | 97602.5909 | 663.0053 | 152.20681 | -8.95017 |
| 271 | V14_UP | drift | 765.02242 | 100663.476 | 97603.205 | 662.79789 | 152.20681 | -8.95017 |
| 272 | IP114A | ionpump | 765.54571 | 100663.019 | 97603.446 | 662.71646 | 152.20681 | -8.95017 |
| 273 | P114SE | drift | 766.04571 | 100662.582 | 97603.6764 | 662.63867 | 152.20681 | -8.95017 |
| 274 | IP114B | ionpump | 780.52485 | 100649.929 | 97610.3455 | 660.38608 | 152.20681 | -8.95017 |
| 275 | P114SE | drift | 781.02485 | 100649.492 | 97610.5758 | 660.30829 | 152.20681 | -8.95017 |
| 276 | IP114C | ionpump | 795.50402 | 100636.839 | 97617.245 | 658.0557 | 152.20681 | -8.95017 |
| 277 | P114SE | drift | 796.00402 | 100636.402 | 97617.4753 | 657.97792 | 152.20681 | -8.95017 |
| 278 | IP114D | ionpump | 810.48319 | 100623.75 | 97624.1444 | 655.7253 | 152.20681 | -8.95017 |
| 279 | | drift | 810.98319 | 100623.313 | 97624.2747 | 655.64751 | 152.20681 | -8.95017 |
| 280 | BPM_UP | DRIFT | 811.50648 | 100622.855 | 97624.6157 | 655.56611 | 152.20681 | -8.95017 |
| 281 | HP115 | BPM | 811.78148 | 100622.615 | 97624.7424 | 655.52333 | 152.20681 | -8.95017 |
| 282 | BPM_DN | DRIFT | 812.31481 | 100622.149 | 97624.9881 | 655.44036 | 152.20681 | -8.95017 |
| 283 | SFOUR_ | adapter | 812.42315 | 100622.054 | 97625.038 | 655.42349 | 152.20681 | -8.95017 |
| 284 | PM115 | MUWIRE | 812.56898 | 100621.927 | 97625.1051 | 655.40082 | 152.20681 | -8.95017 |
| 285 | SFOUR_ | adapter | 813.90231 | 100620.762 | 97625.7193 | 655.19337 | 152.20681 | -8.95017 |
| 286 | Q60_UP | DRIFT | 814.04814 | 100620.634 | 97625.7864 | 655.1707 | 152.20681 | -8.95017 |
| 287 | HQF115 | 3Q60/2 | 814.50647 | 100620.234 | 97625.9976 | 655.09938 | 152.20681 | -8.95017 |
| 288 | HQF115 | 3Q60/2 | 817.00647 | 100618.049 | 97627.1491 | 654.71044 | 152.20681 | -8.95017 |
| 289 | Q60_DN | DRIFT | 819.50646 | 100615.864 | 97628.3006 | 654.32149 | 152.20681 | -8.95017 |
| 290 | MICR_U | DRIFT | 820.04813 | 100615.391 | 97628.5501 | 654.23724 | 152.20681 | -8.95017 |
| 291 | HT115 | MIHC | 820.5377 | 100614.963 | 97628.7756 | 654.16106 | 152.20681 | -8.95017 |

D & B CT
START

| | | | | | | | | |
|-----|---------|---------|-----------|------------|------------|-----------|-----------|----------|
| 292 | MICR_D | DRIFT | 821.53769 | 100614.089 | 97629.2362 | 654.00548 | 152.20681 | -8.95017 |
| 293 | V15_UP | drift | 821.83979 | 100613.825 | 97629.3753 | 653.9585 | 152.20681 | -8.95017 |
| 294 | IP115A | ionpump | 822.10666 | 100613.592 | 97629.4982 | 653.91697 | 152.20681 | -8.95017 |
| 295 | P115SE | drift | 822.60666 | 100613.155 | 97629.7285 | 653.83921 | 152.20681 | -8.95017 |
| 296 | MVA15A | valve | 839.78917 | 100598.14 | 97637.6429 | 651.16602 | 152.20681 | -8.95017 |
| 297 | MVA15B | valve | 840.28917 | 100597.703 | 97637.8732 | 651.08823 | 152.20681 | -8.95017 |
| 298 | PG115 | gauge | 840.78916 | 100597.266 | 97638.1034 | 651.01044 | 152.20681 | -8.95017 |
| 299 | IP115B | ionpump | 841.28916 | 100596.829 | 97638.3338 | 650.93265 | 152.20681 | -8.95017 |
| 300 | V15_DN | drift | 841.78916 | 100596.392 | 97638.564 | 650.85487 | 152.20681 | -8.95017 |
| 301 | BPM_UP | DRIFT | 842.05603 | 100596.159 | 97638.687 | 650.81336 | 152.20681 | -8.95017 |
| 302 | VP116 | BPM | 842.33103 | 100595.919 | 97638.8137 | 650.77058 | 152.20681 | -8.95017 |
| 303 | BPM_DN | DRIFT | 842.86436 | 100595.453 | 97639.0593 | 650.68761 | 152.20681 | -8.95017 |
| 304 | Q12_UP | DRIFT | 842.97269 | 100595.358 | 97639.1092 | 650.67075 | 152.20681 | -8.95017 |
| 305 | HQD116 | 3Q120/2 | 843.54559 | 100594.857 | 97639.3731 | 650.58161 | 152.20681 | -8.95017 |
| 306 | HQD116 | 3Q120/2 | 848.54558 | 100590.488 | 97641.6761 | 649.80375 | 152.20681 | -8.95017 |
| 307 | Q12_DN | DRIFT | 853.54557 | 100586.119 | 97643.9791 | 649.02587 | 152.20681 | -8.95017 |
| 308 | MICR_U | DRIFT | 853.97267 | 100585.746 | 97644.1758 | 648.95943 | 152.20681 | -8.95017 |
| 309 | VT116 | MIHC-R | 854.46223 | 100585.318 | 97644.4013 | 648.88325 | 152.20681 | -8.95017 |
| 310 | MICR_D | DRIFT | 855.46223 | 100584.444 | 97644.8619 | 648.72767 | 152.20681 | -8.95017 |
| 311 | V16_UP | drift | 855.76433 | 100584.18 | 97645.0011 | 648.68069 | 152.20681 | -8.95017 |
| 312 | IP116A | ionpump | 856.04655 | 100583.933 | 97645.1311 | 648.63676 | 152.20681 | -8.95017 |
| 313 | P116SE | drift | 856.54655 | 100583.496 | 97645.3614 | 648.55897 | 152.20681 | -8.95017 |
| 314 | IP116B | ionpump | 872.04655 | 100569.951 | 97652.5007 | 646.14756 | 152.20681 | -8.95017 |
| 315 | P116SE | drift | 872.54655 | 100569.515 | 97652.731 | 646.06977 | 152.20681 | -8.95017 |
| 316 | IP116C | ionpump | 888.04655 | 100555.97 | 97659.8704 | 643.65836 | 152.20681 | -8.95017 |
| 317 | P116SE | drift | 888.54655 | 100555.533 | 97660.1007 | 643.58057 | 152.20681 | -8.95017 |
| 318 | IP116D | ionpump | 904.04655 | 100541.988 | 97667.24 | 641.16916 | 152.20681 | -8.95017 |
| 319 | P116SE | drift | 904.54655 | 100541.551 | 97667.4704 | 641.09137 | 152.20681 | -8.95017 |
| 320 | IP116E | ionpump | 920.04655 | 100528.006 | 97674.6097 | 638.67996 | 152.20681 | -8.95017 |
| 321 | V16_DN | drift | 920.54655 | 100527.569 | 97674.84 | 638.60217 | 152.20681 | -8.95017 |
| 322 | BPM_UP | DRIFT | 920.82877 | 100527.322 | 97674.97 | 638.55827 | 152.20681 | -8.95017 |
| 323 | HP117 | BPM | 921.10377 | 100527.082 | 97675.0966 | 638.51549 | 152.20681 | -8.95017 |
| 324 | BPM_DN | DRIFT | 921.6371 | 100526.616 | 97675.3423 | 638.43252 | 152.20681 | -8.95017 |
| 325 | SFOUR_- | adapter | 921.74543 | 100526.521 | 97675.3922 | 638.41565 | 152.20681 | -8.95017 |
| 326 | PM117 | MUWIRE | 921.89127 | 100526.394 | 97675.4594 | 638.39295 | 152.20681 | -8.95017 |
| 327 | SFOUR_- | adapter | 923.2246 | 100525.229 | 97676.0735 | 638.18553 | 152.20681 | -8.95017 |
| 328 | Q12_UP | DRIFT | 923.37043 | 100525.101 | 97676.1407 | 638.16283 | 152.20681 | -8.95017 |
| 329 | HQF117 | 3Q120/2 | 923.94336 | 100524.601 | 97676.4046 | 638.07372 | 152.20681 | -8.95017 |
| 330 | HQF117 | 3Q120/2 | 928.94335 | 100520.231 | 97678.7076 | 637.29584 | 152.20681 | -8.95017 |
| 331 | Q12_DN | DRIFT | 933.94334 | 100515.862 | 97681.0106 | 636.51795 | 152.20681 | -8.95017 |
| 332 | MICR_U | DRIFT | 934.37041 | 100515.489 | 97681.2073 | 636.45152 | 152.20681 | -8.95017 |
| 333 | HT117 | MIHC | 934.86001 | 100515.061 | 97681.4328 | 636.37533 | 152.20681 | -8.95017 |
| 334 | MICR_D | DRIFT | 935.86 | 100514.187 | 97681.8934 | 636.21979 | 152.20681 | -8.95017 |
| 335 | D2MMI | drift | 936.16207 | 100513.923 | 97682.0326 | 636.17278 | 152.20681 | -8.95017 |
| 336 | SYTR_U | DRIFT | 937.95846 | 100512.353 | 97682.86 | 635.89331 | 152.20681 | -8.95017 |
| 337 | H117 | SYTRIM | 938.60429 | 100511.789 | 97683.1575 | 635.79282 | 152.19507 | -8.95017 |
| 338 | SYTR_D | DRIFT | 941.52095 | 100509.24 | 97684.5014 | 635.33908 | 152.18332 | -8.95017 |
| 339 | V17_UP | drift | 941.97928 | 100508.84 | 97684.7127 | 635.26776 | 152.18332 | -8.95017 |
| 340 | IP117 | ionpump | 942.23233 | 100508.619 | 97684.8293 | 635.22839 | 152.18332 | -8.95017 |

| | | | | | | | | |
|-----|--------|---------|------------|------------|------------|-----------|-----------|----------|
| 341 | P117SE | drift | 942.73233 | 100508.182 | 97685.0598 | 635.1506 | 152.18332 | -8.95017 |
| 342 | V17_DN | drift | 943.30566 | 100507.681 | 97685.3241 | 635.06143 | 152.18332 | -8.95017 |
| 343 | BPM_UP | DRIFT | 943.55868 | 100507.46 | 97685.4407 | 635.02206 | 152.18332 | -8.95017 |
| 344 | VP118 | BPM | 943.83368 | 100507.22 | 97685.5675 | 634.97927 | 152.18332 | -8.95017 |
| 345 | BPM_DN | DRIFT | 944.36701 | 100506.754 | 97685.8133 | 634.8963 | 152.18332 | -8.95017 |
| 346 | Q12_UP | DRIFT | 944.47537 | 100506.659 | 97685.8633 | 634.87944 | 152.18332 | -8.95017 |
| 347 | HQD118 | 3Q120/2 | 945.04827 | 100506.159 | 97686.1274 | 634.7903 | 152.18332 | -8.95017 |
| 348 | HQD118 | 3Q120/2 | 950.04826 | 100501.79 | 97688.4322 | 634.01245 | 152.18332 | -8.95017 |
| 349 | Q12_DN | DRIFT | 955.04825 | 100497.422 | 97690.737 | 633.23456 | 152.18332 | -8.95017 |
| 350 | MICR_U | DRIFT | 955.47535 | 100497.049 | 97690.9339 | 633.16812 | 152.18332 | -8.95017 |
| 351 | VT118 | MIHC_R | 955.96492 | 100496.621 | 97691.1595 | 633.09194 | 152.18332 | -8.95017 |
| 352 | MICR_D | DRIFT | 956.96492 | 100495.747 | 97691.6205 | 632.93637 | 152.18332 | -8.95017 |
| 353 | SFOUR_ | adapter | 957.26702 | 100495.483 | 97691.7597 | 632.88938 | 152.18332 | -8.95017 |
| 354 | CT118T | CALTGT | 957.41285 | 100495.356 | 97691.827 | 632.86668 | 152.18332 | -8.95017 |
| 355 | V18_UP | drift | 958.74618 | 100494.191 | 97692.4416 | 632.65927 | 152.18332 | -8.95017 |
| 356 | IP118A | ionpump | 959.03909 | 100493.935 | 97692.5766 | 632.6137 | 152.18332 | -8.95017 |
| 357 | P118SE | drift | 959.53909 | 100493.498 | 97692.8071 | 632.53591 | 152.18332 | -8.95017 |
| 358 | IP118B | ionpump | 975.04241 | 100479.954 | 97699.9536 | 630.12397 | 152.18332 | -8.95017 |
| 359 | V18_DN | drift | 975.54241 | 100479.517 | 97700.184 | 630.04618 | 152.18332 | -8.95017 |
| 360 | FOUR_6 | adapter | 975.83532 | 100479.261 | 97700.3191 | 630.00061 | 152.18332 | -8.95017 |
| 361 | B2_UPS | DRIFT | 976.00198 | 100479.115 | 97700.3959 | 629.97466 | 152.18332 | -8.95017 |
| 362 | V118_1 | B2 | 976.61658 | 100478.578 | 97700.6792 | 629.87906 | 152.18332 | -8.24945 |
| 363 | B2_DNS | DRIFT | 996.5337 | 100461.145 | 97709.877 | 627.02142 | 152.18332 | -7.54872 |
| 364 | B2_UPS | DRIFT | 997.0858 | 100460.661 | 97710.1324 | 626.94888 | 152.18332 | -7.54872 |
| 365 | V118_2 | B2 | 997.70037 | 100460.122 | 97710.4167 | 626.86814 | 152.18332 | -6.84771 |
| 366 | B2_DNS | DRIFT | 1017.61749 | 100442.633 | 97719.6444 | 624.4935 | 152.18332 | -6.14669 |
| 367 | FOUR_6 | adapter | 1018.16958 | 100442.147 | 97719.9006 | 624.43438 | 152.18332 | -6.14669 |
| 368 | MICR_U | DRIFT | 1018.33625 | 100442.001 | 97719.9779 | 624.41653 | 152.18332 | -6.14669 |
| 369 | HT119 | MIHC | 1018.82582 | 100441.57 | 97720.2051 | 624.36411 | 152.18332 | -6.14669 |
| 370 | MICR_D | DRIFT | 1019.82581 | 100440.691 | 97720.669 | 624.25702 | 152.18332 | -6.14669 |
| 371 | Q60_UP | DRIFT | 1020.12791 | 100440.425 | 97720.8092 | 624.22467 | 152.18332 | -6.14669 |
| 372 | HQF119 | 3Q60/2 | 1020.58625 | 100440.022 | 97721.0218 | 624.17559 | 152.18332 | -6.14669 |
| 373 | HQF119 | 3Q60/2 | 1023.08624 | 100437.824 | 97722.1817 | 623.90791 | 152.18332 | -6.14669 |
| 374 | Q60_DN | DRIFT | 1025.58624 | 100435.626 | 97723.3416 | 623.64022 | 152.18332 | -6.14669 |
| 375 | BPM_UP | DRIFT | 1026.1279 | 100435.149 | 97723.5929 | 623.58222 | 152.18332 | -6.14669 |
| 376 | HP119 | BPM | 1026.4029 | 100434.907 | 97723.7205 | 623.55279 | 152.18332 | -6.14669 |
| 377 | BPM_DN | DRIFT | 1026.93623 | 100434.438 | 97723.968 | 623.49567 | 152.18332 | -6.14669 |
| 378 | FOUR_6 | adapter | 1027.04457 | 100434.343 | 97724.0182 | 623.48405 | 152.18332 | -6.14669 |
| 379 | B2_UPS | DRIFT | 1027.21123 | 100434.197 | 97724.0956 | 623.46621 | 152.18332 | -6.14669 |
| 380 | V118_3 | B2 | 1027.8258 | 100433.656 | 97724.3807 | 623.40043 | 152.18332 | -5.44596 |
| 381 | B2_DNS | DRIFT | 1047.74292 | 100416.121 | 97733.6328 | 621.51017 | 152.18332 | -4.74524 |
| 382 | B2_UPS | DRIFT | 1048.29502 | 100415.634 | 97733.8895 | 621.46451 | 152.18332 | -4.74524 |
| 383 | V118_4 | B2 | 1048.90958 | 100415.092 | 97734.1753 | 621.41365 | 152.18332 | -4.04422 |
| 384 | B2_DNS | DRIFT | 1068.82673 | 100397.521 | 97743.4462 | 620.009 | 152.18332 | -3.34321 |
| 385 | FOUR_6 | adapter | 1069.3788 | 100397.033 | 97743.7033 | 619.97678 | 152.18332 | -3.34321 |
| 386 | Q12_UP | DRIFT | 1069.54547 | 100396.886 | 97743.781 | 619.96707 | 152.18332 | -3.34321 |
| 387 | HQD120 | 3Q120/2 | 1070.1184 | 100396.38 | 97744.0479 | 619.93364 | 152.18332 | -3.34321 |
| 388 | HQD120 | 3Q120/2 | 1075.11839 | 100391.966 | 97746.3771 | 619.64203 | 152.18332 | -3.34321 |
| 389 | Q12_DN | DRIFT | 1080.11838 | 100387.551 | 97748.7064 | 619.35043 | 152.18332 | -3.34321 |

PRE-TABLET
START

| | | | | | | | | |
|-----|--------|---------|------------|------------|------------|-----------|-----------|----------|
| 390 | DRV3TB | drift | 1080.54544 | 100387.174 | 97748.9053 | 619.32553 | 152.18332 | -3.34321 |
| 391 | Q12_UP | DRIFT | 1080.95532 | 100386.812 | 97749.0963 | 619.30162 | 152.18332 | -3.34321 |
| 392 | HQF121 | 3Q120/2 | 1081.52822 | 100386.306 | 97749.3631 | 619.26822 | 152.18332 | -3.34321 |
| 393 | HQF121 | 3Q120/2 | 1086.52821 | 100381.892 | 97751.6924 | 618.97662 | 152.18332 | -3.34321 |
| 394 | Q12_DN | DRIFT | 1091.5282 | 100377.477 | 97754.0217 | 618.68498 | 152.18332 | -3.34321 |
| 395 | MICR_U | DRIFT | 1091.9553 | 100377.1 | 97754.2206 | 618.66008 | 152.18332 | -3.34321 |
| 396 | HT121 | MIHC | 1092.44486 | 100376.668 | 97754.4487 | 618.63154 | 152.18332 | -3.34321 |
| 397 | MICR_D | DRIFT | 1093.44486 | 100375.785 | 97754.9145 | 618.57321 | 152.18332 | -3.34321 |
| 398 | MICR_U | DRIFT | 1093.74696 | 100375.518 | 97755.0552 | 618.55559 | 152.18332 | -3.34321 |
| 399 | VT121 | MIHC-R | 1094.23653 | 100375.086 | 97755.2833 | 618.52704 | 152.18332 | -3.34321 |
| 400 | MICR_D | DRIFT | 1095.23652 | 100374.203 | 97755.7492 | 618.46871 | 152.18332 | -3.34321 |
| 401 | BPM_UP | DRIFT | 1095.53862 | 100373.936 | 97755.8899 | 618.45109 | 152.18332 | -3.34321 |
| 402 | HP121 | SMABPM | 1095.81362 | 100373.693 | 97756.018 | 618.43505 | 152.18332 | -3.34321 |
| 403 | BPM_DN | DRIFT | 1096.34695 | 100373.222 | 97756.2665 | 618.40395 | 152.18332 | -3.34321 |
| 404 | BPM_UP | DRIFT | 1096.45529 | 100373.127 | 97756.3169 | 618.39765 | 152.18332 | -3.34321 |
| 405 | VP121 | SMABPM | 1096.73029 | 100372.884 | 97756.445 | 618.3816 | 152.18332 | -3.34321 |
| 406 | BPM_DN | DRIFT | 1097.26362 | 100372.413 | 97756.6935 | 618.3505 | 152.18332 | -3.34321 |
| 407 | SFOUR_ | adapter | 1097.37195 | 100372.317 | 97756.744 | 618.34417 | 152.18332 | -3.34321 |
| 408 | PM121 | TARGMW | 1097.51779 | 100372.188 | 97756.8119 | 618.33567 | 152.18332 | -3.34321 |
| 409 | V21_UP | drift | 1098.85112 | 100371.011 | 97757.433 | 618.25792 | 152.18332 | -3.34321 |
| 410 | IP121A | ionpump | 1099.14639 | 100370.751 | 97757.5706 | 618.24069 | 152.18332 | -3.34321 |
| 411 | PG121 | gauge | 1099.64639 | 100370.309 | 97757.8035 | 618.21153 | 152.18332 | -3.34321 |
| 412 | MAVL21 | valve | 1100.14639 | 100369.868 | 97758.0364 | 618.18236 | 152.18332 | -3.34321 |
| 413 | P121SE | drift | 1100.64639 | 100369.426 | 97758.2694 | 618.15319 | 152.18332 | -3.34321 |
| 414 | IP121B | ionpump | 1116.48212 | 100355.444 | 97765.6465 | 617.22964 | 152.18332 | -3.34321 |
| 415 | P121SE | drift | 1116.98212 | 100355.003 | 97765.8794 | 617.20047 | 152.18332 | -3.34321 |
| 416 | IP121C | ionpump | 1132.81788 | 100341.021 | 97773.2565 | 616.27692 | 152.18332 | -3.34321 |
| 417 | V21_DN | drift | 1133.31788 | 100340.579 | 97773.4894 | 616.24775 | 152.18332 | -3.34321 |
| 418 | TOR_UP | DRIFT | 1133.61315 | 100340.318 | 97773.627 | 616.23053 | 152.18332 | -3.34321 |
| 419 | TORTGT | TOROID | 1133.94649 | 100340.024 | 97773.7822 | 616.21107 | 152.18332 | -3.34321 |
| 420 | TOR_DN | DRIFT | 1134.23815 | 100339.767 | 97773.9181 | 616.19408 | 152.18332 | -3.34321 |
| 421 | BPM_UP | DRIFT | 1134.61315 | 100339.435 | 97774.0928 | 616.17219 | 152.18332 | -3.34321 |
| 422 | HPTGT | SMABPM | 1134.88815 | 100339.193 | 97774.2209 | 616.15615 | 152.18332 | -3.34321 |
| 423 | BPM_DN | DRIFT | 1135.42148 | 100338.722 | 97774.4694 | 616.12505 | 152.18332 | -3.34321 |
| 424 | BPM_UP | DRIFT | 1135.52982 | 100338.626 | 97774.5198 | 616.11875 | 152.18332 | -3.34321 |
| 425 | VPTGT | SMABPM | 1135.80481 | 100338.383 | 97774.6479 | 616.1027 | 152.18332 | -3.34321 |
| 426 | BPM_DN | DRIFT | 1136.33815 | 100337.912 | 97774.8964 | 616.0716 | 152.18332 | -3.34321 |
| 427 | PMTGT | TARGMW | 1136.44648 | 100337.817 | 97774.9469 | 616.06527 | 152.18332 | -3.34321 |
| 428 | OT_UPS | drift | 1137.77981 | 100336.64 | 97775.568 | 615.98751 | 152.18332 | -3.34321 |
| 429 | OTRTGT | otrmom | 1138.23814 | 100336.235 | 97775.7815 | 615.96078 | 152.18332 | -3.34321 |
| 430 | OT_DNS | drift | 1139.86314 | 100334.8 | 97776.5385 | 615.86603 | 152.18332 | -3.34321 |
| 431 | OUCADR | drift | 1140.20828 | 100334.495 | 97776.6993 | 615.84588 | 152.18332 | -3.34321 |
| 432 | SH_WAL | drift | 1141.20828 | 100333.612 | 97777.1651 | 615.78755 | 152.18332 | -3.34321 |
| 433 | M_TACA | POINT | 1147.20827 | 100328.315 | 97779.9603 | 615.43765 | 152.18332 | -3.34321 |
| 434 | INCADR | drift | 1147.20827 | 100328.315 | 97779.9603 | 615.43765 | 152.18332 | -3.34321 |
| 435 | BAFL2P | BAFFLE | 1160.89253 | 100316.232 | 97786.3351 | 614.63955 | 152.18332 | -3.34321 |
| 436 | TA_OFF | drift | 1165.81378 | 100311.887 | 97788.6276 | 614.35251 | 152.18332 | -3.34321 |
| 437 | TA_UPS | drift | 1167.25383 | 100310.616 | 97789.2985 | 614.26852 | 152.18332 | -3.34321 |
| 438 | HALTA1 | TAR/2 | 1168.04451 | 100309.918 | 97789.6668 | 614.22243 | 152.18332 | -3.34321 |

BRANCH
OF N2
LINE
TO THSA
MERTADICAN

| | | | | | | | | |
|-----|--------|---------|------------|------------|------------|-----------|-----------|----------|
| 439 | MCZERO | point | 1169.19281 | 100308.904 | 97790.2018 | 614.15546 | 152.18332 | -3.34321 |
| 440 | ACTRN1 | horn1 | 1169.29123 | 100308.817 | 97790.2476 | 614.14972 | 152.18332 | -3.34321 |
| 441 | HALTA2 | TAR/2 | 1169.60914 | 100308.536 | 97790.3957 | 614.13119 | 152.18332 | -3.34321 |
| 442 | ENDFIN | fin | 1171.17377 | 100307.155 | 97791.1246 | 614.03991 | 152.18332 | -3.34321 |
| 443 | DWNRN1 | horn_dn | 1179.03531 | 100300.213 | 97794.7869 | 613.58142 | 152.18332 | -3.34321 |
| 444 | D2LOWE | drift | 1181.72283 | 100297.841 | 97796.0389 | 613.42469 | 152.18332 | -3.34321 |
| 445 | UPHRN2 | horn_up | 1201.82168 | 100280.094 | 97805.4019 | 612.25248 | 152.18332 | -3.34321 |
| 446 | ACTRN2 | horn2 | 1202.00114 | 100279.936 | 97805.4856 | 612.24202 | 152.18332 | -3.34321 |
| 447 | DWNRN2 | horn_dn | 1211.84364 | 100271.246 | 97810.0707 | 611.66797 | 152.18332 | -3.34321 |
| 448 | D2MEDE | drift | 1217.18812 | 100266.527 | 97812.5604 | 611.35629 | 152.18332 | -3.34321 |
| 449 | UPHRN2 | horn_up | 1244.47251 | 100242.436 | 97825.2709 | 609.76502 | 152.18332 | -3.34321 |
| 450 | ACTRN2 | horn2 | 1244.65197 | 100242.278 | 97825.3545 | 609.75455 | 152.18332 | -3.34321 |
| 451 | DWNRN2 | horn_dn | 1254.49447 | 100233.588 | 97829.9396 | 609.18051 | 152.18332 | -3.34321 |
| 452 | D2HIGE | drift | 1259.83895 | 100228.869 | 97832.4293 | 608.8688 | 152.18332 | -3.34321 |
| 453 | UPHRN2 | horn_up | 1290.5026 | 100201.795 | 97846.714 | 607.08045 | 152.18332 | -3.34321 |
| 454 | ACTRN2 | horn2 | 1290.68206 | 100201.636 | 97846.7976 | 607.06998 | 152.18332 | -3.34321 |
| 455 | DWNRN2 | horn_dn | 1300.52456 | 100192.946 | 97851.3827 | 606.49597 | 152.18332 | -3.34321 |
| 456 | IHD3 | drift | 1305.86904 | 100188.227 | 97853.8725 | 606.18425 | 152.18332 | -3.34321 |
| 457 | M_CAVE | POINT | 1309.14988 | 100185.33 | 97855.4008 | 605.99292 | 152.18332 | -3.34321 |
| 458 | OVERHA | drift | 1309.14988 | 100185.33 | 97855.4008 | 605.99292 | 152.18332 | -3.34321 |
| 459 | DKINHL | drift | 1319.12085 | 100176.526 | 97860.0459 | 605.41139 | 152.18332 | -3.34321 |
| 460 | M_THAL | POINT | 1337.64936 | 100160.167 | 97868.6774 | 604.33078 | 152.18332 | -3.34321 |
| 461 | DK_PCA | DECA44 | 1337.64936 | 100160.167 | 97868.6774 | 604.33078 | 152.18332 | -3.34321 |
| 462 | DK_PCB | DEC150 | 1483.26094 | 100031.601 | 97936.5106 | 595.83844 | 152.18332 | -3.34321 |
| 463 | DK_PCC | DEC150 | 1975.38594 | 99597.0842 | 98165.7674 | 567.13683 | 152.18332 | -3.34321 |
| 464 | DK_PCD | DEC100 | 2467.51094 | 99162.5678 | 98395.0242 | 538.43521 | 152.18332 | -3.34321 |
| 465 | DK_PCE | DEC100 | 2795.59428 | 98872.8901 | 98547.8621 | 519.3008 | 152.18332 | -3.34321 |
| 466 | DK_PCF | DEC125 | 3123.67761 | 98583.2125 | 98700.6999 | 500.16639 | 152.18332 | -3.34321 |
| 467 | DENCU | drift | 3533.78178 | 98221.1154 | 98891.7473 | 476.24839 | 152.18332 | -3.34321 |
| 468 | DUMP | DUMP | 3540.34344 | 98215.3219 | 98894.804 | 475.86571 | 152.18332 | -3.34321 |
| 469 | DENCD | drift | 3564.35914 | 98194.1175 | 98905.9918 | 474.46506 | 152.18332 | -3.34321 |
| 470 | MU_UP | drift | 3583.78168 | 98176.9685 | 98915.0398 | 473.33232 | 152.18332 | -3.34321 |
| 471 | MUOND | MUON | 3588.71129 | 98172.616 | 98917.3362 | 473.04482 | 152.18332 | -3.34321 |
| 472 | MU_DN | drift | 3590.3545 | 98171.1652 | 98918.1017 | 472.94899 | 152.18332 | -3.34321 |
| 473 | MUUP2 | drift | 3593.79862 | 98168.1242 | 98919.7062 | 472.7481 | 152.18332 | -3.34321 |
| 474 | MU_UP | drift | 3633.23545 | 98133.3039 | 98938.0779 | 470.44807 | 152.18332 | -3.34321 |
| 475 | MUOND | MUON | 3638.16507 | 98128.9513 | 98940.3743 | 470.16058 | 152.18332 | -3.34321 |
| 476 | MU_DN | drift | 3639.80827 | 98127.5005 | 98941.1398 | 470.06474 | 152.18332 | -3.34321 |
| 477 | MUUP3 | drift | 3643.25239 | 98124.4595 | 98942.7442 | 469.86386 | 152.18332 | -3.34321 |
| 478 | MU_UP | drift | 3702.40765 | 98072.229 | 98970.3018 | 466.41383 | 152.18332 | -3.34321 |
| 479 | MUOND | MUON | 3707.33724 | 98067.8765 | 98972.5982 | 466.12633 | 152.18332 | -3.34321 |
| 480 | MU_DN | drift | 3708.98044 | 98066.4257 | 98973.3637 | 466.0305 | 152.18332 | -3.34321 |
| 481 | MUUP4 | drift | 3712.4246 | 98063.3847 | 98974.9682 | 465.82961 | 152.18332 | -3.34321 |
| 482 | MU_UP | drift | 3811.01666 | 97976.3339 | 99020.8973 | 460.07956 | 152.18332 | -3.34321 |
| 483 | MUOND | MUON | 3815.94624 | 97971.9814 | 99023.1938 | 459.79206 | 152.18332 | -3.34321 |
| 484 | MU_DN | drift | 3817.58944 | 97970.5305 | 99023.9593 | 459.69623 | 152.18332 | -3.34321 |
| 485 | SHIELD | drift | 3821.0336 | 97967.4895 | 99025.5637 | 459.49534 | 152.18332 | -3.34321 |
| 486 | TUNNEL | TUNNEL | 4409.14181 | 97448.2257 | 99299.5344 | 425.19584 | 152.18332 | -3.34321 |
| 487 | M_ENCU | EX_ENU | 4484.72906 | 97381.4868 | 99334.7467 | 420.78745 | 152.18332 | -3.34321 |

| | | | | | | | | |
|-----|--------|--------|------------|------------|------------|------------|-----------|----------|
| 488 | MIN_ND | EXP | 4570.37268 | 97305.8687 | 99374.6439 | 415.79257 | 152.18332 | -3.34321 |
| 489 | M_ENCD | EX_END | 4624.95981 | 97257.6716 | 99400.0734 | 412.60895 | 152.18332 | -3.34321 |
| 490 | ILWIMN | drift | 4634.97675 | 97248.8272 | 99404.7398 | 412.02473 | 152.18332 | -3.34321 |
| 491 | MINOFU | EXP_F2 | 2413631.72 | -2029748.9 | 1221637.64 | -140084.97 | 152.18332 | -3.34321 |
| 492 | MINOFD | EXP_F2 | 2413690.88 | -2029801.1 | 1221665.2 | -140088.42 | 152.18332 | -3.34321 |



FERMILAB

ENGINEERING NOTE

SECTION

PROJECT

SERIAL-CATEGORY

PAGE

SUBJECT

MAXIMUM N₂ INTO THSR IF PIPE 'BROKE'
FROM MI-60 DEWAR @ 100 PSI

NAME

D. POSHKA

DATE

8/3/04

REVISION DATE

$$P_1 = 100 \text{ PSIG} \quad \therefore P'_1 = 115 \text{ PSIA}$$

$$P_2 = 0 \text{ PSIG}$$

$$\Delta P = 100 \text{ PSIG}$$

$$\because \Delta P > 40\% P_1 \quad \therefore q'm (\text{cfm}) = 678 \text{ Yd}^2 \sqrt{\frac{\Delta P P'_1}{K T, Sg}}$$

γ = EXPANSION FACTOR

$$\frac{\Delta P}{P'_1} = \frac{100}{115} = .87 \quad \therefore \gamma = .710 \text{ @ sonic limit}$$

$$d = \text{pipe internal diameter} = 0.875 - 2(0.045) \\ = 0.785 "$$

$$Sg = 28/29 = 0.96$$

$$T = \text{ABSOLUTE TEMPERATURE} = 460^\circ + 80^\circ F = 540^\circ R$$

$$K = f \frac{L}{D} \quad D = \frac{0.785"}{12"/FT} = 0.0654$$

$$L = 360' + (1100 - 317) + 65 + 32 + 32 + 16 + 11 + 29 + 50 \\ = 1378 \rightarrow \text{Round To } 1400' \text{ To INCLUDE OFFSETS.}$$

$$f = \cancel{0.010} \text{ for drawn tubing, } \emptyset 1"$$

$$\therefore K = 0.010 \cdot \frac{1400}{0.0654} = 214.0$$

FERMILAB
ENGINEERING NOTE

SECTION

PROJECT

SERIAL-CATEGORY

PAGE

SUBJECT

NAME

D. POSHKA

DATE

8/3/04

REVISION DATE

$$q_m' (\text{cfm}) = 678 \times (.710)(0.785^2) \sqrt{\frac{100 \cdot 115}{214 \cdot 540 \cdot (.96)}}$$

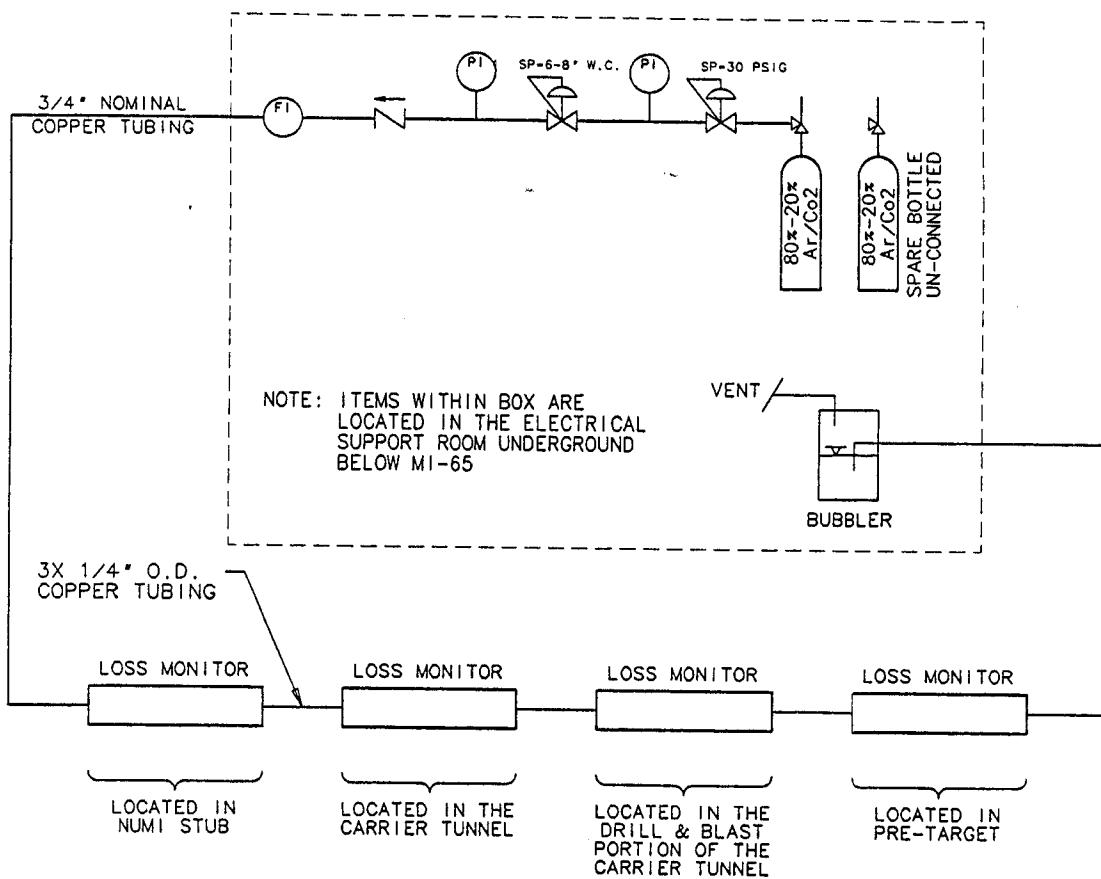
$$= 678 \times .710 \times .785^2 \times 0.3219$$

$$= 95 \text{ cfm}$$

So, assuming the worst case, the N₂ leak rate into MI-65 THSR (Target Hall Support Room) would be 95 cfm, without considering any flow restrictions.

IF L = 360 + ~~400~~⁹⁷⁶ - 317 (PreTARGET), K =
= ~~400~~', ~~400~~' , $q_m' =$
SEE SPREAD SHEETS

| REV | DESCRIPTION | DRAWN | DATE |
|-----|-------------|-------|------|
| A | YED | | DATE |



| UNLESS OTHERWISE SPECIFIED | | | ORIGINATOR | D.PUSHKA | 30-JUL-2004 |
|---|-------|--------|------------|-----------|-------------|
| .XX | .XXX | ANGLES | DRAWN | R.L.SMITH | 30-JUL-2004 |
| ± -- | ± --- | ± - | CHECKED | | |
| 1. BREAK ALL SHARP EDGES MAX. | | | APPROVED | D.PUSHKA | 30-JUL-04 |
| 2. DO NOT SCALE DRAWING. | | | USED ON | *** | |
| 3. DIMENSIONS BASED UPON ASME Y14.5M-1994 | | | MATERIAL | **** | |
| 4. MAX. ALL MACH. SURFACES X/ | | | | | |
| 5. DRAWING UNITS: INCHES | | | | | |



FERMI NATIONAL ACCELERATOR LABORATORY
UNITED STATES DEPARTMENT OF ENERGY

NUMI/UTILITIES
TOTAL LOSS MONITOR
GAS SYSTEM SCHEMATIC

| SCALE | DRAWING NUMBER | SHEET | REV |
|-------|--------------------|--------|-----|
| NONE | 8875.117-MB-433163 | 1 OF 1 | |

CREATED WITH : Ideas3m3 GROUP: PPD/MECHANICAL DEPARTMENT

| UTILITIES IN TARGET SHAFT | | | | | | |
|---------------------------|------|-------------------|---------------|-------------------|-------|-------|
| PIPELINE | SIZE | TYPE | PIPELINE RATE | PIPELINE PRESSURE | POINT | TEMP. |
| LAWN | " 2" | NO. 80 SINTER STL | 200 GPM | NOT RECD | 100°F | 60°F |
| LAWN | " 2" | NO. 80 SINTER STL | 200 GPM | NOT RECD | 40°F | 60°F |
| SEWAGE | " 2" | NO. 80 SINTER STL | 200 GPM | > A-100°F | 210°F | 210°F |
| AMU-TRE-1 | " 2" | NO. 80 GALV. STL | 7.6 GPM | 100°F | 100°F | 60°F |
| AMU-TRE-2 | " 1" | NO. 80 GALV. STL | 7.6 GPM | 100°F | 100°F | 60°F |

HVAC GENERAL NOTES

- ALL DUCTWORK SHALL BE FURNISHED AND INSTALLED IN ACCORDANCE WITH SECTION 1615 OF THE SPECIFICATIONS.

HVAC SUBCONTRACTOR SHALL BE RESPONSIBLE FOR FURNISHING AND INSTALLING ALL DUCTWORK, FAN/THERM, REFRIGERANT PIPING, AIR HANDLING UNITS, COOLING TOWER, ROOF TOP COOLER, DRILLING MACHINERY, DAMPERS, COOLING COIL, COMPRESSORS, VALVES, THERMOMETERS, INSULATION, LIKENESS AND FLEXIBLE CONNECTORS.

HVAC SUBCONTRACTOR SHALL BE RESPONSIBLE FOR SEALING ALL DUCTWORK AND FURNISHING ALL PENETRATIONS THROUGH NEW AND EXISTING STRUCTURES.

INSTALLATION OF MATERIALS, EQUIPMENT, AND SYSTEMS NOT LISTED IN THE CONTRACT DOCUMENTS OR IN THE DRAWINGS. INTENT OF DESIGNS MUST HAVE PRIOR WRITTEN APPROVAL.

HVAC SUBCONTRACTOR SHALL VERIFY ALL DOING DIMENSIONS PRIOR TO FABRICATION, ERECTION, OR CONSTRUCTION OF DUCTWORK & DUCTILE FITTINGS.

LOCATE THERMOMETERS AND SWITCHES AT 4'-0" ABOVE FINISHED FLOOR, WHERE REQUIRED.

HVAC SUBCONTRACTOR SHALL BE RESPONSIBLE FOR STAND-UP AND ASSEMBLY OF ALL SYSTEMS. FURNISH AND ERECT COMPLETE START-UP, SPARE PARTS, AND TROUBLESHOOTING MANUALS FOR ALL SYSTEMS. THESE SHOULD BE PROVIDED BY SUBCONTRACTOR AS A SEPARATE ITEM.

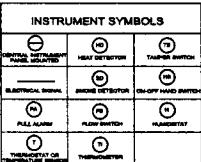
HVAC SUBCONTRACTOR TO DEMONSTRATE ALL WALL AND ROOF PENETRATION AREAS AND LOCATIONS.

HVAC SUBCONTRACTOR TO TRANSITION DUCT WORK REQUIRED TO FIT EQUIPMENT ACTUALLY PURCHASED.

HVAC SUBCONTRACTOR SHALL FURNISH SUPPORT STEEL FOR CIVIC EQUIPMENT AND ANY ADDITIONAL SUPPORT STEEL, SUBCONTRACTOR TO DESIGN AND INSTALL PER HIRE. REQUIREMENT FOR CIVIC EQUIPMENT, SUBCONTRACTOR COORDINATE THE DAMPER SIZES AND INSTALL ALL DUCTWORK.

ALL DUCTS TO BE CONSTRUCTED FOR 10 W.G. PRESSURE CLASS.

| GENERAL SYMBOLS | |
|-----------------|---------------------|
| | NORMALLY OPEN |
| | NORMALLY CLOSED |
| | BALANCE VALVE |
| | SWINGING VALVE |
| | ANGLE VALVE |
| | OPEN DRAIN OR PURGE |
| | THREE-WAY VALVE |
| | PORT REDUCER |
| | SUSPENDED REDUCER |
| | STRAINER |
| | CONCENTRIC REDUCER |
| | Pipe Direct, Casing |



| POWER EXHAUST VENTILATOR SCHEDULE | | | | | | | | | | | | | |
|-----------------------------------|-------------------------|------------------|---------------------------|--------------|---|-----------|------|--------|------------|-------|-------|---------|---|
| TAG NO. | LOCATION | PERFORMANCE DATA | | | SELECTION DATA | | | | MOTOR DATA | | | REMARKS | |
| | | CFM | INTERNAL S.P. IN. W.G. | MANUFACTURER | TYPE & MODEL # | SIZE | RPM | DRIVE | HP | VOLTS | PHASE | CYCLE | ACCESSORIES PROVIDED WITH UNIT |
| SP-4A-1 | MUON ALCOVE 2 | 580 | 0.18 | COOK | CENTRI - VANE INLINE CENTRIFUGAL (COVTD) | 10 | 1725 | DIRECT | 1/6 | 120 | 1 | 60 | INLET SCREEN INLET SCREEN VARIABLE SPEED CONTROLLER, WALL MOUNTED, VARIABLE FAN, HAVING TWO GUARD FOR DUCT CONNECTIONS |
| SP-4A-2 | MUON ALCOVE 3 | 580 | 0.18 | COOK | CENTRI - VANE INLINE CENTRIFUGAL (COVTD) | 10 | 1725 | DIRECT | 1/6 | 120 | 1 | 60 | |
| SP-4A-3 | MUON ALCOVE 4 | 580 | 0.18 | COOK | CENTRI - VANE INLINE CENTRIFUGAL (COVTD) | 10 | 1725 | DIRECT | 1/6 | 120 | 1 | 60 | |
| EF-6 | MUON ALCOVE VENTILATION | 220 | 1.38 | AEROVENT | CENTRIFAL -VANE CENTRIFUGAL, COO | 12 | 1725 | DIRECT | 1/2 | 120 | 1 | 60 | |
| EF-1 | UPSTREAM PRE-TARGET | 1800 | 1.75 | GREENHECK | UPLAFT CENTRIFUGAL MODEL: CUBE | 181XP-18 | 1725 | BELT | 1-1/2 | 480 | 3 | 60 | |
| EF-2 | UPSTREAM DECAY | 1070 | 0.85 | GREENHECK | UPLAFT CENTRIFUGAL MODEL: CUBE | 181-10 | VFD | BELT | 1 | 480 | 3 | 60 | |
| EF-3 | DOWNSTREAM DECAY | 3600 | 2.38 | GREENHECK | UPLAFT CENTRIFUGAL MODEL: CUBE | 300XP-30 | 1280 | BELT | 3 | 480 | 3 | 60 | |
| EF-4 | MARSH HALL | 8800 | 3.08 | GREENHECK | UPLAFT CENTRIFUGAL MODEL: CUBE | 300XP-48 | VFD | BELT | 8 | 480 | 3 | 60 | |
| EF-7-1 | CARRIER TUNNEL | 1000 | 0.49 | GREENHECK | WALL MOUNT PROPELLER FAN MODEL: 81 | 12-438-A4 | 1750 | DIRECT | 1/4 | 120 | 1 | 60 | |
| EF-7-2 | PRE-TARGET TUNNEL | 1000 | 0.80 | GREENHECK | WALL MOUNT PROPELLER FAN MODEL: 81 | 14-438-A3 | 1750 | DIRECT | 1/3 | 120 | 1 | 60 | |

| TAG NO. | LOCATION | PERFORMANCE DATA | | SELECTION DATA | | | MOTOR DATA | | | REMARKS | | | |
|---------|--|------------------|---------------|----------------|------------------------------|---------------------------|------------|------|------|---------|-------|-------|---|
| | | GPM | TOTAL FT. HD. | WATER TEMP | DESIGN BASIS MANUFACTURER | TYPE | MODEL | RPM | HP | VOLTS | PHASE | CYCLE | |
| SP-4A-1 | MINOS ACCESS SHAFT BUMP PIT | 340 | 400 | 56° - 80° F | GOULD | SUBMERSIBLE TURBINE | VIB-TOLC | 3600 | .95 | 460 | 3 | 60 | FLOAT CONTROLLED. SIMPLEX UNITS. EACH PUMP SHALL HAVE DETAILED INSTRUCTIONS FOR THE USE OF THE PUMP CONTROL PANEL FOR LEAD/LAG BETWEEN THE TWO PUMPS. |
| SP-4T-1 | TARGET AREA BUMP PIT | 40 | 37 | 56° F | FLYGT | DUPLEX SUBMERSIBLE | 882062.170 | 3450 | 0.5 | 460 | 3 | 60 | 40F |
| SP-4T-3 | TARGET ELEVATOR PIT | 6 | 12 | 56° F | FLYGT | DEWATERING PUMP | 83-2 | 3450 | 0.35 | 115 | 1 | 60 | |
| SP-4A-3 | MINOS ACCESS SHAFT BUMP PIT | 480 | 400 | 56° - 80° F | GOULD | SUBMERSIBLE TURBINE | VIB-TCHC | 3450 | .80 | 460 | 3 | 60 | FLOAT CONTROLLED. SIMPLEX UNIT. SEE CONTROL SEQUENCE FOR SPECIAL ELECTRICAL PROTECTION |
| SP-4M-1 | ABSORBER & MINOS HALL COOLING LOOP | 380 | 214 | 56° F | FLYGT | SUBMERSIBLE CIRCULATOR | 842151.011 | 3450 | .80 | 460 | 3 | 60 | SEE CONTROL NOTE: |
| SPWP-A1 | DECAY PIPE COOLING | 70 | 180 | 70° F | BELL & GORRETT | CIRCULATOR | SERIES 100 | 3600 | 10 | 460 | 5 | 60 | WILL BE INTERLOCKED WITH SP-4A-1 & SP-4A-3. SPWP-A1 (DR 54) DO NOT OPERATE WHEN SP-4A-1 & SP-4A-3 ARE "OFF". |

CONTROLS NOTES

- Sequence of controls for HM-4/HM-4S and HM-4A/HM-4-2**

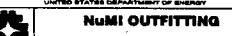
 - 1. Controller for HM-4 and HM-4S shall have a low level alarm at 24" pump depth (adjustable) and a pump shutdown setting point at 42" pump depth. At any level above the low water cut-off the pump shall be disabled by the duplex control panel.
 - 2. The pump shall be controlled by a pump shutdown switch located on the duplex control panel. Levelling switch(es) shall be incorporated by starting the leg pump and pumping four times for 60 seconds (quiescent) before the previously held pump is shut down.
 - 3. The test pump shall be started and stopped at the control panel based on the need to provide a minimum of 1000 GPM of flow to the system at the surface or 1000 GPM underground. Run verification shall be determined by individual pressure sensors located in each pump discharge piping upstream of the check valve. If the head pump's pressure sensor indicates a pressure drop of 10% or more than the low pressure sensor is energized and the lead pump shall be de-energized and alarm. If neither pump pressure sensor indicates a pressure drop, the pump will remain in the control panel. Audible controls in the pump shall allow monitoring of the pump status.
 - 4. HM-4 and HM-4-2 (based on head/tank) shall be energized to run and the associated 2 pressure valve shall open upon any 80' HM-4 or 80' HM-4-2 running. The associated 3 way valve shall be controlled by a discharge temperature sensor located in the return line. The 3 way valve shall be energized to open to allow the pump to maintain the discharge at 40°F (adjustable). If either HM-4 or HM-4-2 is not running for 10 minutes the associated 2 pressure valve shall close.
 - 5. HM-4 and HM-4-2 (based on head/tank) shall start and the associated 2 pressure valve shall close.

NOTES:

1. SITE PROJECT 8-7-6 FOR SURFACE EQUIPMENT SERVICING THE UNDERGROUND FACILITY OTHER THAN EXHAUST VENTS ATTACHED

| ELECTRIC UNIT HEATER SCHEDULE | | | | | | | | | | | | |
|-------------------------------|-----------------------|--------------|-----------|------|------------|-----------------|------|------------|------|-----------|-------------------------|-------------------------|
| TAG NO. | LOCATION | MFR | MODEL NO. | KW | TEMP. RATE | HEATER VOLTS/HZ | FLA | MOTOR H.P. | COPM | THROW FT. | MTL. WT. BOTTOM OF UNIT | REMARKS |
| EUH-1-T-2.3 | PRETAIN TUNNEL | U.S. COIL | 1000-1000 | 3.3 | 20°F | 2771/60 | 11.9 | 1/12 | 400 | 12 | 8'@2' | |
| EUH-1-T-3.4 | TARGET EXIT STARWELL | U.S. COIL | 1000-1000 | 3.3 | 20°F | 2771/60 | 11.9 | 1/12 | 400 | 12 | 8'@2' | |
| EUH-1-T-5 | TARGET COOMAH AREA | U.S. COIL | 1000-1000 | 3.3 | 20°F | 2771/60 | 11.9 | 1/12 | 400 | 12 | 8'@2' | |
| EUH-1-T-6, 8, 9 | TARGET HALL | TRANE | 1000-1000 | 4.0 | 40°F | 2771/60 | 18.1 | 1/12 | 400 | 12 | 8'@2' | |
| EUH-1-M-2, 3, 9 | MUON ALCOVE | TRANE | 1000-1000 | 3.3 | 20°F | 2771/60 | 11.9 | 1/12 | 400 | 12 | 8'@2' | |
| EUH-1-M-4 | ARMED ENCLOSURE | U.S. COIL | 1000-1000 | 3.3 | 20°F | 2771/60 | 11.9 | 1/12 | 400 | 12 | 8'@2' | |
| EUH-1-M-5, 6, 10 | ARMED ACCESS TUNNEL | U.S. COIL | 1000-1000 | 3.3 | 20°F | 2771/60 | 11.9 | 1/12 | 400 | 12 | 8'@2' | |
| EUH-1-M-11, 12, 13 | MINOR ACCESS TUNNEL | U.S. COIL | 1000-1000 | 3.3 | 20°F | 2771/60 | 11.9 | 1/12 | 400 | 12 | 8'@2' | |
| EUH-1-M-14 | MINOR ELEVATOR SHAFT | U.S. COIL | 1000-1000 | 6.0 | 40°F | 2771/60 | 18.1 | 1/12 | 400 | 12 | 8'@2' | |
| EDH-1-T | TARGET EXIT PARABOWAY | INDUSCORR/TU | 1000-1000 | 3.78 | 10.8°F | 2771/60 | 14.4 | N/A | 700 | N/A | N/A | 2 STEP CONTROL W/ PANEL |
| EDH-1-M | MINOR EXIT PARABOWAY | INDUSCORR/TU | 1000-1000 | 3.78 | 8.8°F | 2771/60 | 15.6 | N/A | 1000 | N/A | N/A | 2 STEP CONTROL W/ PANEL |

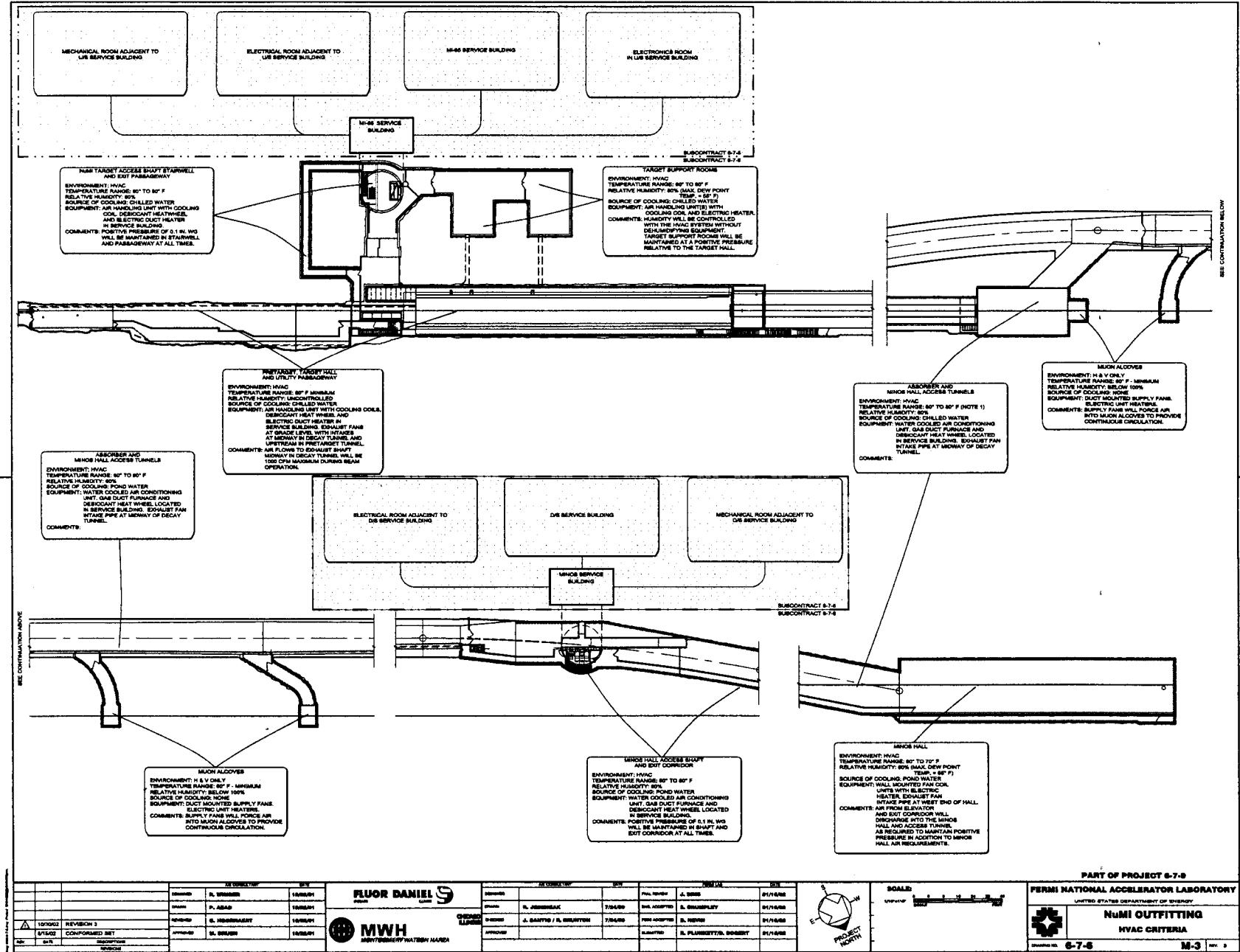
1999-2000 年度全国普通高等学校毕业生就业情况统计表



MECHANICAL EQUIPMENT SCHEDULE

ITEM NO. 6-7-6 M-2 REV. 11

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PART OF PROJECT 8-7-B

DOE/NATIONAL ACCELERATOR LABORATORY

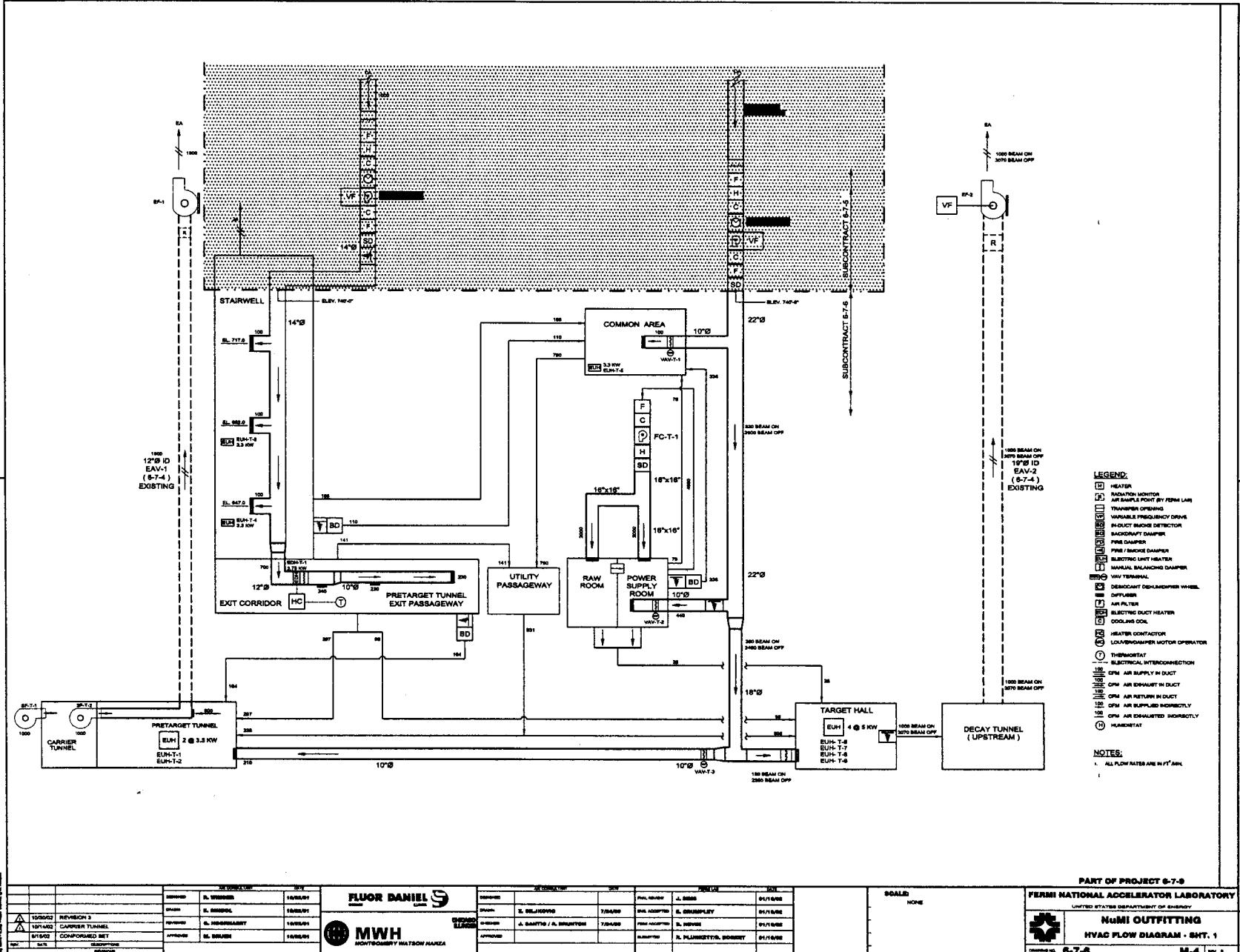
UNITED STATES DEPARTMENT OF ENERGY

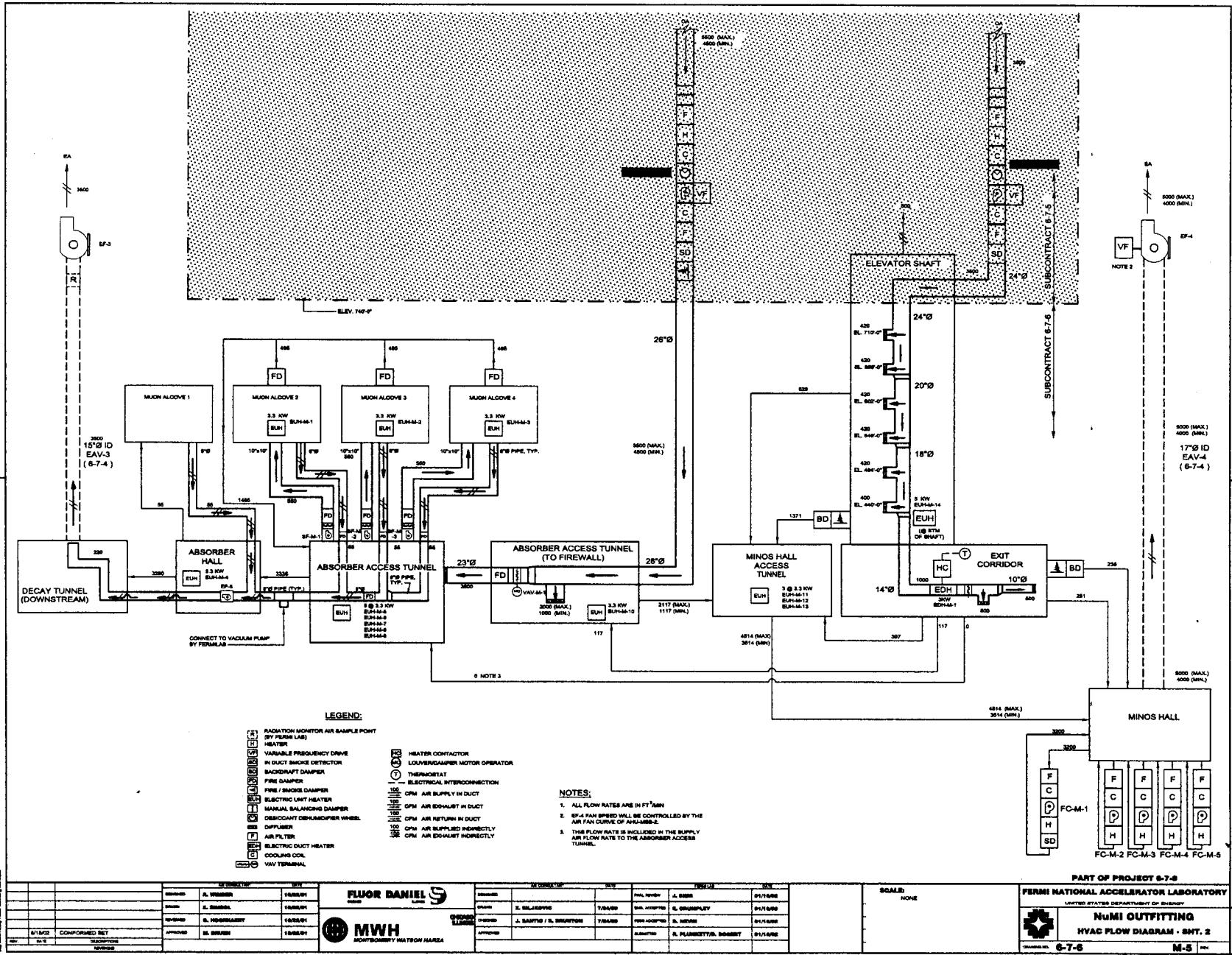
NUMBER OF PAGES

NOVAC CULTURA

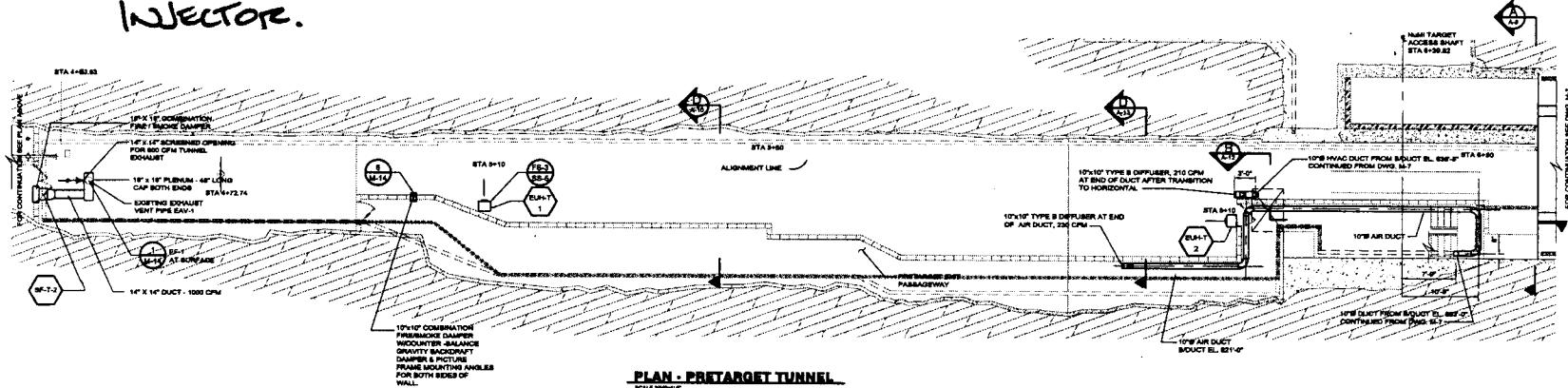
WVAC CRITERIA

6-7-6 M-3

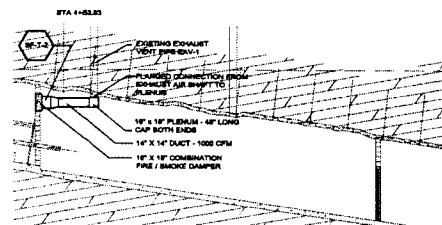




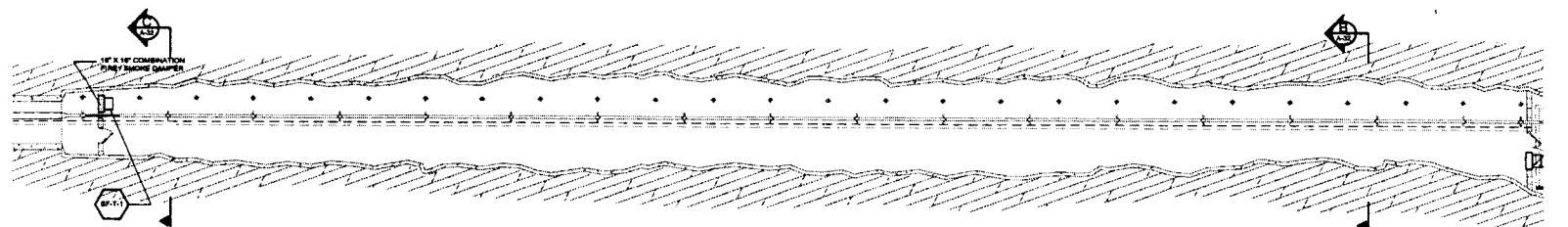
TLM IS INSTALLED ALONG ENTIRE TUNNEL SECTION SHOWN ON THIS
DWG. ALSO EXTENDS U.S. TO THE NORMI STUB IN THE MAIN
INJECTOR.



PLAN • PRETARGET TUNNEL

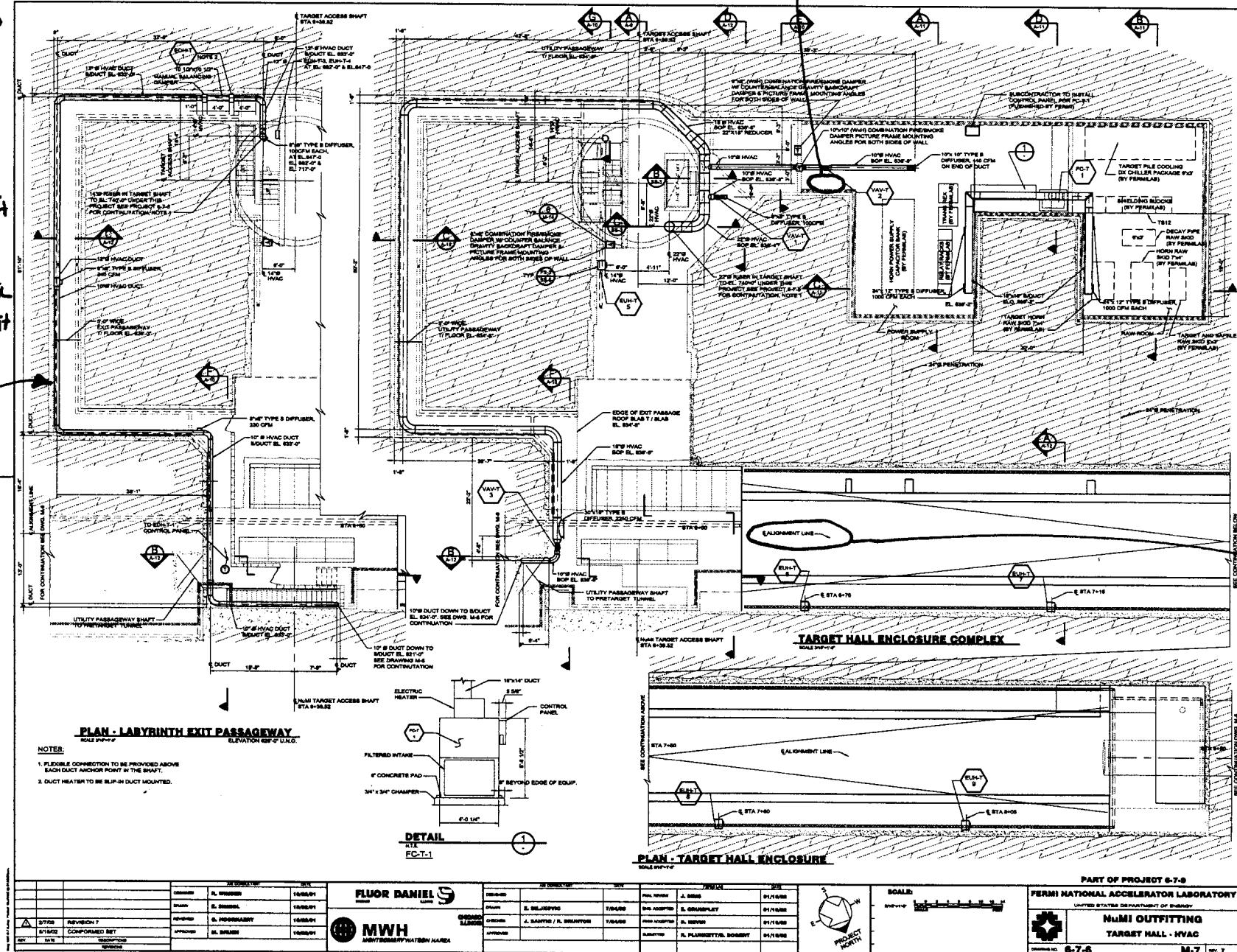


SECTION : PRETARGET TUNNEL



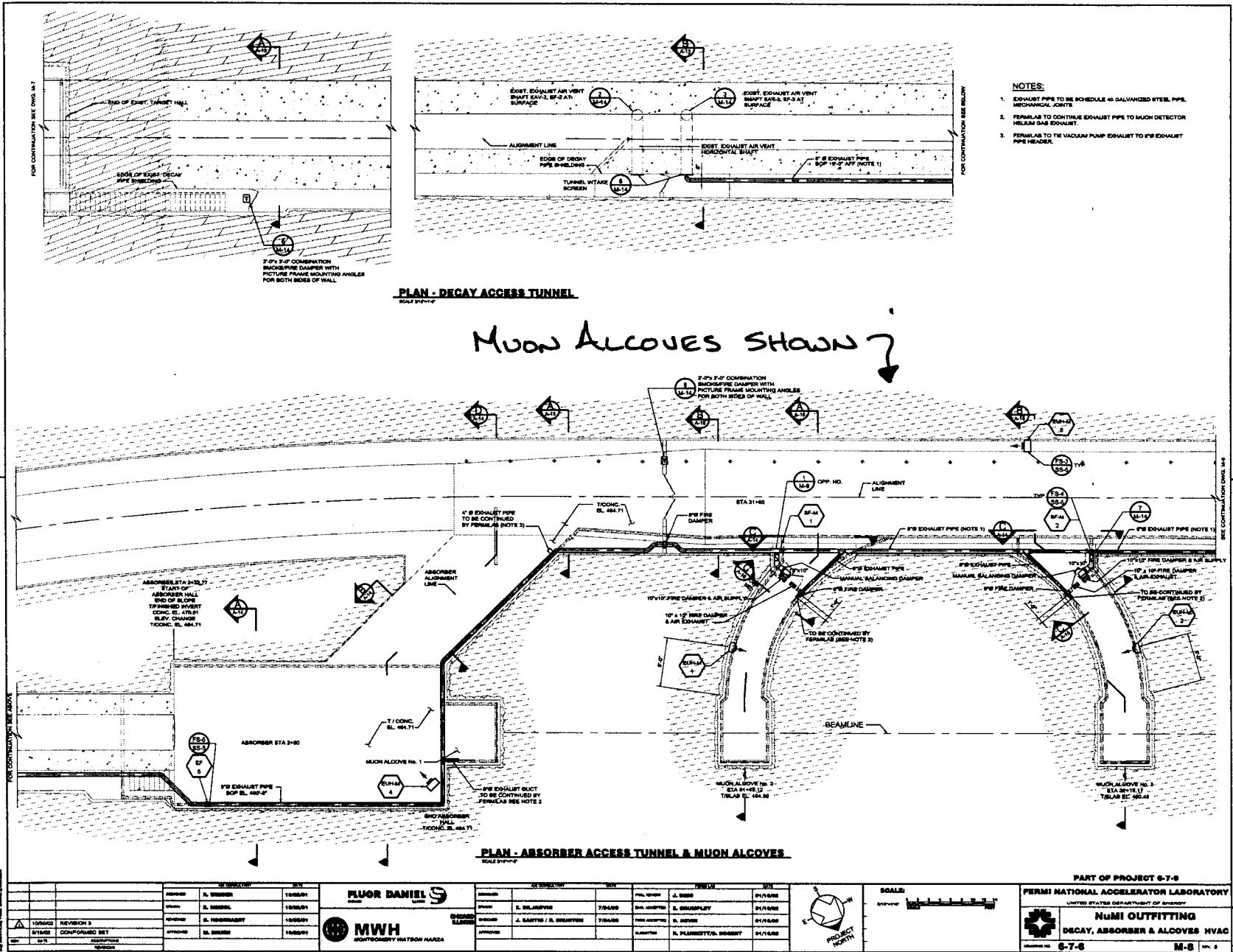
PLAN - CARRIER TUNNEL

TLM AND
 THE HORN
 RAW SYS
 GN2
 PIPE
 CHASE
 LABYRINTA
 ABOVE
 PERSONAL
 LABYRINTA

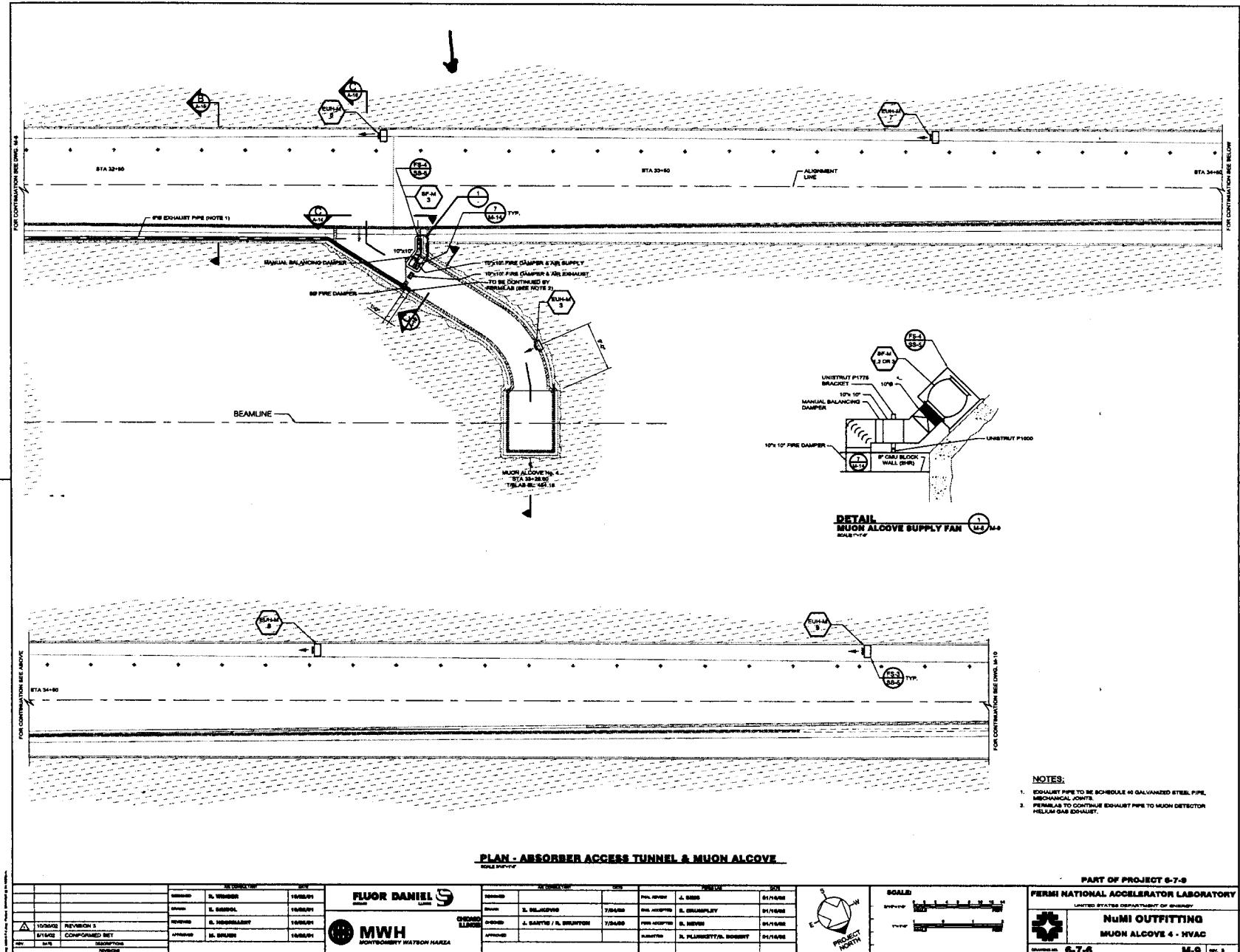


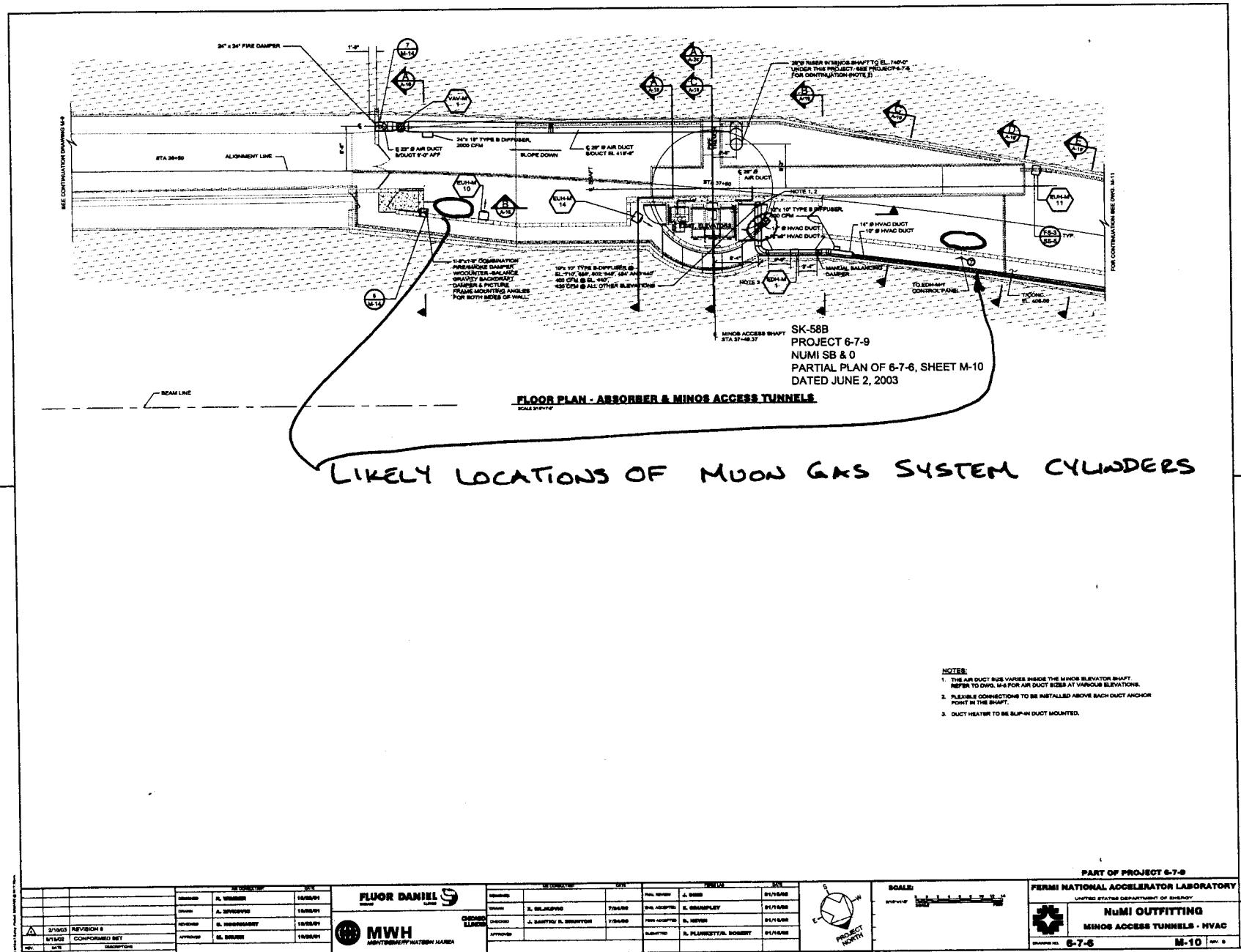
}
RAW SKID LOCATIONS
 w/ POSSIBLE
 GN2 or A
 cylinder
 during
 commission

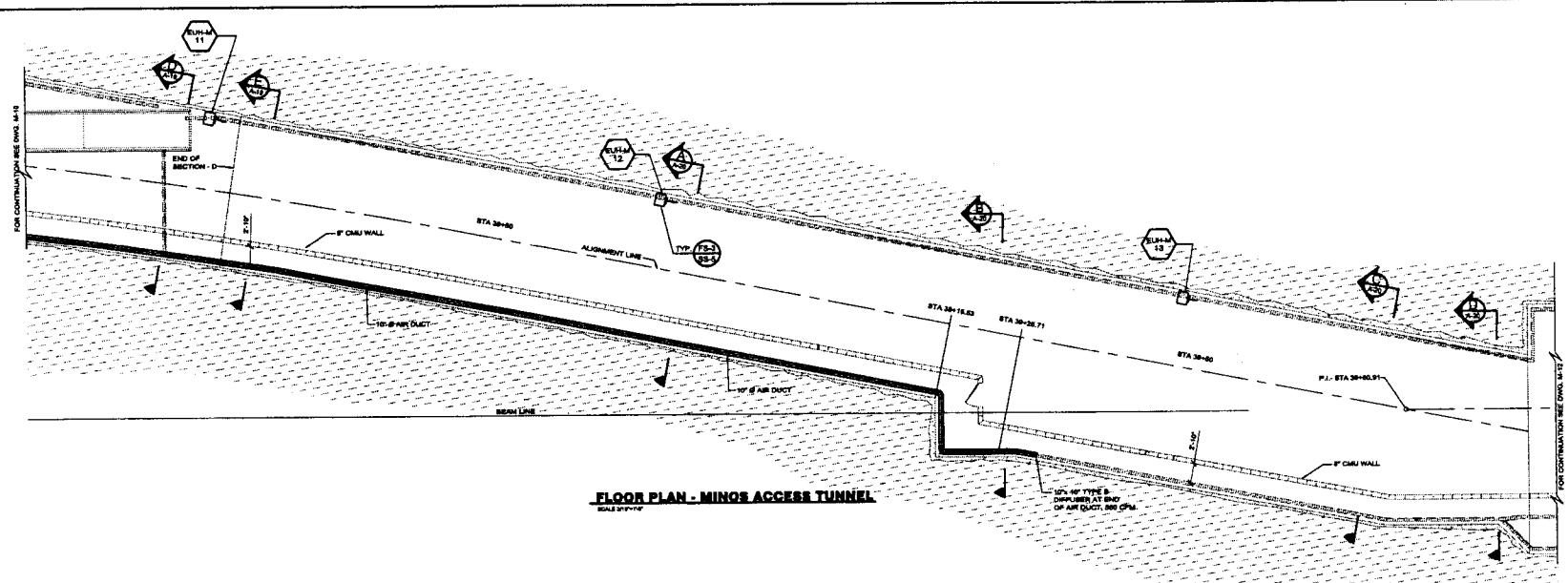
}
LOCATION
 OF THE
 TARGET



D.S. Most Muon Acova



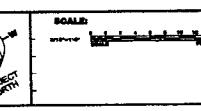




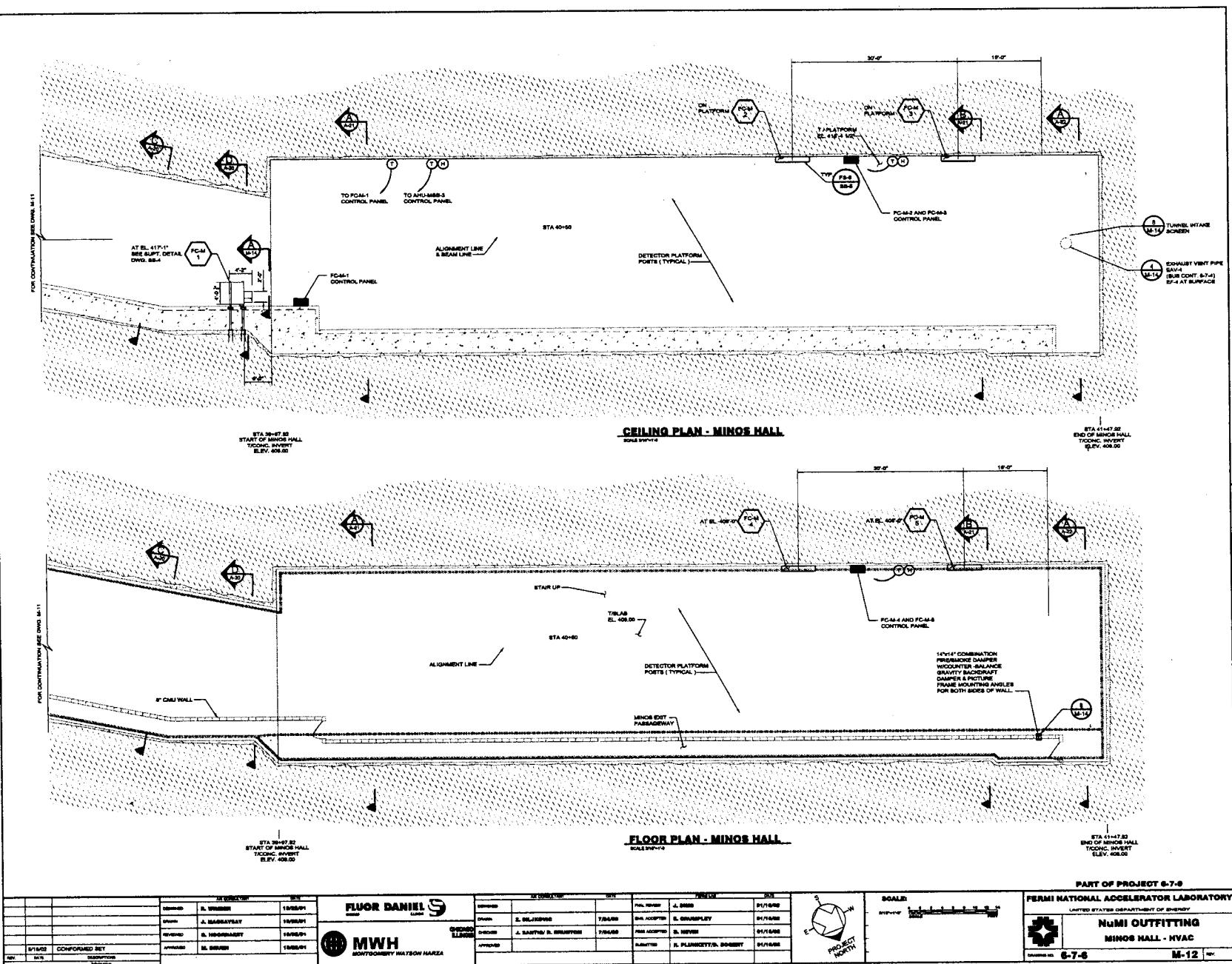
| IN CONSTRUCTION DATE | | |
|----------------------|---------------|--------|
| REMOVED | S. WILSON | 1/2004 |
| REMOVED | P. ADAM | 1/2004 |
| REMOVED | G. HORNIGRANT | 1/2004 |
| APPROVED | M. BRAUN | 1/2004 |



| IN CONSTRUCTION DATE | IN OPERATION DATE | PERIOD | PERIOD | PERIOD | PERIOD |
|----------------------|-------------------|--------|--------|-----------------------|--------|
| REMOVED | S. WILSON | 1/2004 | PERIOD | J. BAKER | PERIOD |
| REMOVED | P. ADAM | 1/2004 | PERIOD | S. GRAMPOLY | PERIOD |
| REMOVED | G. HORNIGRANT | 1/2004 | PERIOD | S. HENRY | PERIOD |
| APPROVED | M. BRAUN | 1/2004 | PERIOD | R. PLUMMETT, DIRECTOR | PERIOD |



PART OF PROJECT G-7-B
FERMI NATIONAL ACCELERATOR LABORATORY
UNITED STATES DEPARTMENT OF ENERGY
NuMI OUTFITTING
MINOS ACCESS & TUNNEL HVAC
DRAWING NO. G-7-B M-11 -
10 JUNE 2004



TARGET CONTROL NOTES:

CONTROL WIRES, CABLE, DEVICES, AND RELAY SHALL BE INSTALLED BY THE SUBCONTRACTOR.
CONTROL SYSTEMS FOR EA-1 PC-T-1, VAV-T-1 THROUGH VAV-T-3, EF-2 SHALL BE PROGRAMMED AND COMMISSIONED BY FERMILAB.

VAV BOXES SHALL BE INSTALLED TO CONTROL THE AIRFLOW IN THE DIFFERENT DUCT BRANCHES OF DISTRIBUTION. THE VAV BOXES FOR VAV-T-1, VAV-T-2, VAV-T-3 SHALL BE EQUIPPED WITH THE FOLLOWING JOHNSON CONTROLS VAV CONTROLLER, DAMPER MOTORS, AND DIFFERENTIAL PRESSURE RELIEFS. 24 VAC POWER THESE VAV BOXES SHALL BE SUPPLIED BY A TRANSFORMER LOCATED IN PANEL NC-35 EN-4.

CABLE COUNT, INSTALLATION MATERIALS, ETC. SHALL BE PROVIDED BY THE SUBCONTRACTOR. REFER TO THE FERMI LABORATORY DESIGN DRAWINGS FOR DETAILS.

LOW VOLTAGE CONTROL CABLE 4/2P THAT 24 VOLT SHALL BE 14 AWG STRANDED CABLE, 2 OR 3 CONDUCTORS AS NEEDED. CABLE LENGTH IS REQUIRED FOR CABLE BELOW IF ABOVE FINISHED FLOOR LEVEL.

CONNECT IS RECOMMENDED FOR HIGH VOLTAGE CABLE (NOT GREATER THAN 25 VOLTS). HIGH AND LOW VOLTAGE CABLE SHOULD NOT BE MIXED IN THE SAME CONDUIT.

CABLE TERMINATIONS ARE NOT REQUIRED AT CONTROL PANELS. SUBCONTRACTOR SHALL LEAVE AN EXTRA LOOP OF CABLE INSIDE THE PANEL.

LOW VOLTAGE CABLES INSTALLED WITHIN CONCEALED/ACCESSIBLE LOCATIONS DO NOT REQUIRE CONDUIT. USE OF WIRINGWAYS OR CABLE HOSES EVERY 4' IS ACCEPTABLE.

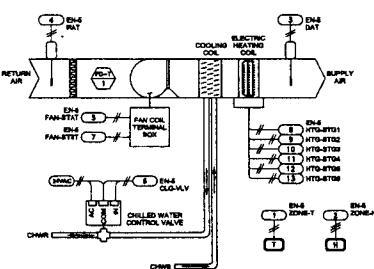
LOW VOLTAGE CABLE SHALL NOT BE TWISTED OR TAPE TO EXISTING CABLE, PIPE, OR CONDUIT.

CABLES SHALL BE NUMBERED AT BOTH ENDS ACCORDING TO NUMBERS SHOWN ON DRAWINGS.

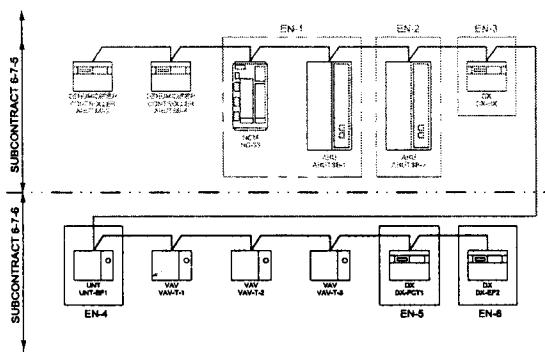
CABLES INSTALLED WITHIN AIR PURIFIES SHALL BE PURIFIED RATED.

NO NETWORK CABLE SHALL BE 14 AWG STRANDED 3 CONDUCTOR CABLE. INPUT PERI-SHA OR APPROVED EQUAL. NO CABLE SHALL BE RUN ACCORDING TO NC-35 NO NETWORK WIRING DRAWING AS SHOWN ON THIS DRAWING.

RESTORE EXPANDED PAMERS OF CUT OR PATCHED AREAS IN A MANNER THAT WILL ELIMINATE EVIDENCE OF PATCHING OR REPAIRING. UTILIZE ARCHITECTURALLY COMPATIBLE DEVICES FOR INSTALLATION IN FINISHED SPACE.

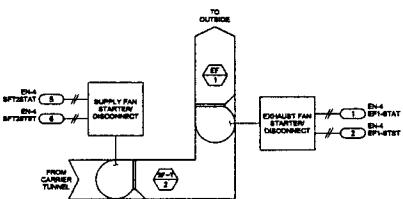


FAN COIL UNIT FC-T-1 CONTROL SYSTEM LAYOUT

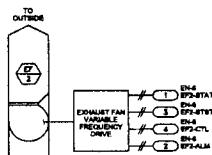


NC-35 N2 NETWORK WIRING

| REF ID | DESCRIPTION |
|----------|----------------|
| A-101468 | CARRIER TUNNEL |
| B-15050 | CONFORMED SET |



EXHAUST FAN EF-1 CONTROL SYSTEM LAYOUT



EXHAUST FAN EF-2 CONTROL SYSTEM LAYOUT

EF-1, EF-2, SF-T-1, AND SF-T-2 SEQUENCE OF OPERATIONS (FOR INFORMATION ONLY - PROGRAMMING NOT IN CONTRACT)

EF-1 OPERATION: Exhaust Fan EF-1 shall be controlled through software with damper/valve controller.

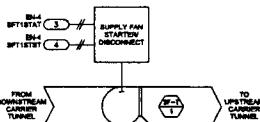
EF-2 OPERATION: Exhaust Fan EF-2 shall be controlled through software with damper/valve controller. The speed of EF-2 shall be converted through a variable frequency drive. When the fan is running at 100% speed, the variable frequency drive will be set to 1000 RPM (maximum). When the fan is set to 50% speed, the variable frequency drive will be set to 500 RPM. The DDC controller shall set the variable frequency drive to a speed calculated from the EF-2 fan curve to deliver 3075 RPM (maximum).

SF-T-1 OPERATION: Supply Fan SF-T-1 shall be controlled through software with exhaust fan EF-1.

SF-T-2 OPERATION: Supply Fan SF-T-2 shall be controlled through software with exhaust fan EF-1.

| ITEM SUPPLIED BY FERMILAB, INSTALLED BY SUBCONTRACTOR FOR 2 EXHAUST FANS |
|--|
| EF-STAT 2 CURRENT SWITCH |

EXHAUST FAN BILL OF MATERIALS



SUPPLY FAN BILL OF MATERIALS

| ITEM SUPPLIED BY FERMILAB, INSTALLED BY SUBCONTRACTOR FOR 2 SUPPLY FANS |
|---|
| EF-STAT 2 CURRENT SWITCH |

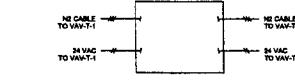
SUPPLY FAN SF-T-1 CONTROL SYSTEM LAYOUT

VAV-T-1, VAV-T-2, AND VAV-T-3, SEQUENCE OF OPERATIONS (FOR INFORMATION ONLY - PROGRAMMING NOT IN CONTRACT)

VAV OPERATION: VAV boxes shall be installed to control air flow to each zone. Each zone has a room temperature sensor, a room humidity sensor, a differential pressure sensor, a return air duct sensor, and a return air duct actuator. The VAV boxes shall be supplied with a Johnson Controls DDC controller, damper motor, and differential pressure sensor to sense air flow velocity. The DDC controller shall receive signals from the room temperature sensor, room humidity sensor, and differential pressure sensor. The DDC controller shall be set to the airflow shown on drawings A-4 for damper/timer AH-TRB-4.



VAV-T-1 PANEL DETAIL



VAV-T-2 PANEL DETAIL

FAN COIL UNIT BILL OF MATERIALS

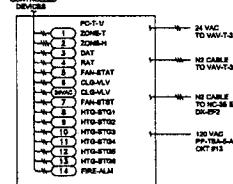
| ITEM SUPPLIED BY FERMILAB, INSTALLED BY SUBCONTRACTOR FOR 1 FAN COIL UNITS |
|--|
| ZONE-6T 1 ROOM TEMPERATURE SENSOR |
| ZON-HM 1 ROOM HUMIDITY SENSOR |
| DAT 1 DRAUGHT AIR DUCT SENSOR |
| RAT 1 RETURN AIR DUCT SENSOR |
| FAN-STAT 1 CURRENT SWITCH |
| CLD-HLV 1 VALVE AND ACTUATOR ASSEMBLY |
| EN4 1 CONTROLLER ENCLOSURE |



NC-35 EN-4 PANEL DETAIL



NC-35 EN-5 PANEL DETAIL



NC-35 EN-6 PANEL DETAIL

PART OF PROJECT 6-7-6

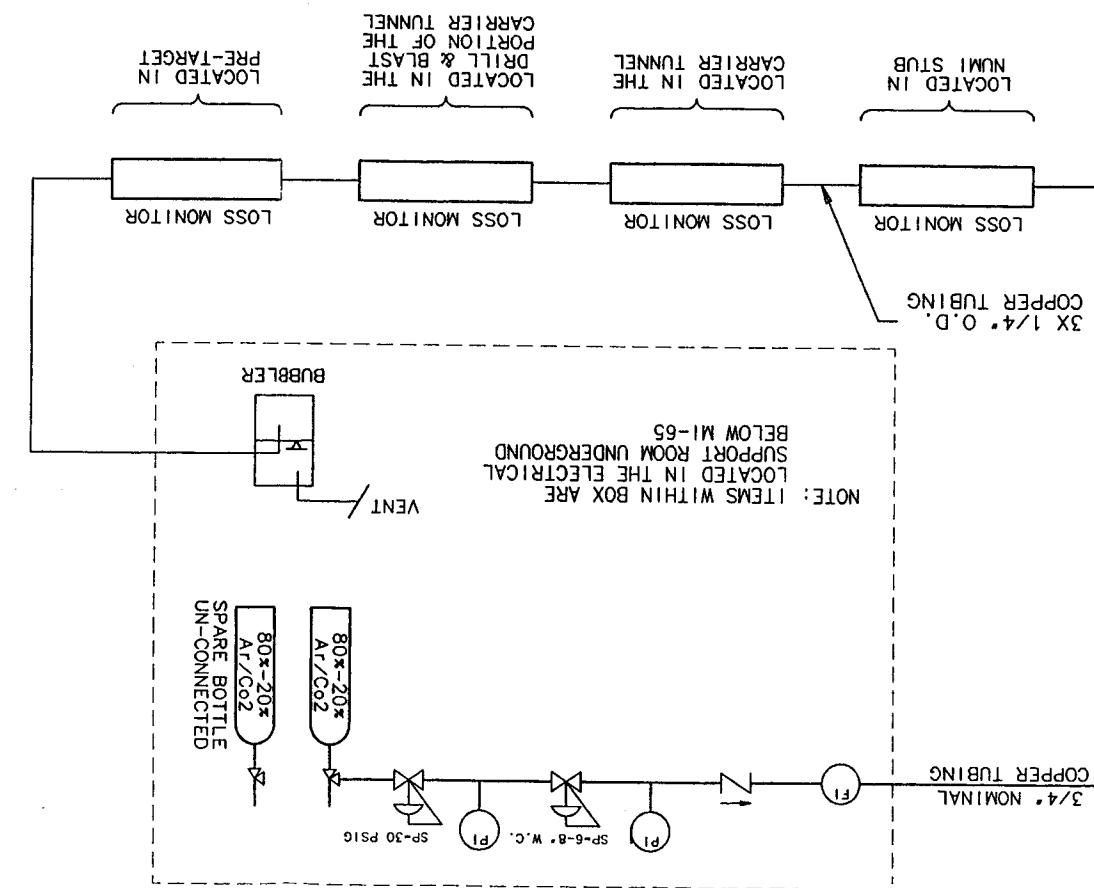
FERMI NATIONAL ACCELERATOR LABORATORY
UNITED STATES GOVERNMENT BY EXCERPT

NMRI OUTFITTING
TARGET HVAC CONTROLS

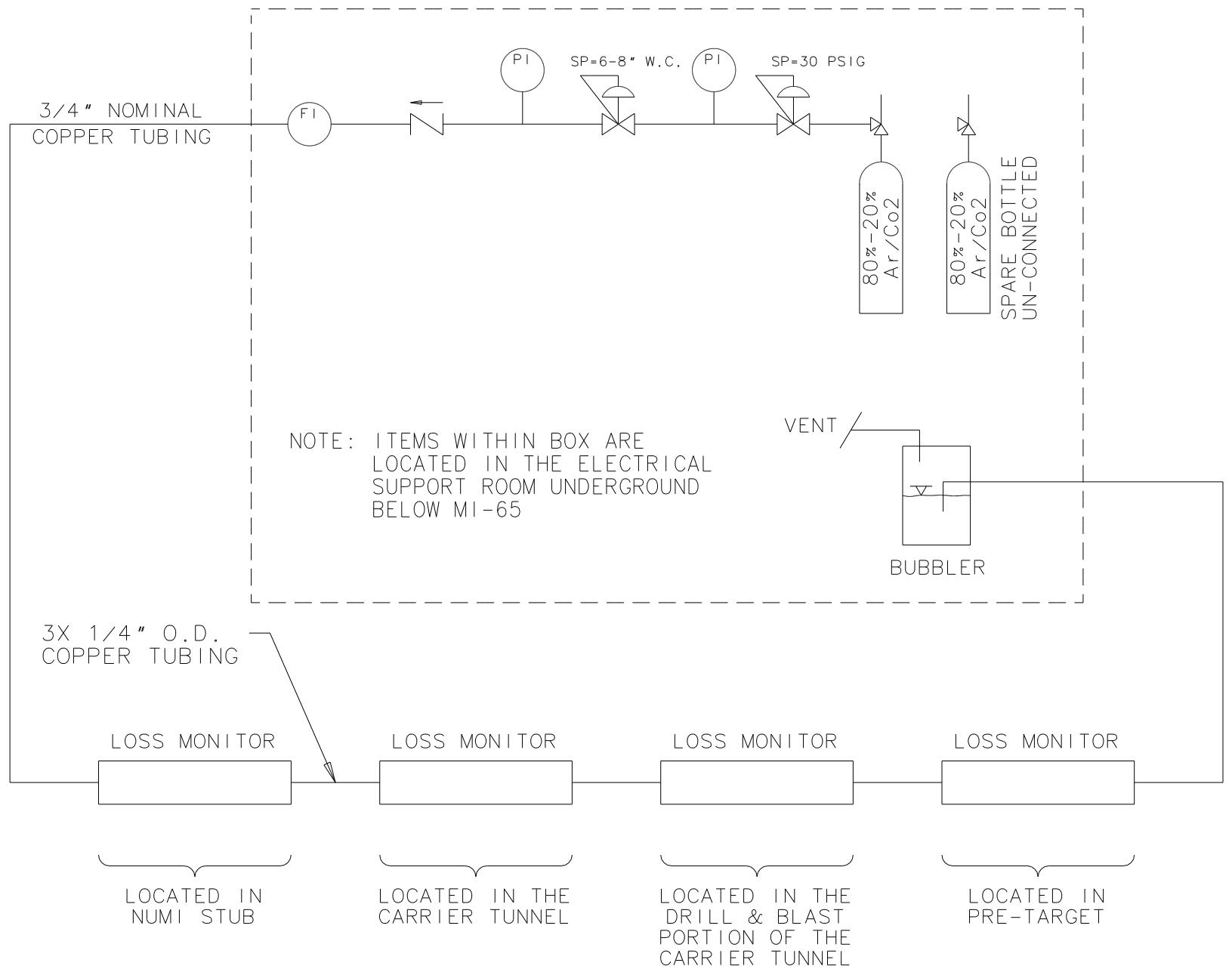
DRAWING NO. 6-7-6 M-13 REV. 2

14 DEC 2004

| | | | | | |
|----------------|--|------------------------------------|--|---|-------------|
| DRAWING NUMBER | | 8875.117-MB-4331 | | GROUP : PPD/MATERIAL DEPARTMENT | DATE WITH : |
| SHEET | | 1 OF 1 | | 10-2004 | |
| REV | | | | XX | |
| DRAWING NUMBER | | D.PUSKHA | | MATERIALS SPECIFICATION | |
| SHEET | | 30-JUL-2004 | | R.R. SMITH | |
| REV | | XXX | | DR. PUSKHA | |
| DRAWING NUMBER | | APPROVED | | APPROVED | |
| SHEET | | 30/JUL/04 | | 30/JUL/04 | |
| REV | | --- | | R.L. SMITH | |
| DRAWING NUMBER | | C.E.CODE | | C.E.CODE | |
| SHEET | | 30-JUL-2004 | | DR. PUSKHA | |
| REV | | --- | | DR. PUSKHA | |
| DRAWING NUMBER | | USD ON | | USD ON | |
| SHEET | | 30/JUL/04 | | 30/JUL/04 | |
| REV | | --- | | DO NOT SCALE DRAWINGS USE VI-S-1948 | |
| DRAWING NUMBER | | MATERIALS SERVICES | | MAINTENANCE, SERVICES | |
| SHEET | | 30-JUL-2004 | | MAX. AL 1000, MM | |
| REV | | --- | | DRAWINGS BASED ON SPECIFICATIONS | |
| DRAWING NUMBER | | UNITED STATES DEPARTMENT OF ENERGY | | FEDERAL NATIONAL ACCELERATOR LABORATORY | |
| SHEET | | 30/JUL-2004 | | NUMI UTILITIES | |
| REV | | --- | | TOTAL LOSS MONITOR GAS SYSTEM SCHEMATIC | |
| DRAWING NUMBER | | 8875.117-MB-4331 | | SCALE | |
| SHEET | | 1 OF 1 | | NONE | |
| REV | | | | DEPARTMENT WITH : | |



| EV | DESCRIPTION | DRAWN | DATE | APPROVED | DATE |
|----|-------------|-------|------|----------|------|
|----|-------------|-------|------|----------|------|



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