



**Particle Physics Division  
Mechanical Department Engineering Note**

Number: PPD doc-1347

Date: April 4, 2011

Project: CMS Upgrade Cooling System Test Design

Title: CMS CO<sub>2</sub> Test Stand Piping Note

Author(s): Erik Voirin

Reviewer(s): Dave Pushka

Key Words: Piping note, 31.3, ASME, 5031

Abstract Summary:

The CMS CO<sub>2</sub> Detector test stand contains piping which runs from the storage tank suspended in Lab C to the South Clean room of Lab C and back again. This document serves to provide details on the piping system and its components. The piping could be subject to up to 1200 psi and a temperature drop from room temperature, down to -73C, (-100F). This piping note analyzes these criteria and shows stress does not exceed the amount allowed by ASME 31.3 code for process piping.

## Table of Contents

1. Engineering Note . . . . .	3
2. Description and Identification . . . . .	5
3. Design Verification . . . . .	9
4. Pressure Containment / Relief System . . . . .	52
5. Welding Information . . . . .	71
6. Welders qualifications . . . . .	73
7. Inspection Plan / Examiners Report . . . . .	86
8. Component Identification . . . . .	98
9. Leak / Pressure Test Procedures . . . . .	178

# **1. FESHM 5031.1 PIPING ENGINEERING NOTE FORM**

Prepared by: **Erik Voirin**

Preparation Date: **2-28-2011**

Piping System Title: **CMS CO2 Cooling Test Stand**

Lab Location: **Lab C**

Location code: **604**

Purpose of system: **Two Phase Carbon Dioxide Cooling Experiments**

Piping System ID Number: **none assigned to date**

Appropriate governing piping code: **ASME B31.1 Category C**

Fluid Service Category (if B31.3): **Category-C**

Fluid Contents: **Carbon Dioxide**

Design Pressure: **1200 psi @ -110F**

Piping Materials: **304 SS**

Drawing Numbers (PID's, weldments, etc.): **9212-750-ME-466879, Appendix E, F**

Designer/Manufacturer: **Fermilab**

Test Pressure: **1320 psig**

Test Fluid: **Nitrogen**

Test Date: **TBD**

## **Statements of Compliance**

Piping system conforms to FESHM 5031.1, installation *is not* exceptional: **Yes**

Piping system conforms to FESHM 5031.1, installation *is* exceptional and has been designed, fabricated, inspected, and tested using sound engineering principles: **N/A**

Reviewed by: \_\_\_\_\_ (Print Name)

Signature: \_\_\_\_\_ Date: \_\_\_\_\_

D/S Head's Signature: \_\_\_\_\_ Date: \_\_\_\_\_

The following signatures are required for exceptional piping systems:

ES&H Director's Signature: \_\_\_\_\_ Date: \_\_\_\_\_

Director's Signature or Designee: \_\_\_\_\_ Date: \_\_\_\_\_

## Pipe Characteristics

Size: **Schedule 10: ½” to 1.5”**: Refer to Drawings

Volume: **~ 15 Gallons**

Relief Valve Information:

Type: **Spring Loaded**

Manufacturer: **Anderson Greenwood**

Set Pressure: not applicable Relief Capacity: **1200 psig**

Relief Design Code: **ASME**

Is the system designed to meet the identified governing code? **Yes**

Fabrication Quality Verification:

Process and Instrumentation diagram appended? **Yes, Appendix E**

Process and Instrumentation component list appended? **Yes, Appendix E**

Is an operating procedure necessary for safe operation? **No**

If 'yes', procedure must be appended.

Exceptional Piping System

Is the piping system or any part of it in the above category? **No**

If "Yes", follow the requirements for an extended engineering note for Exceptional Piping Systems.

Quality Assurance

List vendor(s) for assemblies welded/brazed off site: **None**

List welder(s) for assemblies welded/brazed in-house:

**(Ryan - Welder #3), (Mike Jenniga Welder #2), (Mike Cooper)**

Append welder qualification Records for in-house welded/brazed assemblies.

**Yes, Appendix C**

Append all quality verification records required by the identified code (e.g. examiner's certification, inspector's certification, test records, etc.)

**Yes, Appendix C**

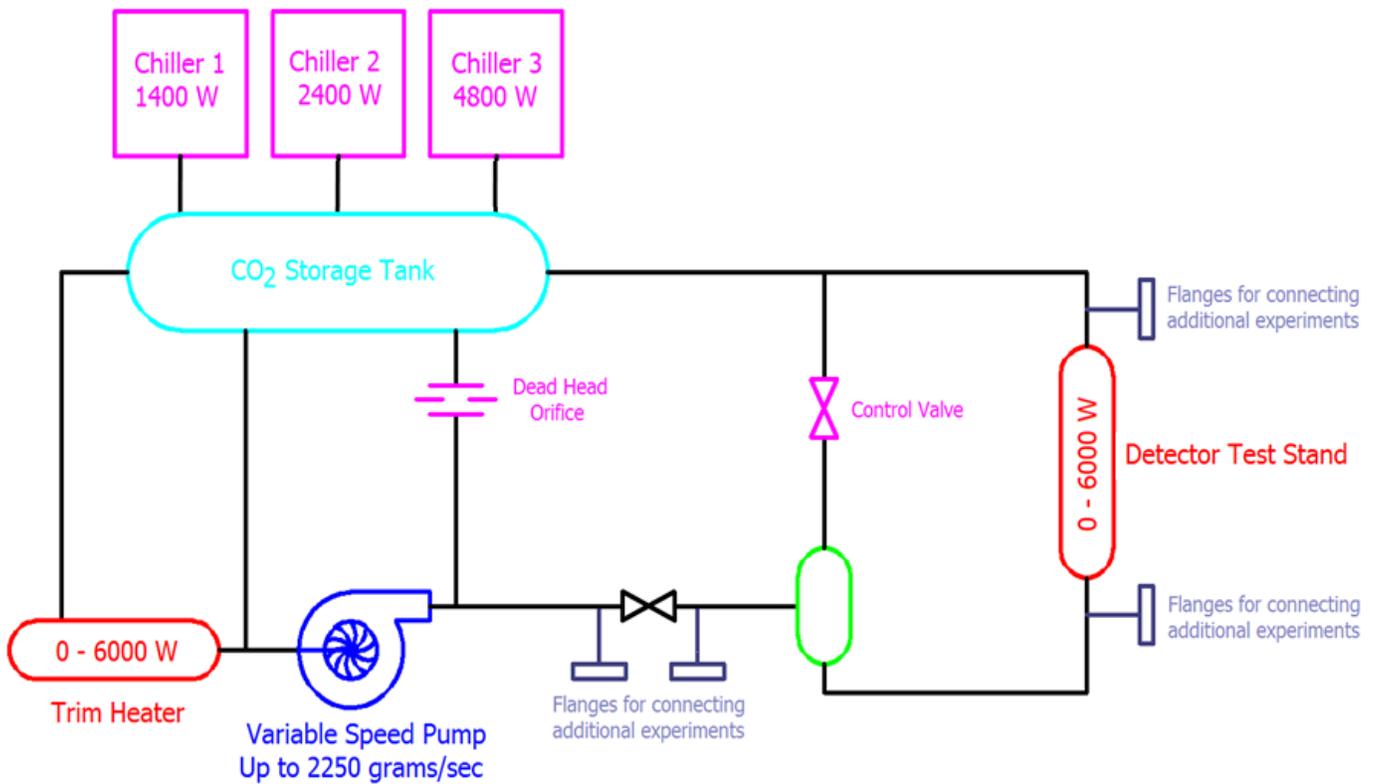
## **2. Description and Identification**

The piping in the CMS CO<sub>2</sub> Cooling Test stand is an experimental setup which will be used to transfer liquid, gaseous, and supercritical CO<sub>2</sub> from the storage tank of the system to the CMS detector test stand and back again. The cooling system uses three commercial chillers using R-404a as a refrigerant to cool the 300 lbs. of Carbon Dioxide in the cooling system. The piping network also contains several pressure vessels each of which serve a different purpose for the cooling system. These vessels are all ASME stamped pressure vessels, all of which have been designed and tested to ASME standards. As seen in the Figure 1, the vessels are the **STORAGE TANK**, **HEATER VESSELS (2)**, and the **PHASE SEPARATION TANK**. Pressure vessel notes for the four vessels have been completed, reviewed, and approved. Links to Engineering Notes: [Storage Tank](#), [Trim Heater Vessel](#), [Test Heater Vessel](#), [Phase Separation Tank](#).

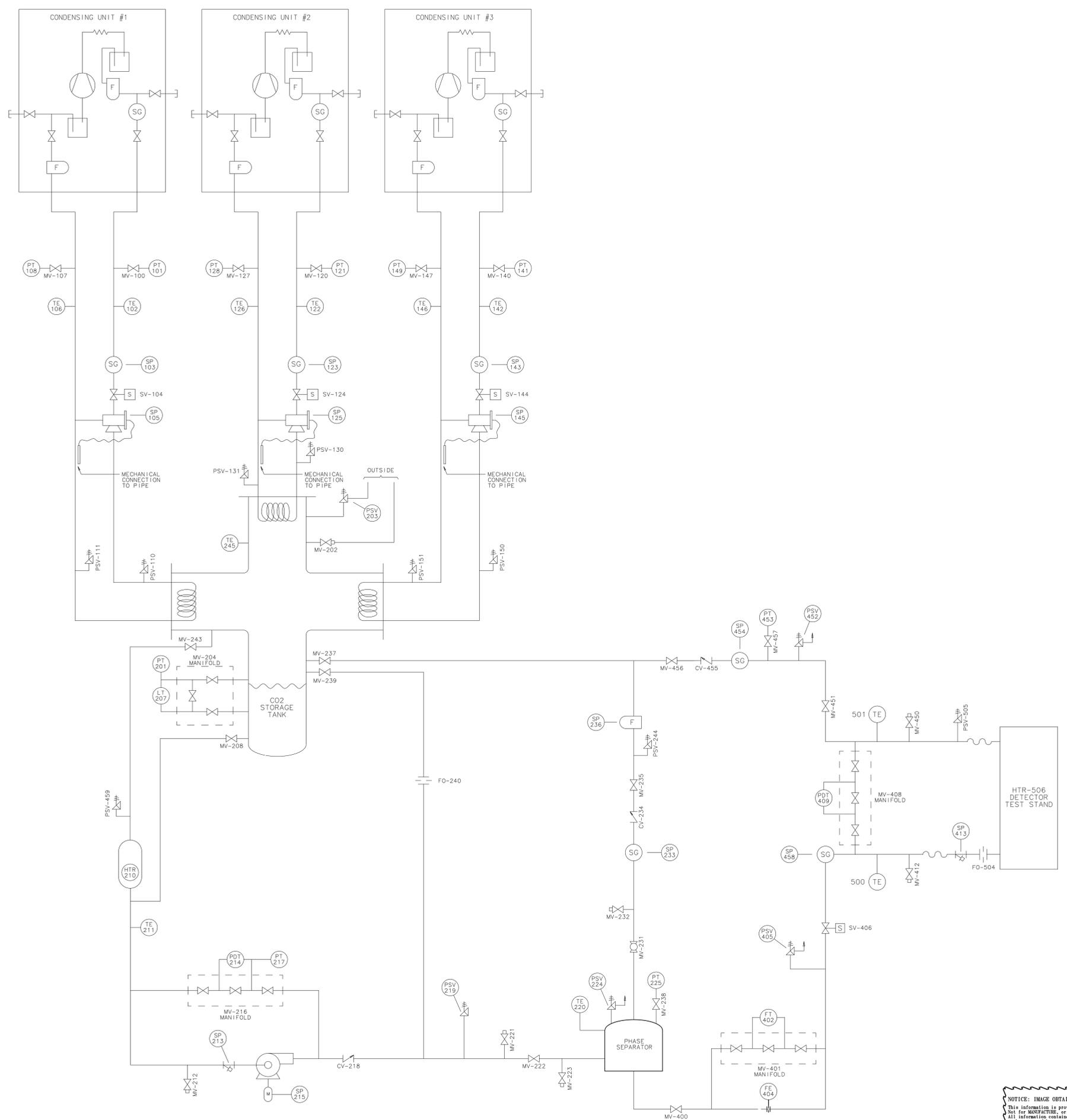
The piping system and all vessels are designed to 1200 psi of internal pressure, and -110F shock temperature. This design pressure was chosen so the system could sit pressurized at room temperature for extended periods of time without the need for evacuating the system. The saturation pressure of CO<sub>2</sub> is 1070 psi at 88F, beyond that temperature CO<sub>2</sub> becomes supercritical and pressures are dependent on density of the fluid due to the volume of containment. The design temperature of the system was chosen as -110F is the temperature in which CO<sub>2</sub> will flash to during a pipe rupture, or other sudden release of pressure down to atmospheric. This temperature was obtained by following a line of constant enthalpy on the CO<sub>2</sub> phase diagram. The piping will be

insulated by 2” thick fiberglass pipe insulation and hung from pipe hangers throughout the building. All piping is grade 304 or 304L stainless steel, schedule 10 or thicker. Nominal Diameters range from ½” to 1- ½”.

A system overview can be seen in Fig.1, which is drawn spatially similar to the piping and instrument diagram which is attached for reference on the following page.



*Fig.1 – CMS CO<sub>2</sub> test stand cooling system overview.*



UNLESS OTHERWISE SPECIFIED	ORIGINATOR	M. ADAMOWSKI	04-FEB-2010
±	DRAWN	J. CATALANIELLO	09-FEB-2010
±	CHECKED	E. VOIRIN	02-AUG-2010
±	APPROVED	E. VOIRIN	02-AUG-2010
1. BREAK ALL SHARP EDGES	USED ON		
2. DO NOT SCALE DRAWING.			
3. DIMENSIONS BASED UPON			
4. MAX. ALL MACH. SURFACES	MATERIAL		
5. DRAWING UNITS:			

FERMI NATIONAL ACCELERATOR LABORATORY  
UNITED STATES DEPARTMENT OF ENERGY

CMS/DETECTORS  
PIXEL  
CMS CO2 COOLING P&ID

SCALE	DRAWING NUMBER	SHEET	REV
NONE	9212.750-ME-466879	1 OF 1	

NOTICE: IMAGE OBTAINED FROM FERMILAB WEB SITE  
This information is provided for REFERENCE use only.  
Not for MANUFACTURE, or DESIGN INFORMATION.  
All information contained in this document represents  
work sponsored by an agency of the U.S. Government.  
Neither the U.S. Government nor any agency thereof,  
nor any employee or officer, makes any warranty, express  
or implied, or assumes any legal liability or  
responsibility for the accuracy, completeness, or  
usefulness of any information, apparatus, product or  
process disclosed, or represents that its use would not  
infringe privately owned rights.

### **3. Design Verification**

The CMS piping meets the requirements of Section 5031.1 of the Fermilab ES&H Manual. This section states that this piping system falls under the category of Normal Fluid Service and shall adhere to the requirements of the ASME Process Piping Code B31.3.

**Materials:**

The piping is fabricated from 304 or 304L stainless steel tube and pipe. The lowest allowable stress for both of these materials from Table A-1 of ASME B31.3 is 16,700 psi. The CO<sub>2</sub> lines are primarily made of schedule 10 pipe.

The piping will be operated at -40C (-40F) minimum. This is above the minimum temperature listed for 304/316 stainless steel pipe or tube (19 K). According to Table 323.2.2 of the Code, impact testing is not required for these austenitic stainless steels. (Reference “Bo LarTPC Cryostat Piping System Engineering Note” by T. Tope)

The minimum possible temperature would happen under a pipe rupture, where the pipe could reach temperatures down to -73C (-100F) due to the sudden expansion of the CO<sub>2</sub> and flashing of the fluid down to this Temperature. This is above the minimum temperature listed for 304/316 stainless steel pipe or tube (19 K). According to Table 323.2.2 of the Code, impact testing is not required for these austenitic stainless steels. (Reference “Bo LarTPC Cryostat Piping System Engineering Note” by T. Tope)

### **Stress analysis:**

Calculations were done for stress due to pressure, pipe weight, and thermal contraction. The design uses standard tubing and fittings, which meet specifications of ASTM A403, and are therefore rated to the same temperature and pressure as the same pipe size and schedule number according to ASME 31.3.

The minimum thickness of the pipes is evaluated using the procedures in 304.1.2(a) of ASME B31.3. All trapped volume relief valves are set at 1200 psig. The minimum tube thickness for seamless or longitudinally welded piping for  $t < D/6$  is given by the equation:

$$t = \frac{PD}{2(SEW + PY)}$$

Where:  $t$  = wall thickness,

$P$  = internal design pressure

$D$  = outside diameter (manufacturer's nominal value is used)

$S$  = allowable stress from table A-1 = 16.7 ksi

$E$  = quality factor from table A-1B = 1 for seamless, 0.8 for clamshell

$W$  = weld joint strength reduction factor = 1 for seamless tubing, 0.8 for clamshell  
per 302.3.4.

$Y$  = coefficient from Table 304.1.1 = 0.4

The piping system contains four sizes of schedule 10 piping: ½”, ¾”, 1”, and 1-½”  
 Calculations for the stresses seen in these four pipe sizes in order due to the design  
 pressure of 1200 psi are as follows:

$$t = \frac{P \cdot D}{2 \cdot (S \cdot E \cdot W + P \cdot Y)} \text{ solve, } S \rightarrow \frac{\frac{D \cdot P}{t} - 2 \cdot P \cdot Y}{2 \cdot E \cdot W}$$

$$D := \begin{pmatrix} 0.840 \\ 1.050 \\ 1.315 \\ 1.9 \end{pmatrix} \text{ in} \quad t := \begin{pmatrix} 0.083 \\ 0.083 \\ 0.109 \\ 0.109 \end{pmatrix} \text{ in} \quad W := 1 \quad Y := 0.4$$

$$E := 1 \quad P := 1200 \text{ psi}$$

$$S := \frac{\frac{D \cdot P}{t} - 2 \cdot P \cdot Y}{2 \cdot E \cdot W} = \begin{pmatrix} 5592 \\ 7110 \\ 6759 \\ 9979 \end{pmatrix} \text{ psi}$$

This shows a stress due to internal pressure below the allowable limit of 16.7 ksi.  
 Stresses seen were between 5592 psi for the smallest pipe size of ½”, up to 9979 psi seen  
 in the largest pipe size of 1-½”. Calculations for thermal contraction are much more  
 involved, so ANSYS was used to compute these stresses, see Appendix A for details on  
 this as well as pipe weight and secondary stress analysis.

# Route descriptions, calculations, and analyses

## Section Contents:

FEA Boundary Conditions

FEA simple model testing

Pipe section weight calculation

Section 1

Section 2

Section 3

Section 4

Section 5

Sections 3, 4, and 5 combined

Section 6

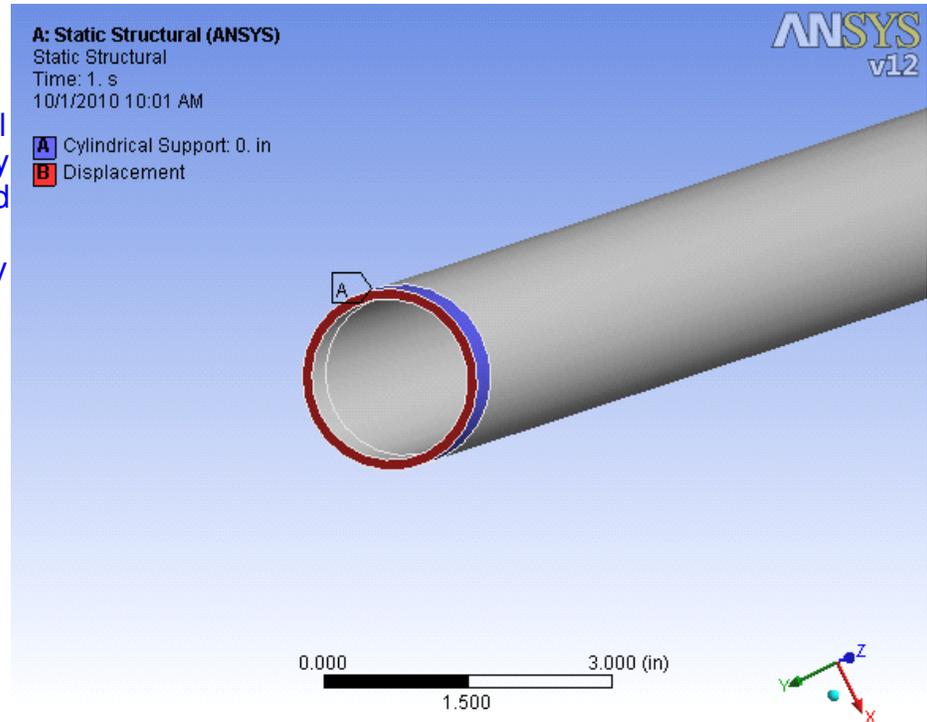
Pressure Vessel Block off Plates

## FEA / Boundary condition Testing

Ansys is a very powerful FEA program and fully capable of performing any thermal or structural analysis, yet it is generic in the respects it is not specifically designed for piping systems. boundary condition selection must be made to match real world fixing points, supports, weights, and such. Piping programs have predefined "pipe hanger supports" "flanged connections" ect. where in Ansys these must be simulated. This report explains boundary conditions for the analyses and conducts simple Calculations which can be checked with hand calculations in order to assure correct boundary conditions and accuracy

Since the ends will be flanged connections, they will be somewhat fixed position wise, but the cylinder will be able to expand and contract radially and axially since the flange will expand and contract due to temperature just as the pipe will. The flange would only assist in holding internal pressure, so the free radial expansion is conservative for a pressure application.

The pipe shown in the figure has the displacement set to zero in the Z direction and is free in all others. The cylindrical support is fixed tangentially and free in all others.



## Hand Calculations for Stress / Boundary condition Testing

Pipe is grade 304 Stainless Steel

### Temperature Change Stress

Coefficient of Thermal Expansion

$$\alpha := \frac{1.7 \cdot 10^{-5}}{\text{K}}$$

Modulus of Elasticity

$$E := 1.93 \cdot 10^{11} \text{ Pa}$$

Initial Temperature

$$T_i := 71.6$$

Final Temperature

$$T_f := 20$$

$$\Delta T := (T_i - T_f) \left( \frac{5}{9} \right) \text{ K}$$

Thermal strain

$$\epsilon := \alpha \cdot \Delta T = 4.873 \times 10^{-4}$$

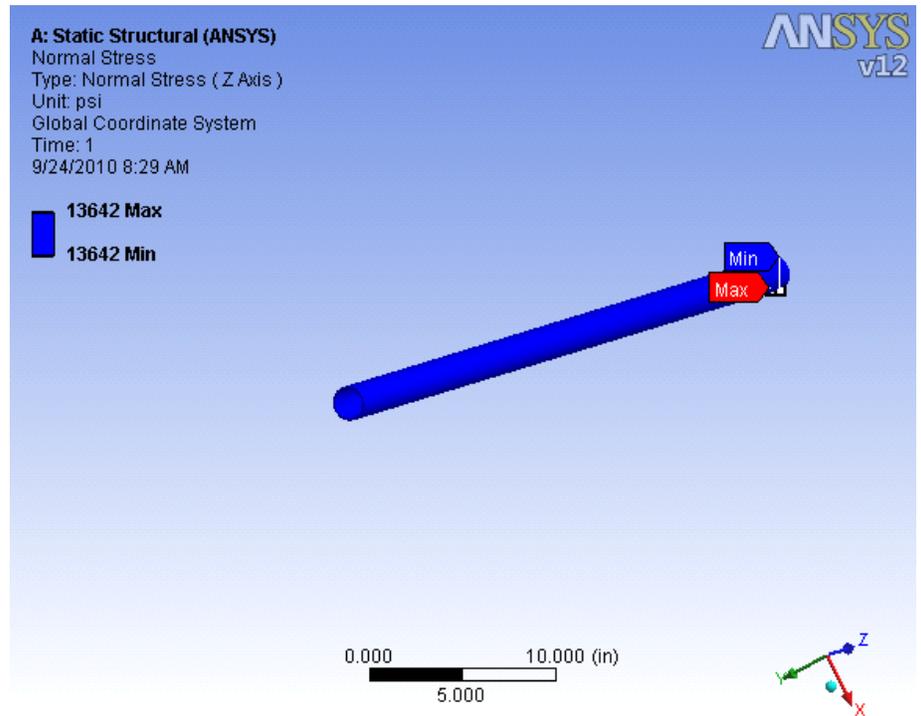
Using Duhamel Neumann form of Hooke's law, the deformation is zero so the mechanical strain must equal the thermal strain.

## Stress

$$\epsilon \cdot E = \sigma \quad \sigma := \epsilon \cdot E = 13642 \cdot \text{psi}$$

Ansys computes:

Boundary conditions applicable for temperature induced stress



## Stress due to weight of pipe

$$\text{Weight} := 50 \text{ lbf}$$

$$D_o := 1.9 \text{ in} \quad D_i := 1.682 \text{ in}$$

$$I := \frac{\pi}{64} \cdot (D_o^4 - D_i^4) = 0.247 \cdot \text{in}^4$$

$$c := \frac{D_o}{2} = 0.95 \cdot \text{in}$$

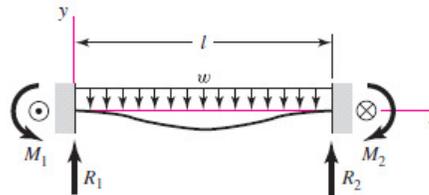
$$\text{Length} := 48 \text{ in}$$

$$w := \frac{\text{Weight}}{\text{Length}} = 1.042 \cdot \frac{\text{lbf}}{\text{in}}$$

$$y_{\text{max}} := \frac{w \cdot \text{Length}^4}{384 E \cdot I} = 0.00208 \cdot \text{in}$$

$$M := \frac{w \cdot \text{Length}^2}{12} = 200 \cdot \text{lbf} \cdot \text{in}$$

## 16 Fixed supports—uniform load



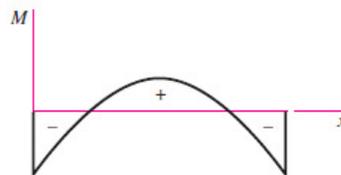
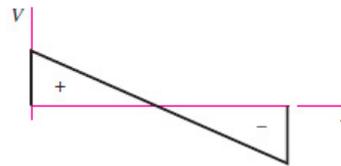
$$R_1 = R_2 = \frac{wl}{2} \quad M_1 = M_2 = \frac{wl^2}{12}$$

$$V = \frac{w}{2}(l - 2x)$$

$$M = \frac{w}{12}(6lx - 6x^2 - l^2)$$

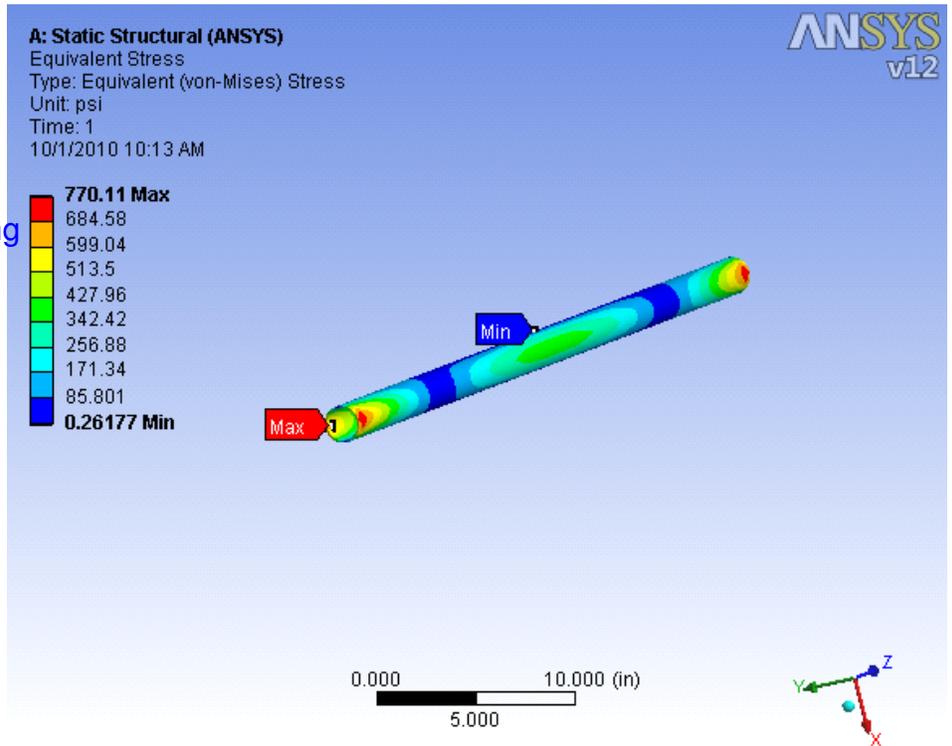
$$y = -\frac{wx^2}{24EI}(l - x)^2$$

$$y_{\text{max}} = -\frac{wl^4}{384EI}$$



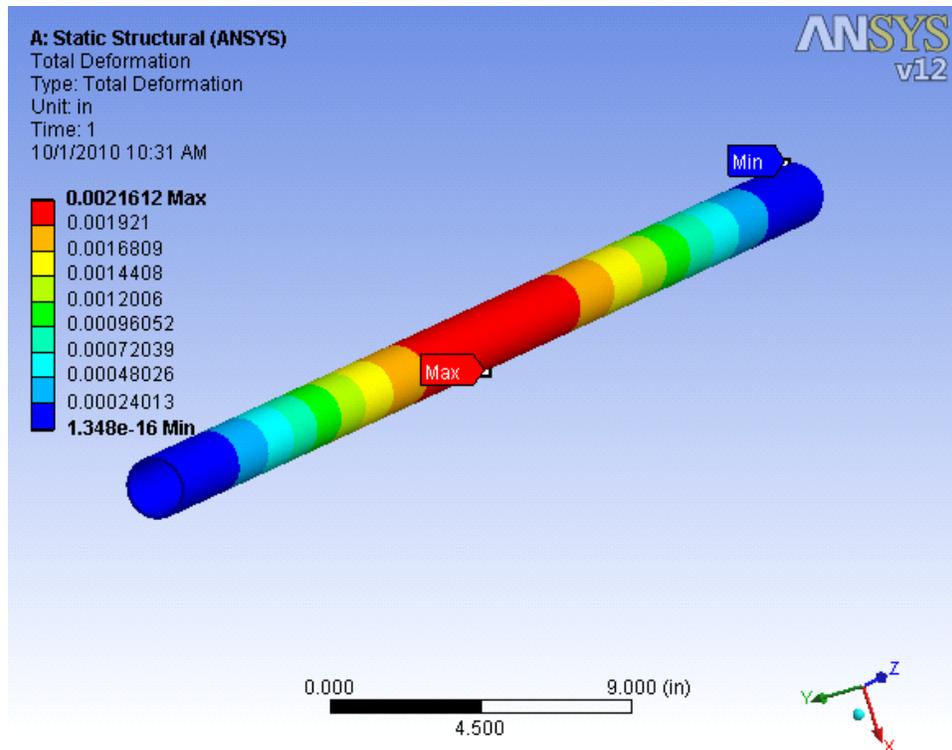
Boundary condition applicable for bending

$$\sigma := \frac{M \cdot c}{I} = 769.795 \cdot \text{psi}$$



Boundary condition app. for deflection

$$\text{deflection} := y_{\max} = 0.002084 \cdot \text{in}$$

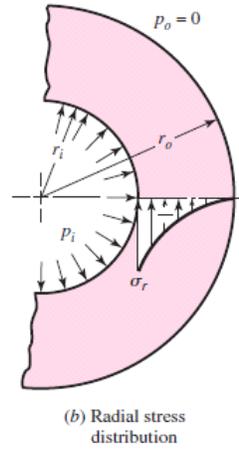
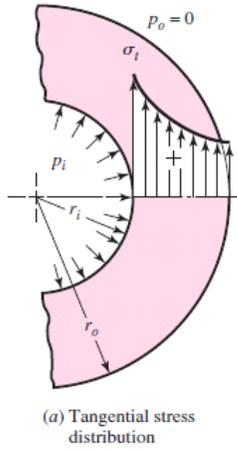


## Stress due to internal Pressure

$$r_i := \frac{D_i}{2} \quad r_o := \frac{D_o}{2} \quad p_i := 1200 \text{ psi}$$

$$\sigma_t := \frac{r_i^2 \cdot p_i}{r_o^2 - r_i^2} \cdot \left( 1 + \frac{r_o^2}{r_i^2} \right) = 9895 \cdot \text{psi}$$

$$\sigma_r := \frac{r_i^2 \cdot p_i}{r_o^2 - r_i^2} \cdot \left( 1 - \frac{r_o^2}{r_i^2} \right) = -1200 \cdot \text{psi}$$



$$\sigma_t = \frac{r_i^2 p_i}{r_o^2 - r_i^2} \left( 1 + \frac{r_o^2}{r_i^2} \right)$$

$$\sigma_r = \frac{r_i^2 p_i}{r_o^2 - r_i^2} \left( 1 - \frac{r_o^2}{r_i^2} \right)$$

$$\nu := 0.30$$

$$\epsilon_x = \frac{1}{E} [\sigma_x - \nu(\sigma_y + \sigma_z)]$$

$$\epsilon_z := 0$$

$$\epsilon_z = \frac{1}{E} (\sigma_z - \nu(\sigma_t + \sigma_r))$$

$$\epsilon_y = \frac{1}{E} [\sigma_y - \nu(\sigma_x + \sigma_z)]$$

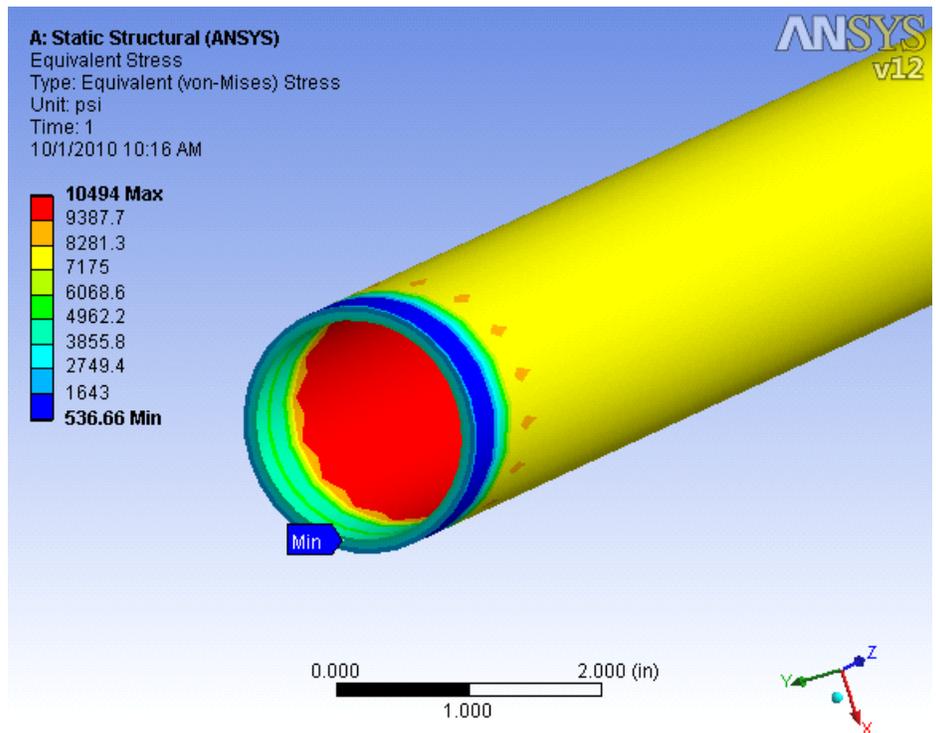
$$\sigma_z := \epsilon_z \cdot E + \nu \cdot (\sigma_t + \sigma_r) = 2609 \cdot \text{psi}$$

$$\epsilon_z = \frac{1}{E} [\sigma_z - \nu(\sigma_x + \sigma_y)]$$

$$\text{vonMises} := \left[ \frac{(\sigma_t - \sigma_z)^2 + (\sigma_z - \sigma_r)^2 + (\sigma_r - \sigma_t)^2}{2} \right]^{\frac{1}{2}} = 9765 \cdot \text{psi}$$

## Boundary condition app. for pressure

$$\text{Pressure} := \text{vonMises} = 9.765 \times 10^3 \cdot \text{psi}$$



## Pipe supports

Since Ansys WB does not have pipe supports, judgement was used in determining the type of supports to use.

The pipe will be supported by pipe hangers and will be inside 2" fiberglass insulation. Physical examination of the insulation showed a square inch of the insulation could be compressed from two to 1 inches with about 10-20 lbs of pressure. Therefore an elastic support with a foundation stiffness of 15lb/in<sup>3</sup> was inserted on the pipe at the locations of the pipe cradles.

Weight of Pipe on other components for dead weight analysis:

$$OD_{1.5} := 1.9\text{in}$$

$$AO_{1.5} := \frac{\pi}{4} \cdot OD_{1.5}^2$$

$$ID_{1.5} := 1.682\text{in}$$

$$AI_{1.5} := \frac{\pi}{4} \cdot ID_{1.5}^2$$

$$OOD_{1.5} := OD_{1.5} + 4\text{in}$$

$$AOO_{1.5} := \frac{\pi}{4} \cdot OOD_{1.5}^2$$

$$A_{1.5} := AO_{1.5} - AI_{1.5} = 0.613 \cdot \text{in}^2$$

$$OD_1 := 1.315\text{in}$$

$$AO_1 := \frac{\pi}{4} \cdot OD_1^2$$

$$ID_1 := 1.097\text{in}$$

$$AI_1 := \frac{\pi}{4} \cdot ID_1^2$$

$$OOD_1 := OD_1 + 4\text{in}$$

$$AOO_1 := \frac{\pi}{4} \cdot OOD_1^2$$

$$A_1 := AO_1 - AI_1 = 0.413 \cdot \text{in}^2$$

## Densities of Components

## Weight per foot of components

$$\rho_{SS} := 7500 \frac{\text{kg}}{\text{m}^3} = 0.271 \cdot \frac{\text{lb}}{\text{in}^3}$$

$$W_{SS_{1.5}} := \rho_{SS} \cdot A_{1.5} = 1.994 \cdot \frac{\text{lb}}{\text{ft}}$$

$$W_{SS_1} := \rho_{SS} \cdot A_1 = 1.343 \cdot \frac{\text{lb}}{\text{ft}}$$

$$\rho_{CO_2} := 1000 \frac{\text{kg}}{\text{m}^3} = 0.036 \cdot \frac{\text{lb}}{\text{in}^3}$$

$$W_{CO_2_{1.5}} := \rho_{CO_2} \cdot AI_{1.5} = 0.963 \cdot \frac{\text{lb}}{\text{ft}}$$

$$W_{CO_2_1} := \rho_{CO_2} \cdot AI_1 = 0.41 \cdot \frac{\text{lb}}{\text{ft}}$$

$$\rho_{Ins} := 3 \frac{\text{lb}}{\text{ft}^3} = 0.0017 \cdot \frac{\text{lb}}{\text{in}^3}$$

$$W_{Ins_{1.5}} := \rho_{Ins} \cdot (AOO_{1.5} - AO_{1.5}) = 0.511 \cdot \frac{\text{lb}}{\text{ft}}$$

$$W_{Ins_1} := \rho_{Ins} \cdot (AOO_1 - AO_1) = 0.434 \cdot \frac{\text{lb}}{\text{ft}}$$

## Total weight of CO<sub>2</sub> filled, and insulated 1.5" pipe

$$W_{1.5} := W_{SS_{1.5}} + W_{CO_2_{1.5}} + W_{Ins_{1.5}} = 3.468 \cdot \frac{\text{lb}}{\text{ft}}$$

$$W_1 := W_{SS_1} + W_{CO_2_1} + W_{Ins_1} = 2.186 \cdot \frac{\text{lb}}{\text{ft}}$$

## Weight of particular pipe sections

$$\text{Section1} := W_{1.5} \cdot 291\text{in} = 84.097 \cdot \text{lb}$$

$$\text{Section4} := W_1 \cdot 962.13\text{in} = 175.304 \cdot \text{lb}$$

$$\text{Section2} := W_{1.5} \cdot 262\text{in} = 75.716 \cdot \text{lb}$$

$$\text{Section3} := W_1 \cdot 688\text{in} = 125.357 \cdot \text{lb}$$

$$\text{Section5} := W_1 \cdot 100\text{in} = 18.22 \cdot \text{lb}$$

## Pipe Section 1

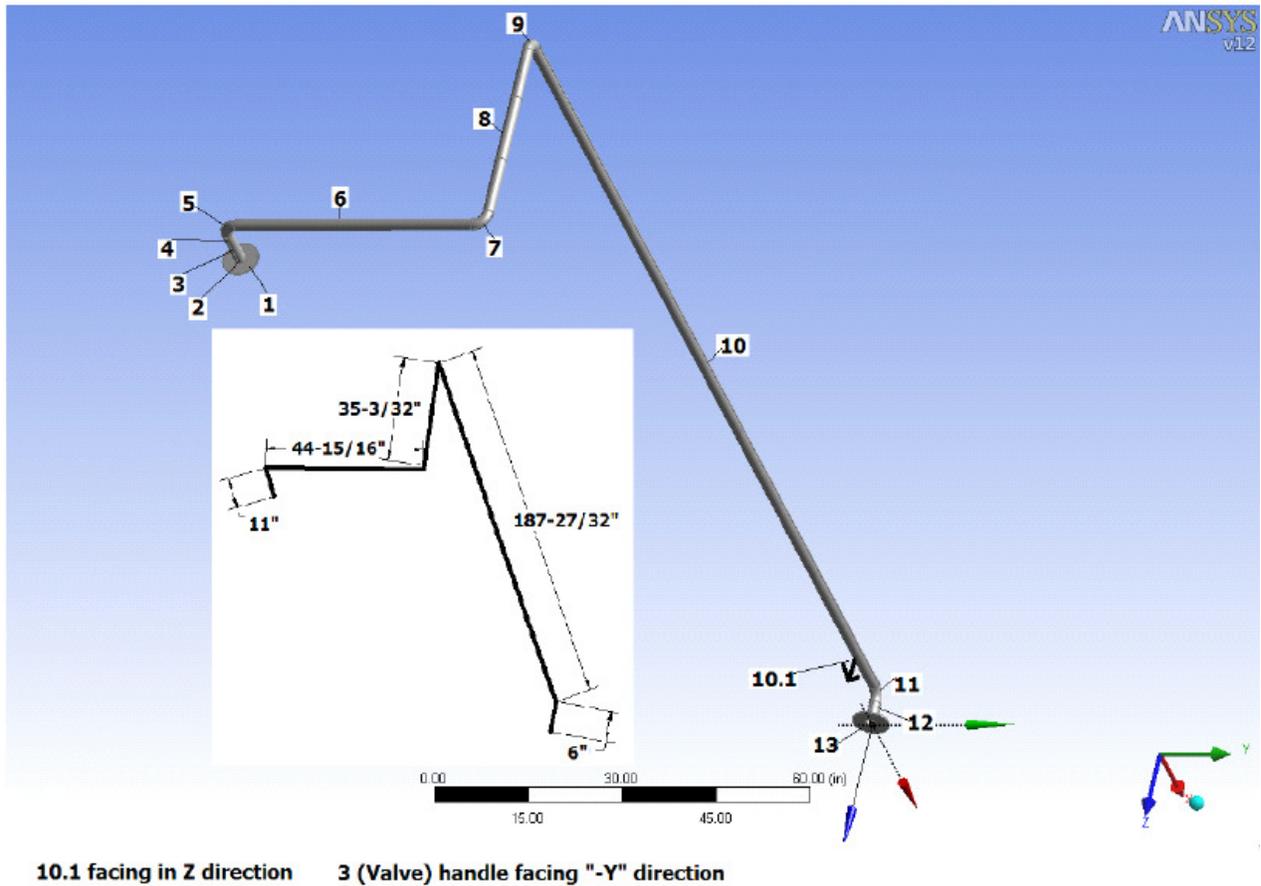
Each section was modeled and then analyzed in Ansys with the described boundary conditions and subjected to numerous loads, weight of pipe was included in each analysis:

- 1.) Temperature drop from 71.6F to -110F
- 2.) Internal Pressure of 1200 psig
- 3.) Operating Temperature of -40F and Pressure of 131 psig

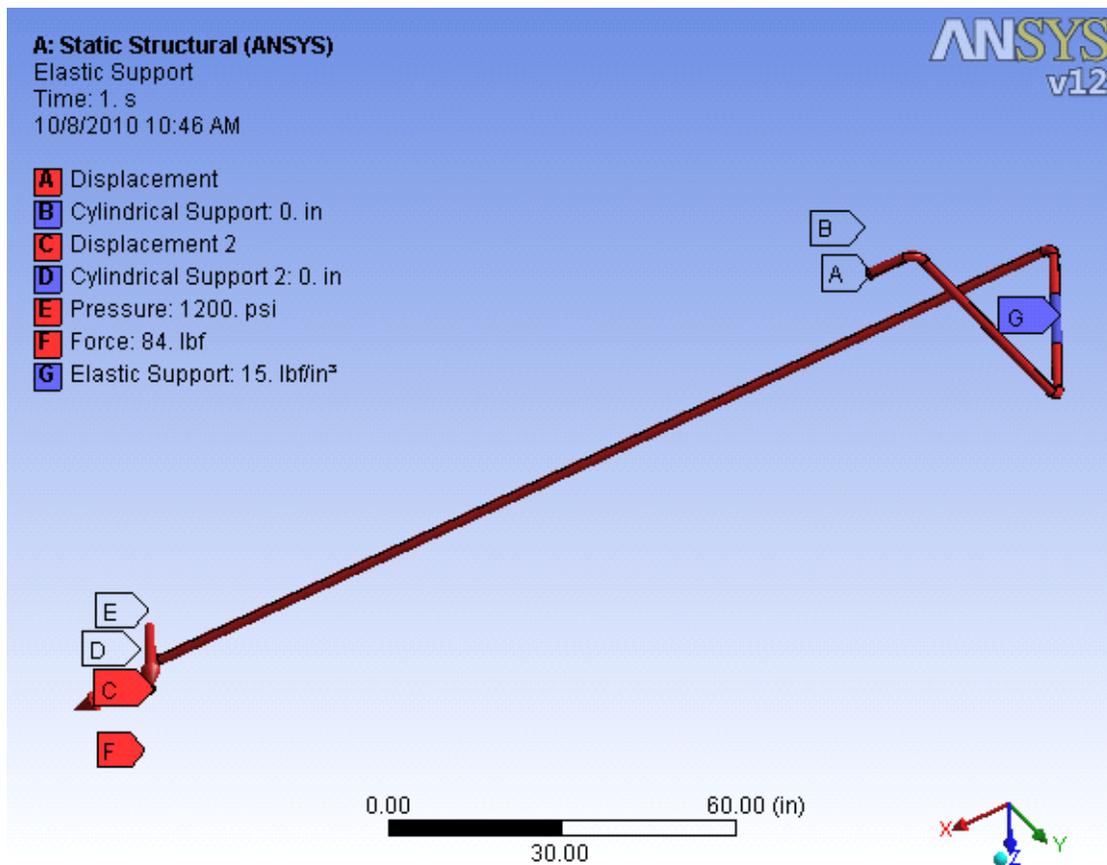
Material and equipment descriptions:

Assembly 1						
Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1.5	1	600# flange	0.875"			1480
1.5	2	Pipe	1.88	SW-flange	SW- valve	2000
1.5	3	Valve	5			1480
1.5	4	Pipe	1	SW- valve	Butt-elbow	2000
1.5	5	elbow	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	6	Pipe	40.44	Butt-elbow	Butt-elbow	2000
1.5	7	elbow	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	8	Pipe	30.85	Butt-elbow	Butt-elbow	2000
1.5	9	elbow	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	10	Pipe	183.35	Butt-elbow	Butt-elbow	2000
1	10.1	Saddle fitting				3000
1	10.2	relief valve				10000 psi burst
1	10.3	fitting	1			3000
1	10.4	Pipe	16	Butt Fitting	Butt elbow	3000
1	10.5	elbow	1.5	Butt-Pipe		3000
1.5	11	elbow	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	12	Pipe	2.88	Butt-elbow	SW-flange	2000
1.5	13	600# flange	0.875"			1480

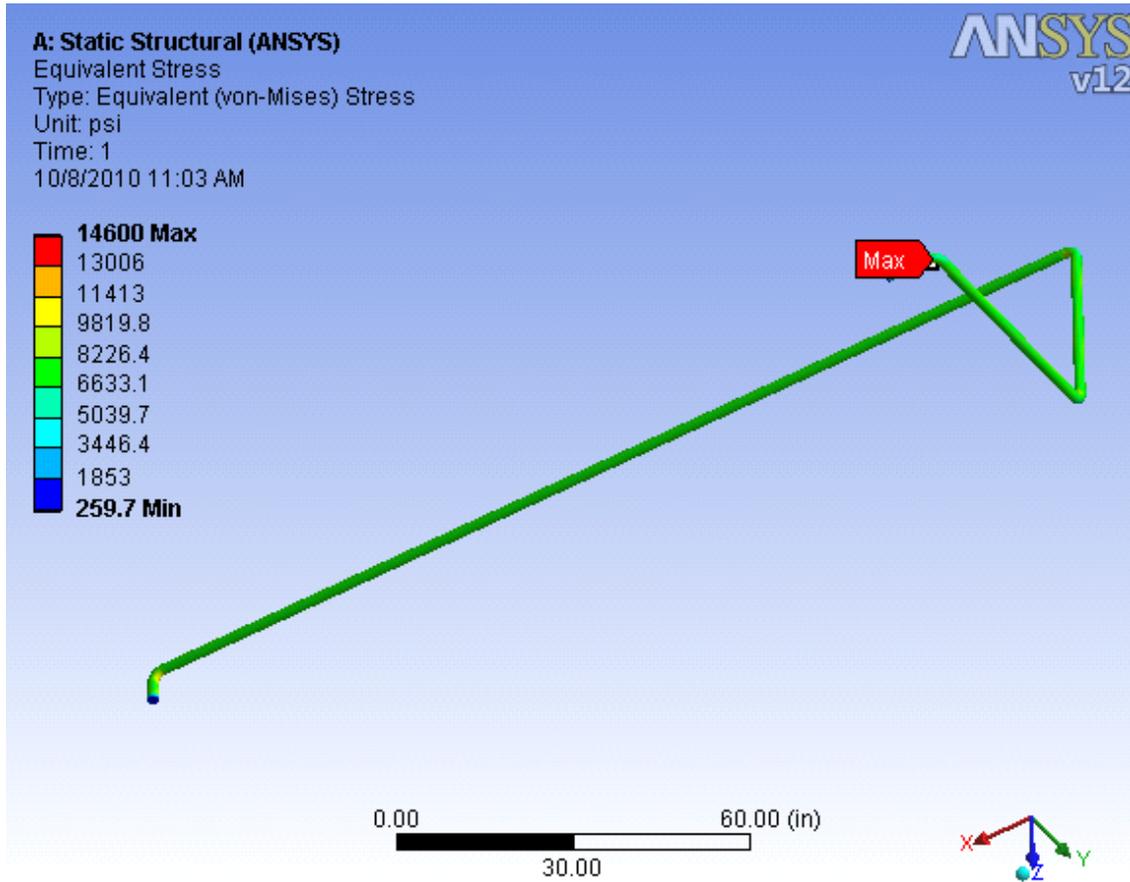
## Physical Description / Visual representation



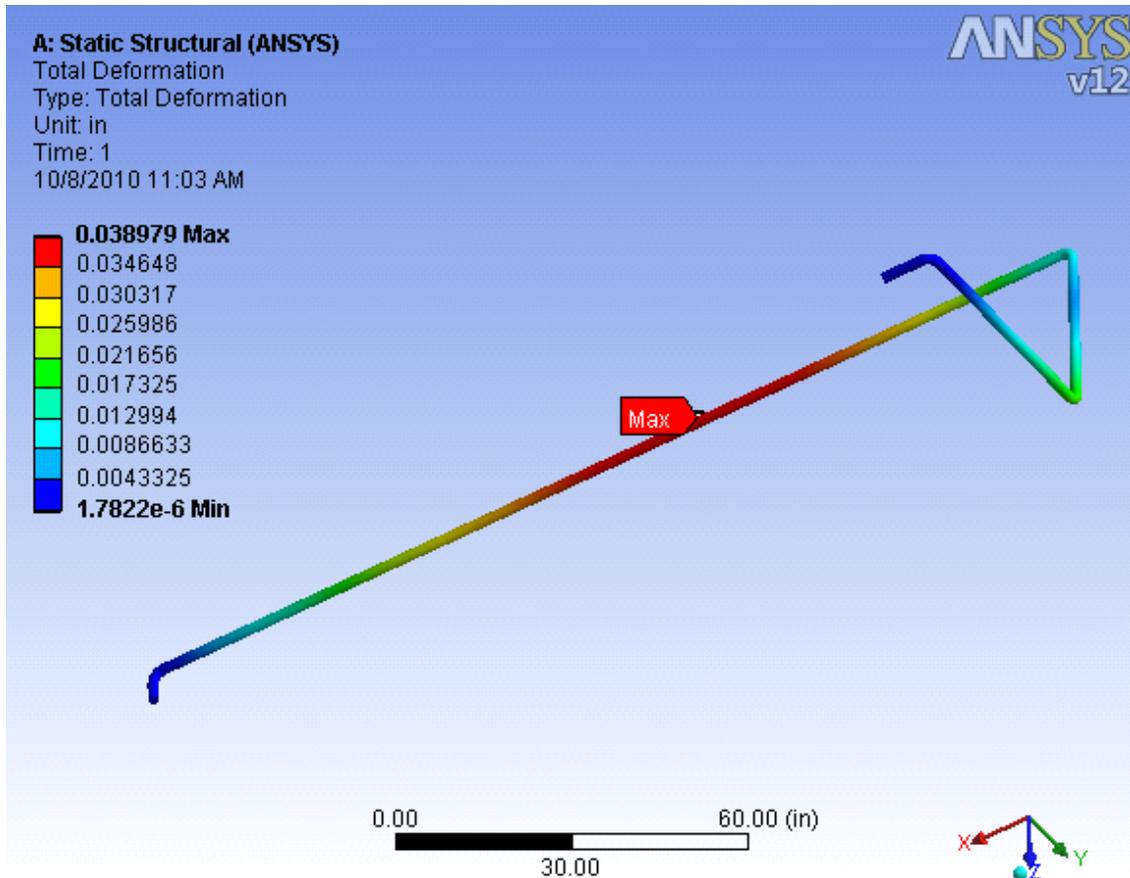
## Boundary Conditions Internal Pressure



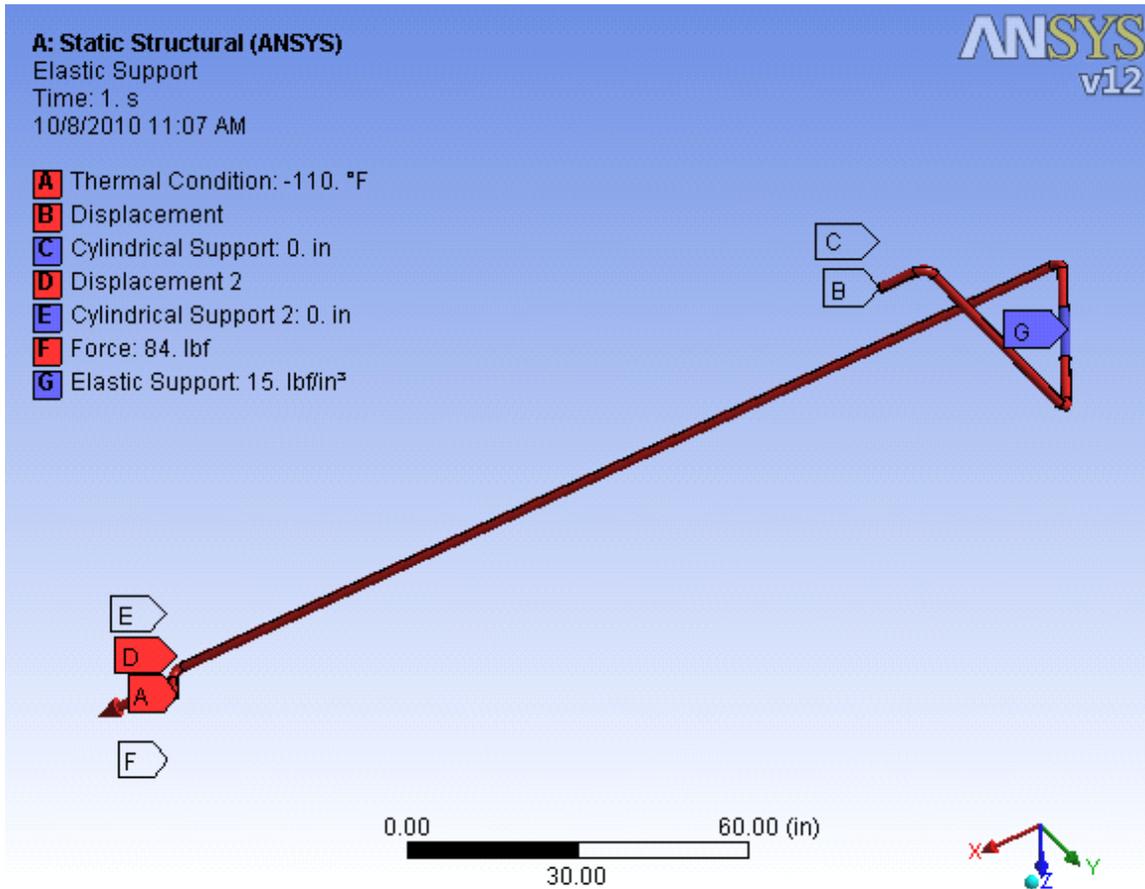
## Stress Plot



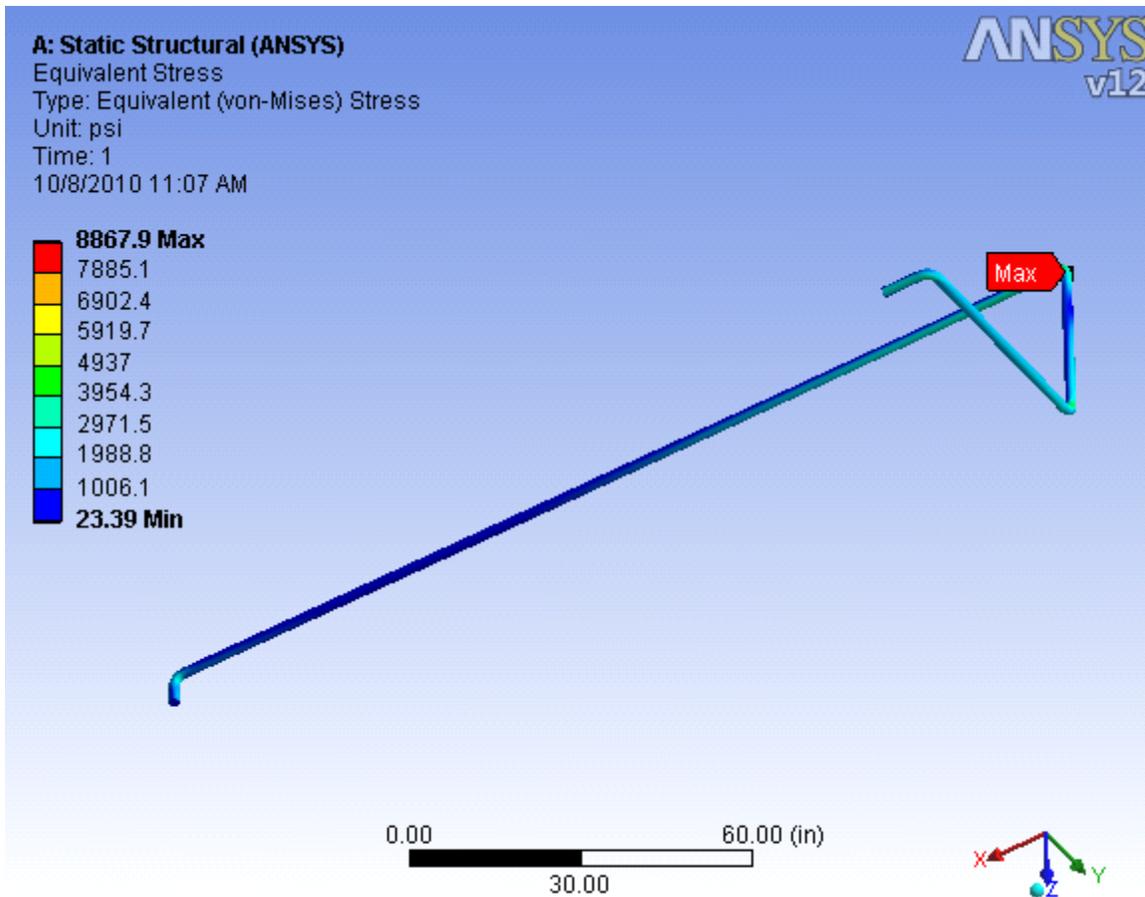
## Deformation Plot



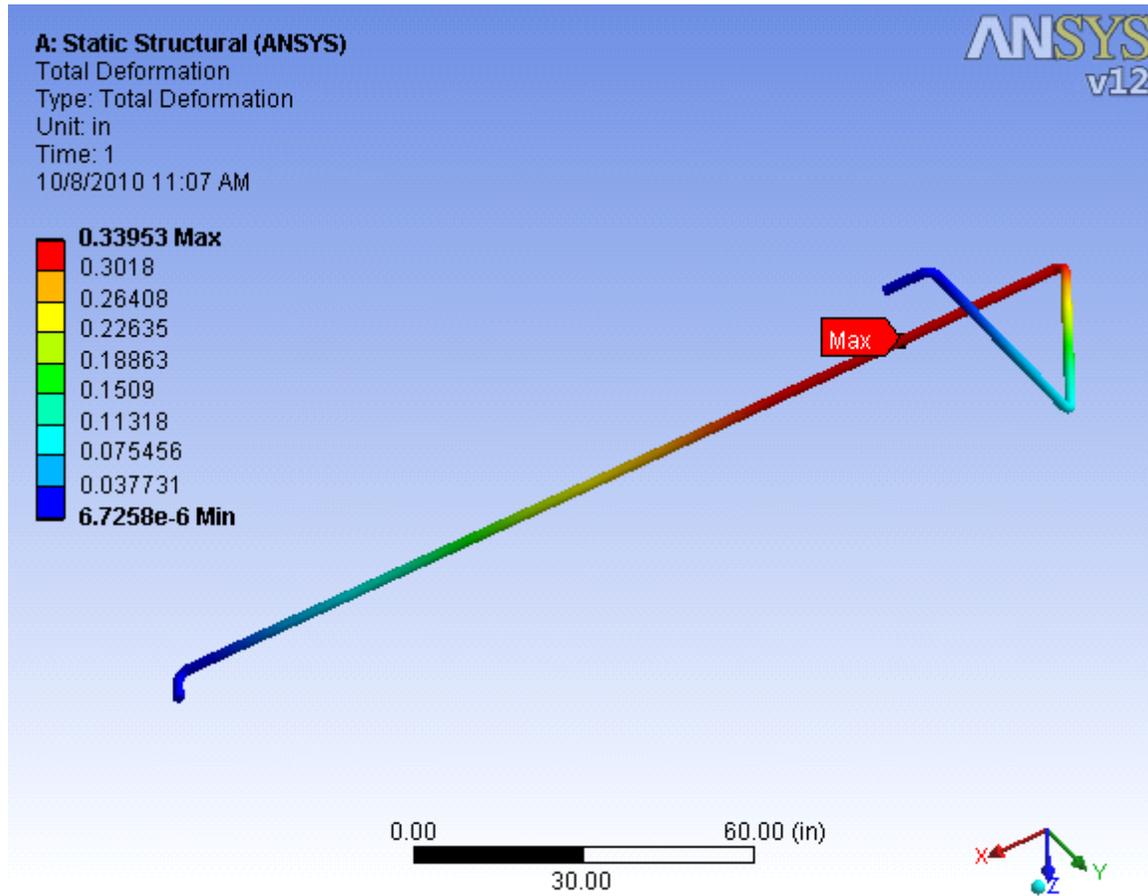
## Boundary Conditions



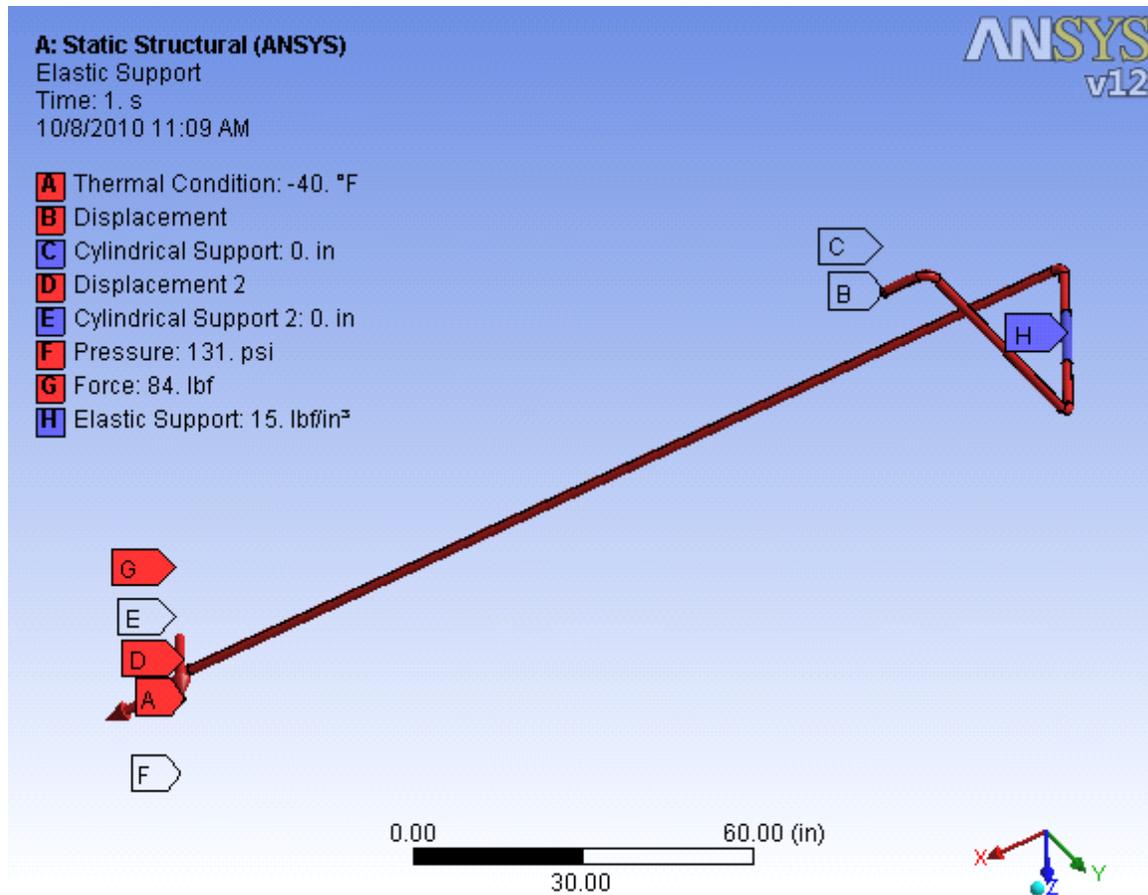
## Stress Plot



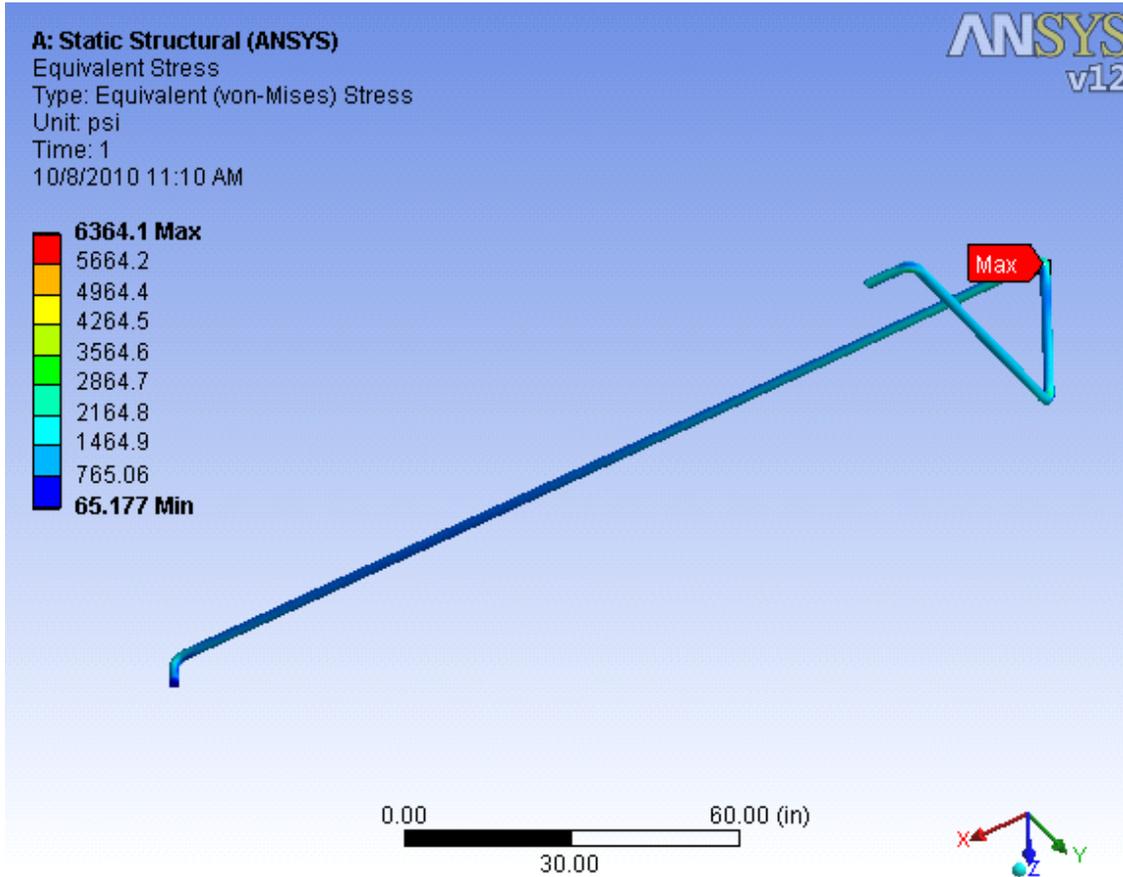
## Deformation Plot



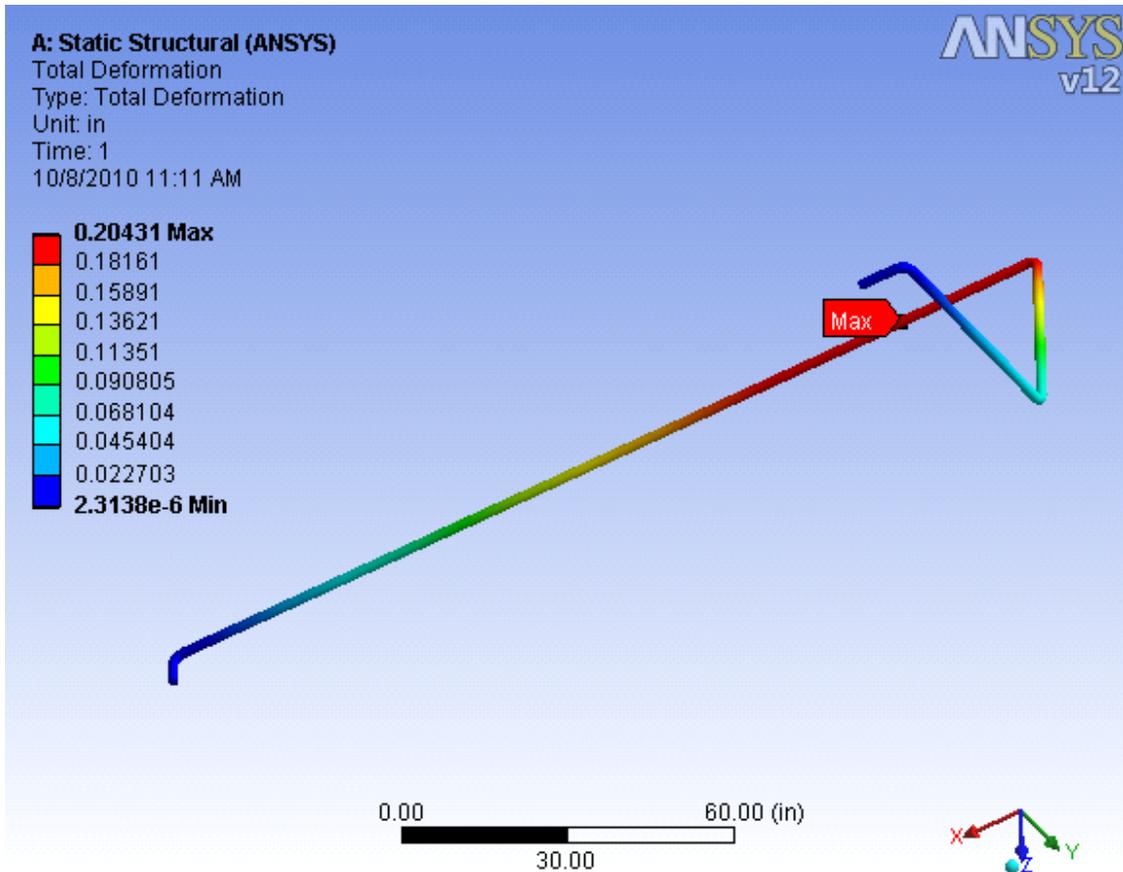
## Boundary Conditions Temperature drop to -110F



## Stress Plot



## Deformation Plot



## Result Summary For section #1

The stress levels fall below the allowed 16.7 ksi in ASME 31.3 process piping code. Fittings are designed thicker than the pipe itself, and are rated for the temperature and pressure and allowed by 31.3. Stress levels in the fittings should be somewhat lower than shown in the ansys model since they are modeled the same thickness as the pipe itself for a conservative approach. Deformation levels are reasonable and could easily be allowed by the pipe insulation and hangers without constraint. One can see from these results the operating temperature and pressure is low with respect to the two other extreme cases. Analysis for operating procedure will not be shown for additional pipe sections.

## Pipe Section 2

Each section was modeled and then analyzed in Ansys with the described boundary conditions and subjected to numerous loads:

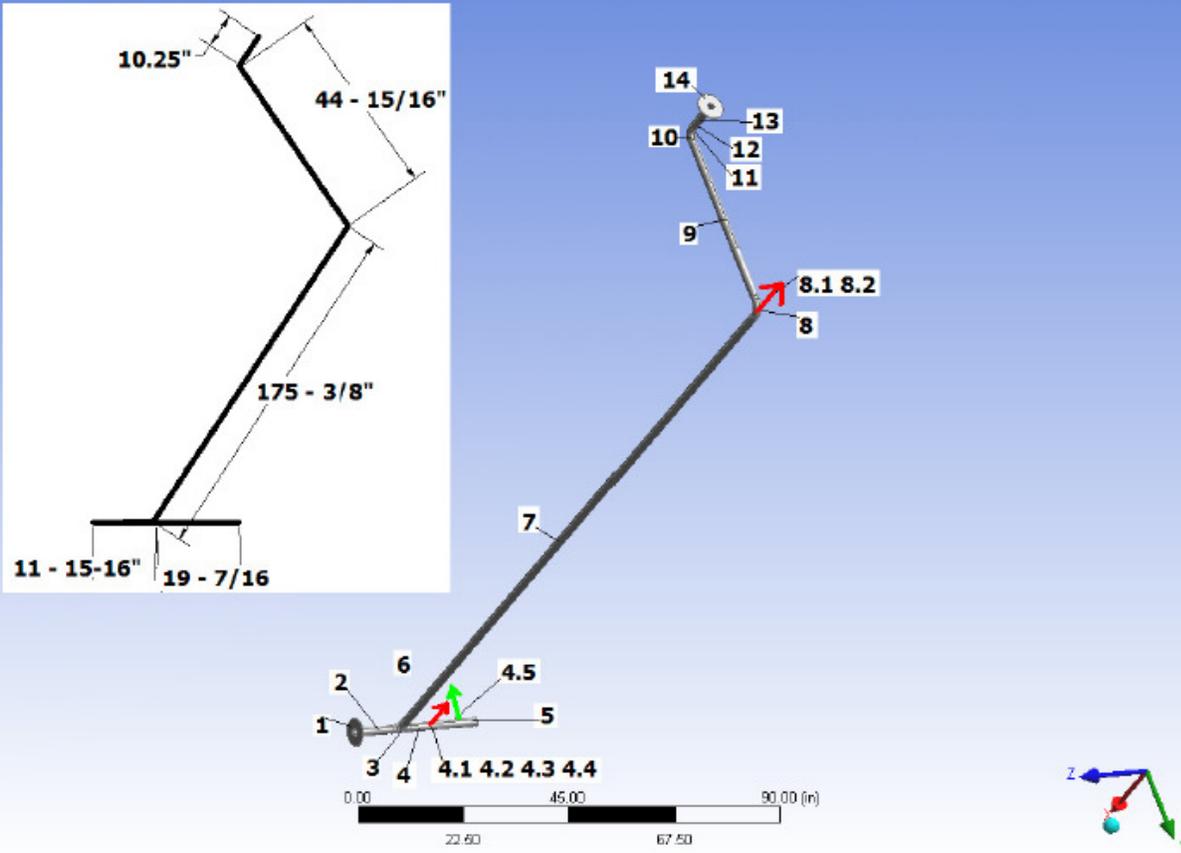
- 1.) Temperature drop from 71.6F to -110F
- 2.) Internal Pressure of 1200 psig

### Material and Equipment description

Assembly 2						
Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1.5	1	600# flange	0.875"			2000
1.5	2	Pipe	8.52	SW-flange	Butt-Tee	2000
1.5	3	Tee	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	4	Pipe	5.19	Butt-Tee	Butt-Flex	2000
0.5	4.1	Pipe saddle 1/2"		FW to piece 4	.5" Threaded	3000
0.5	4.2	threaded nipple		4.1	4.3	3000
0.5	4.3	1/2" valve		4.2	4.4	1480
0.5	4.4	1/2" pipe plug		4.3		3000
0.25	4.5	Pipe saddle 1/4"		FW to piece 4	for PDT	3000
1.5	5	Flex Hose	12	Butt-Pipe		1500
1.5	6	Strainer	5.5 inches			1480
1.5	7	Pipe	166.125	Butt-Tee	Butt-Pipe	2000
1.5	8	Tee	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	8.1	SW coupling		SW Tee	Thermowell	3000
1.5	8.2	thermowell	TW30-1-1/2-L4-SS316			20000
1.5	9	Pipe	40.44	Butt-elbow	Butt-elbow	2000
1.5	10	elbow	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	11	Pipe	1	Butt-elbow	SW- valve	2000
1.5	12	Valve	5			1480
1.5	13	Pipe	0.9	SW- valve	SW-flange	2000
1.5	14	600# flange	0.875"			1480

Physical Description / Visual representation

ANSYS  
v12

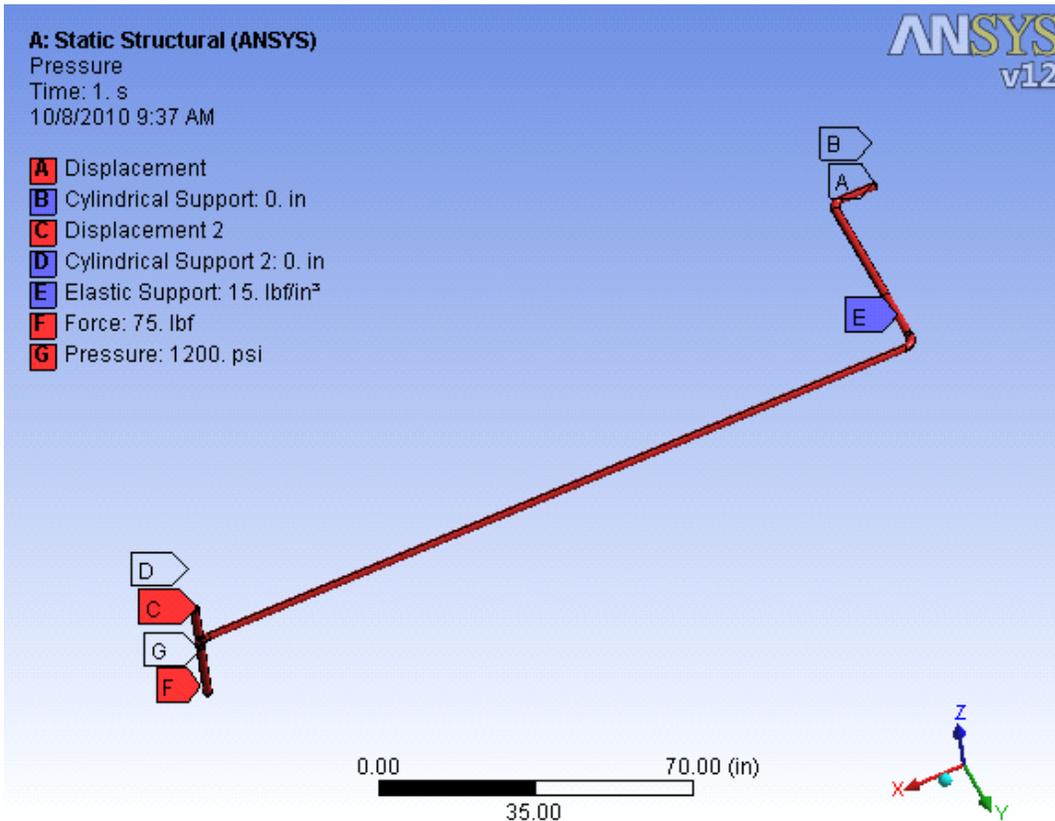


4.1,2,3,4 facing up "-X" direction

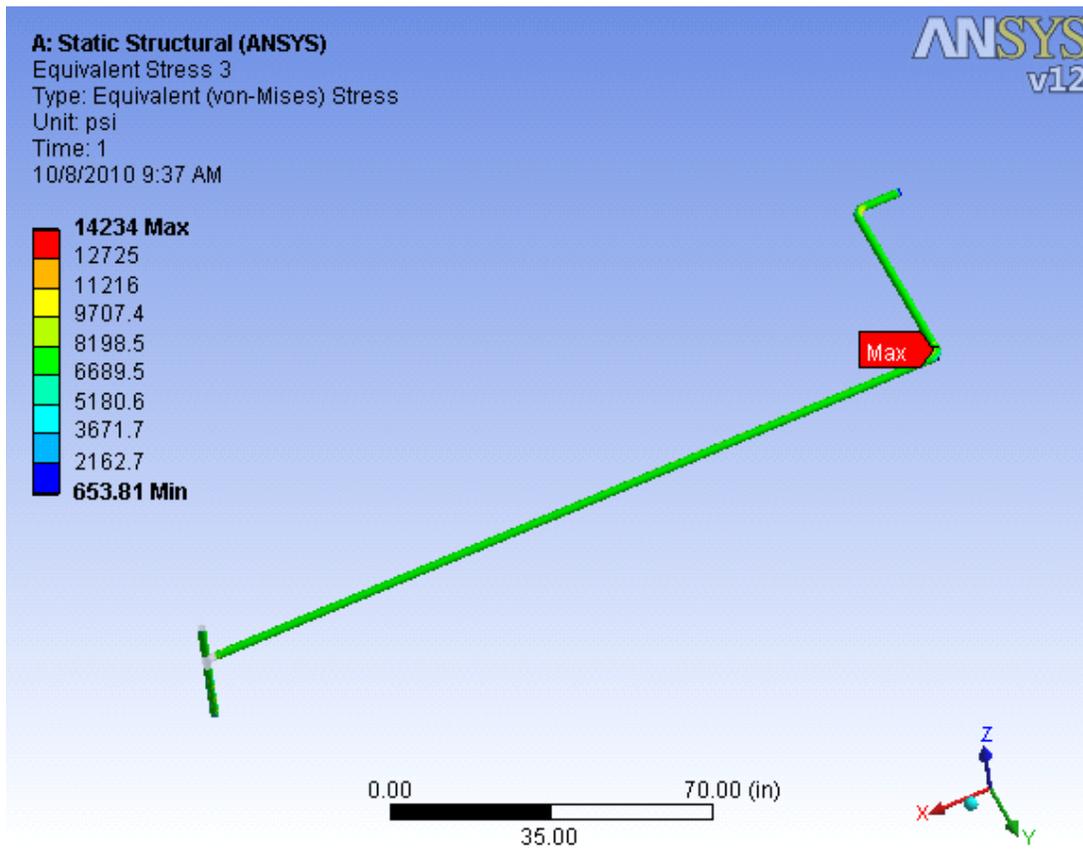
4.5 facing "-Y" direction

8.1,2 facing up "-X" direction

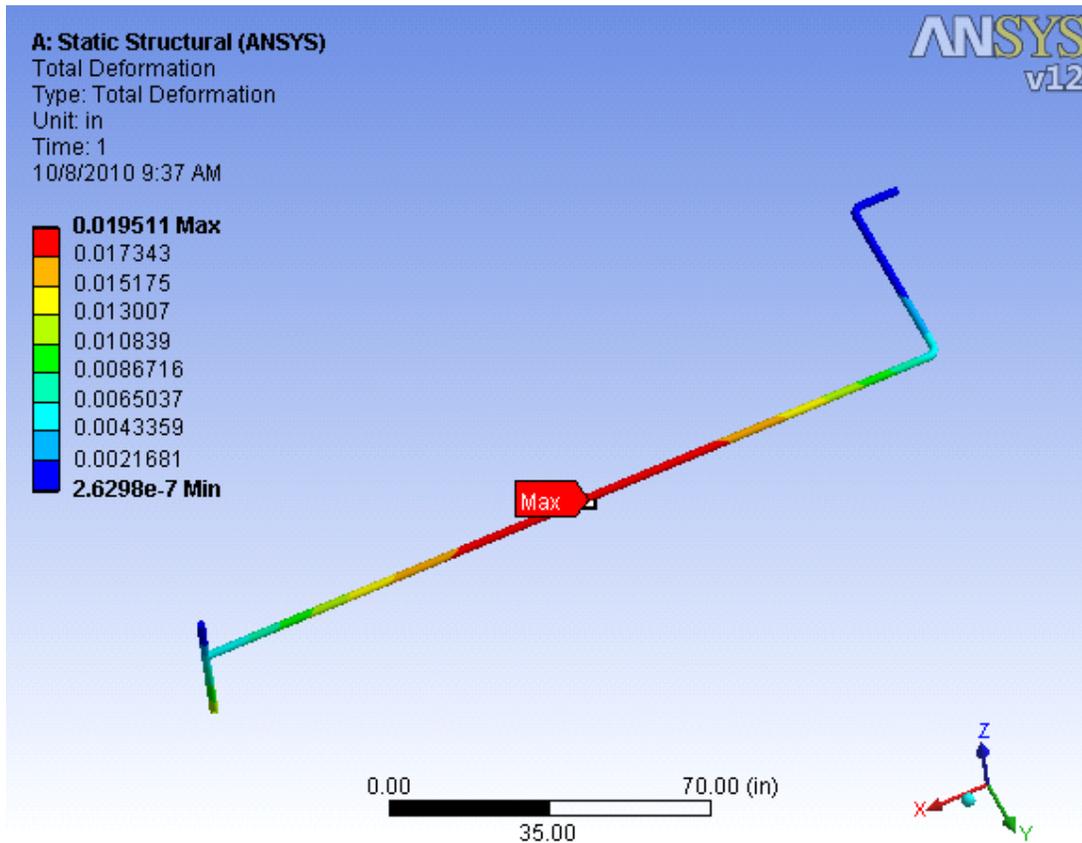
## Boundary Conditions Internal Pressure



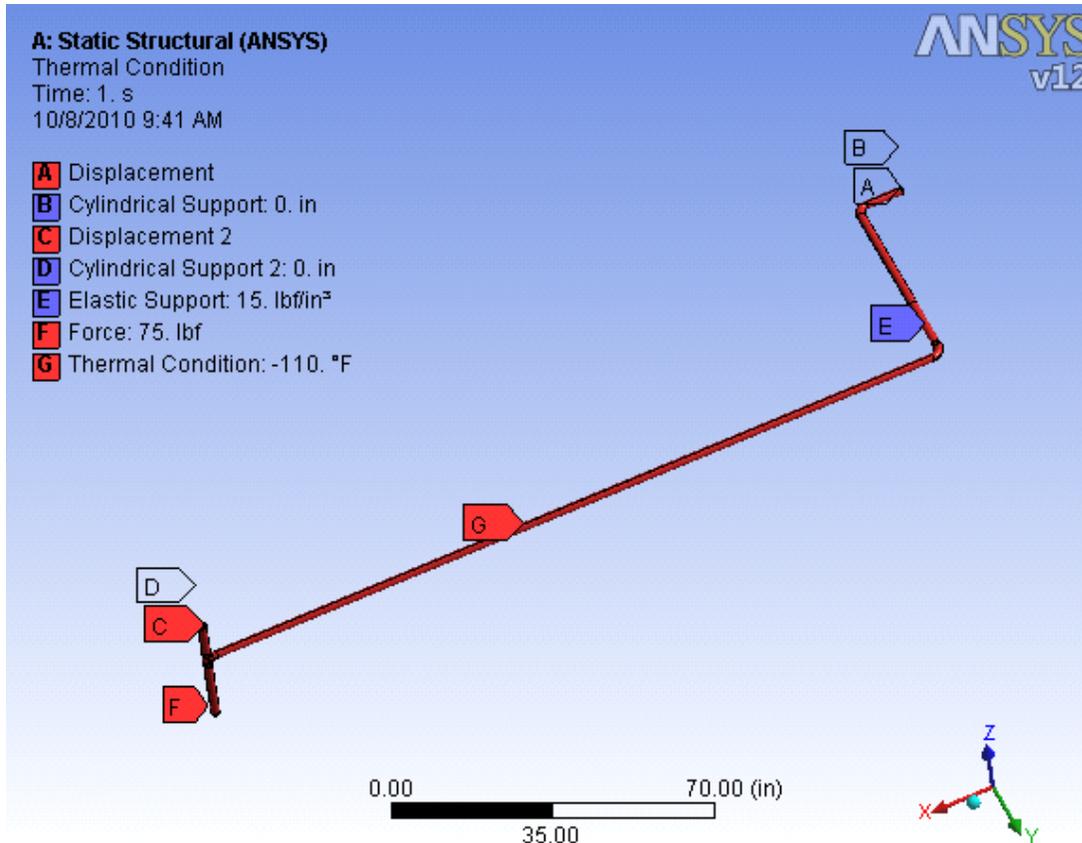
## Stress Plot



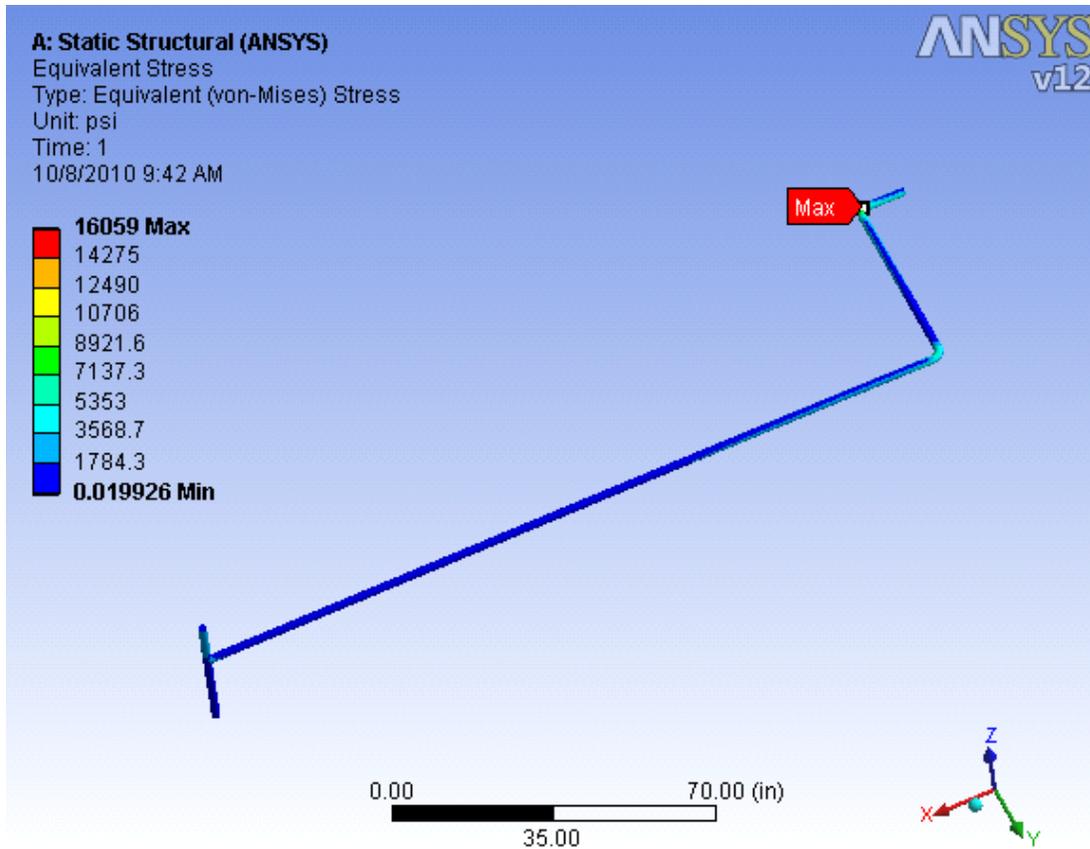
## Deformation Plot



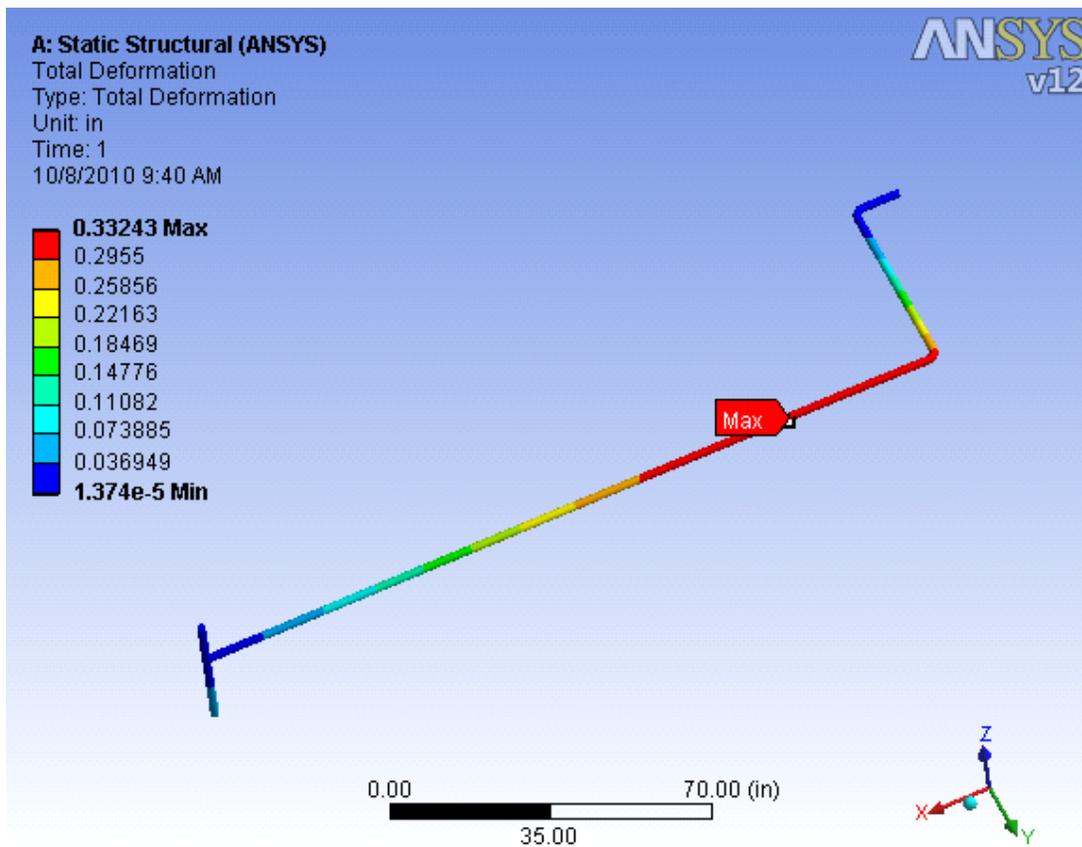
## Boundary Conditions Temperature drop to -110F



## Stress Plot



## Deformation Plot



## Result Summary For section #2

The stress levels fall below the allowed 16.7 ksi in ASME 31.3 process piping code. Fittings are designed thicker than the pipe itself, and are rated for the temperature and pressure and allowed by 31.3. Stress levels in the fittings should be somewhat lower than shown in the ansys model since they are modeled the same thickness as the pipe itself for a conservative approach. The pipe Tee was left out of the stress plot in the pressure analysis since it is rated to the temperature and pressure for ASME31.3. Deformation levels are reasonable and could easily be allowed by the pipe insulation and hangers without constraint.

### Pipe Section 3

Pipe section 3 is two assemblies joined by a Hart union. The two were joined in an assembly and the model was then analyzed in Ansys with the described boundary conditions and subjected to numerous loads:

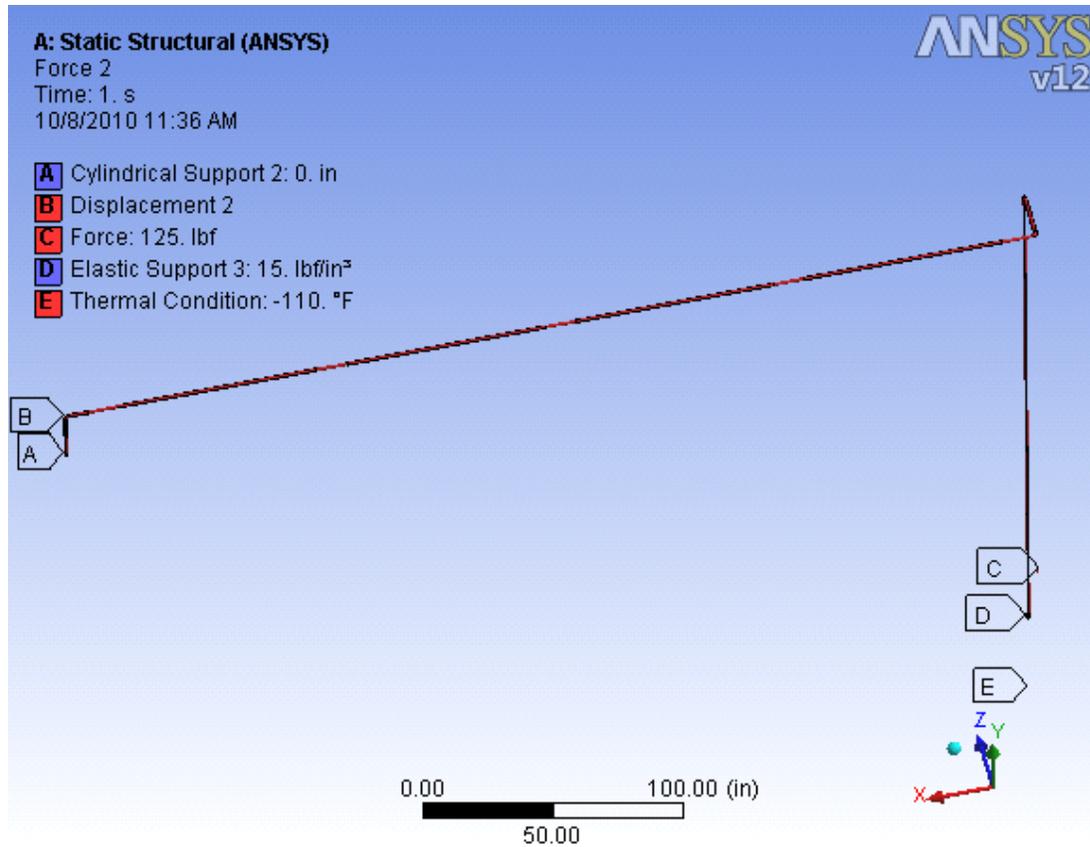
- 1.) Temperature drop from 71.6F to -110F
- 2.) Internal Pressure of 1200 psig

### Pipe and equipment descriptions

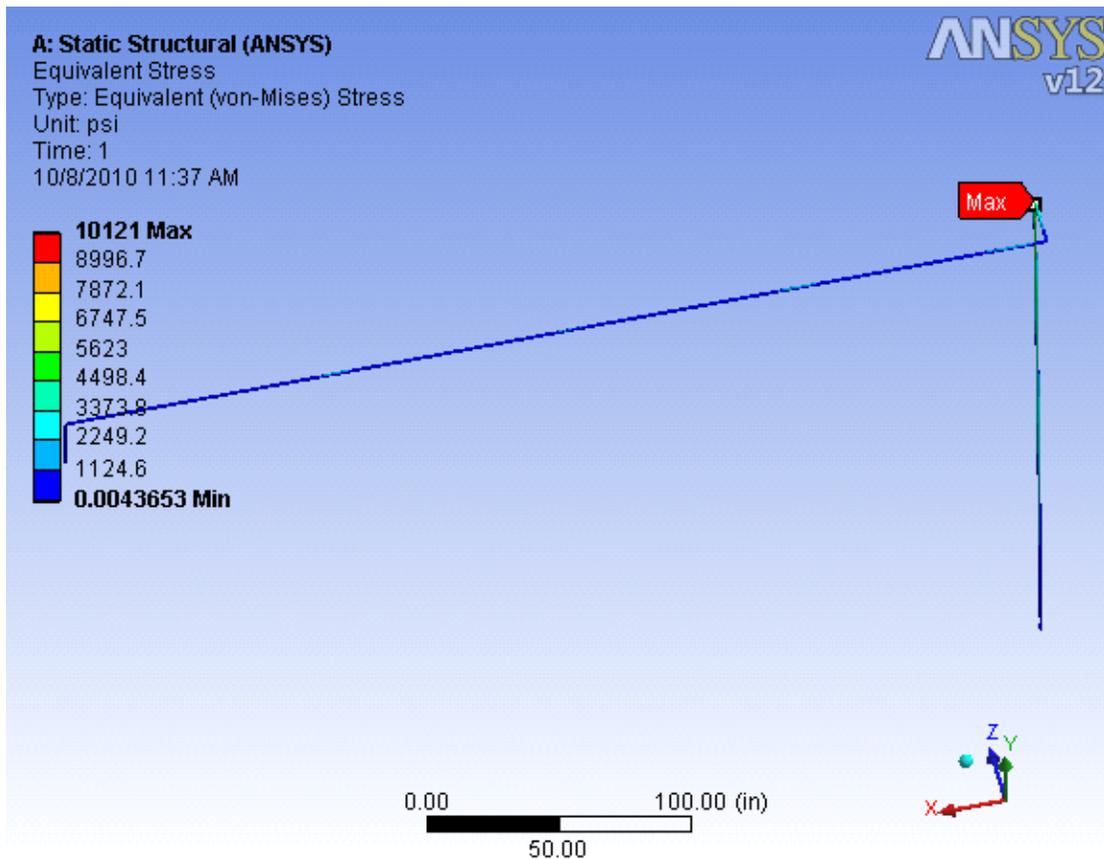
Assembly 6 - return line 1						
Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1.5	1	flange	1.125	Vessel		1480
1.5	2	Pipe	1	SW flange	SW valve	2000
5	3	valve	5			1480
1.5 to 1	4	reducer	2.5	SW Valve	Butt-Pipe	2000
1	5	Pipe	12.625	Butt-Reducer	Butt-elbow	3000
1	6	elbow	1.5			3000
1	7	Pipe	263	Butt-elbow	SW Union	3000
1 to 3/4	7.1	saddle ftng (3/4)			relief Valve	3000
.75	7.2	relief valve				2000
1	7.3	fitting	1			3000
1	7.4	Pipe	63	Butt Fitting	Butt elbow	3000
1	7.5	elbow	1.5	Butt-Pipe	Outside	3000
1	8	SW union Thrd End			(Assm 8)	3000

Assembly 8 - return line						
Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1	1	Union Nut End		(Assm 6)		3000
1	2	Pipe	113.87	Butt-pipe	Butt-elbow	3000
1	3	elbow		Butt-Pipe	Butt-Pipe	3000
1	4	Pipe	17.5	Butt-elbow	Butt-elbow	3000
1	5	elbow		Butt-Pipe	Butt-Pipe	3000
1	6	Pipe	256	Butt-elbow	Butt-elbow	3000
1	7	elbow		Butt-Pipe	Butt-Pipe	3000
1	8	Pipe	3	Butt-elbow	SW Union	3000
1	9	Union TE	2.25/2	Piece 19	(to Assm 7)	3000

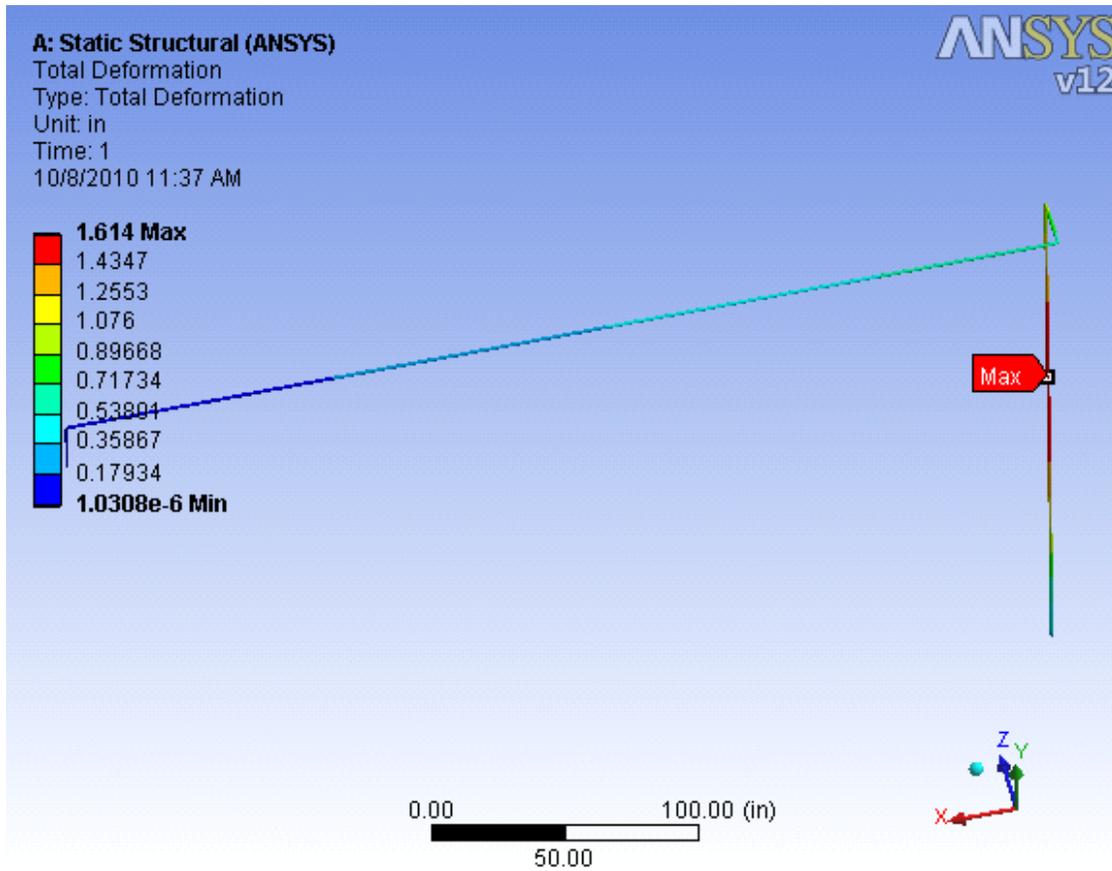
## Boundary Conditions Temperature drop to -110F



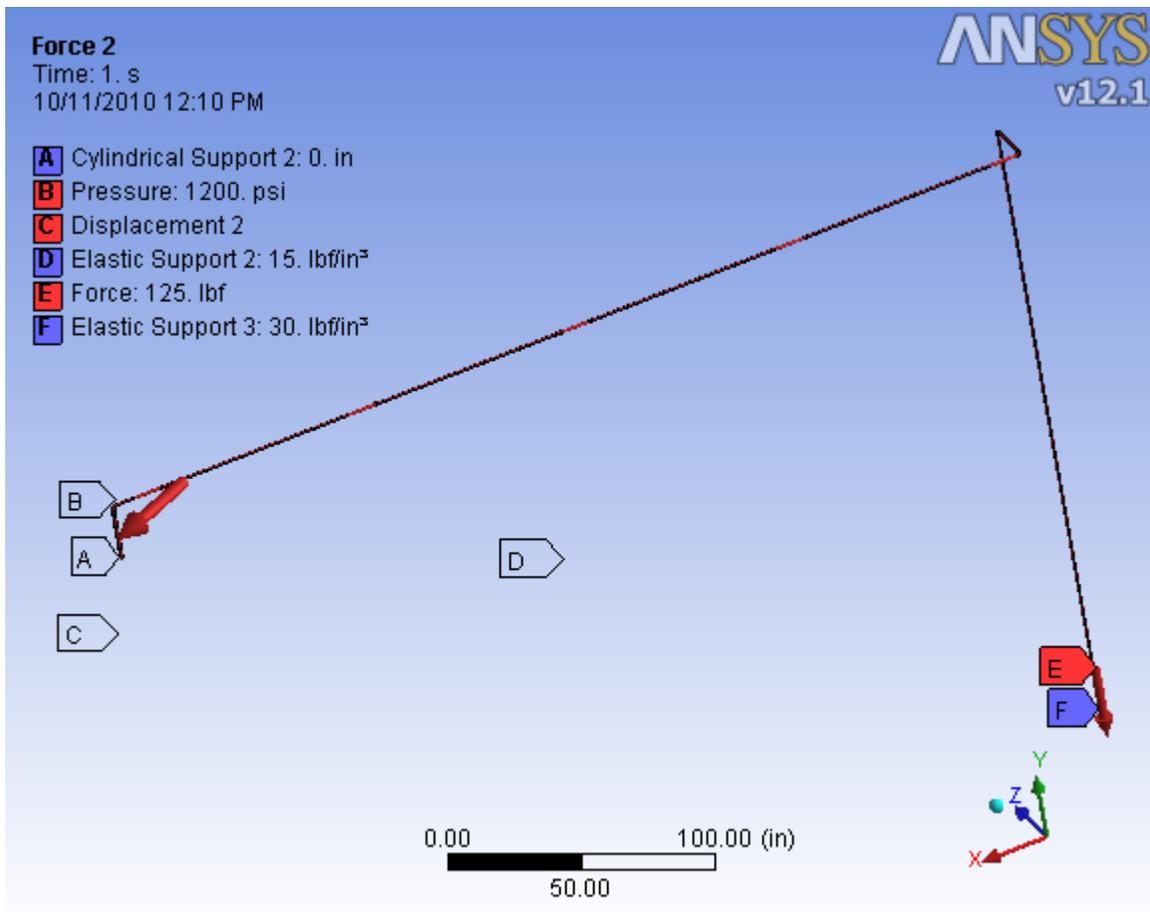
## Stress Plot



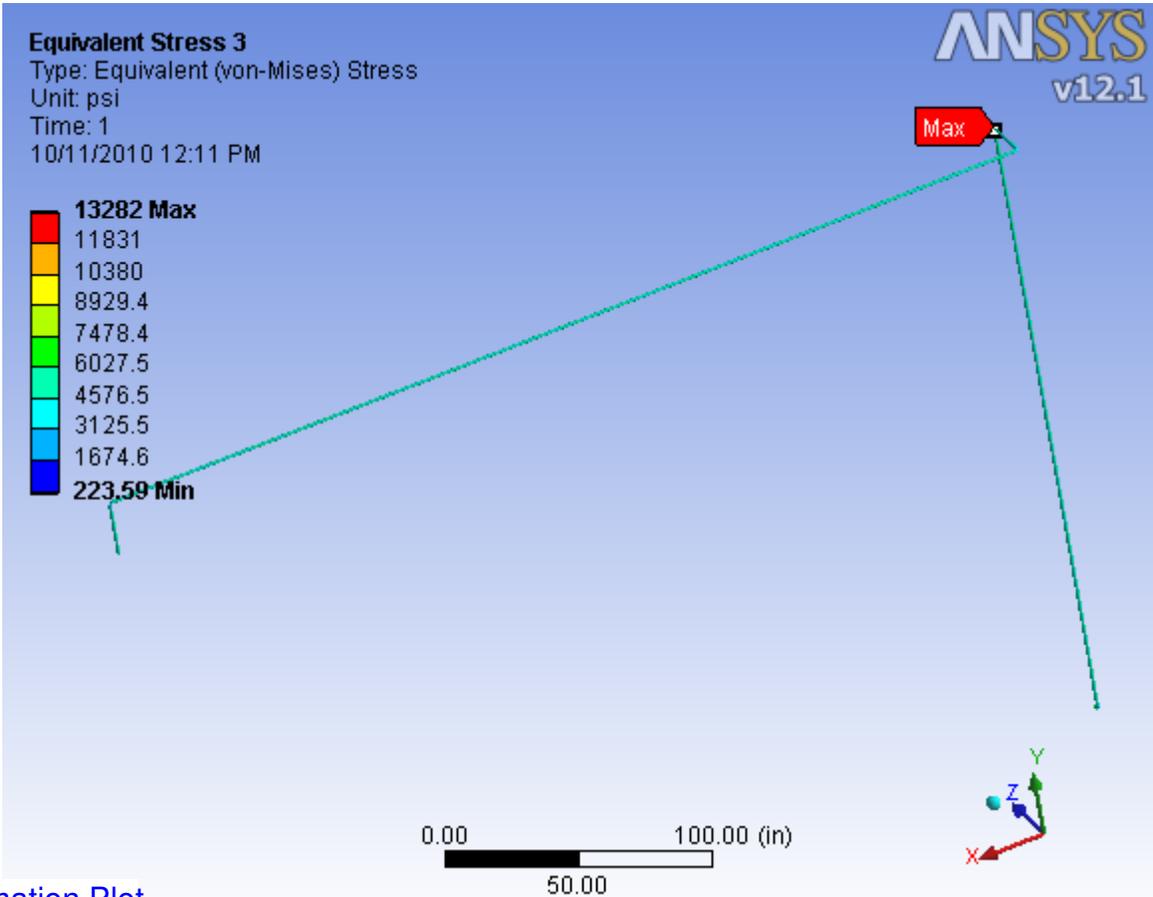
## Deformation Plot



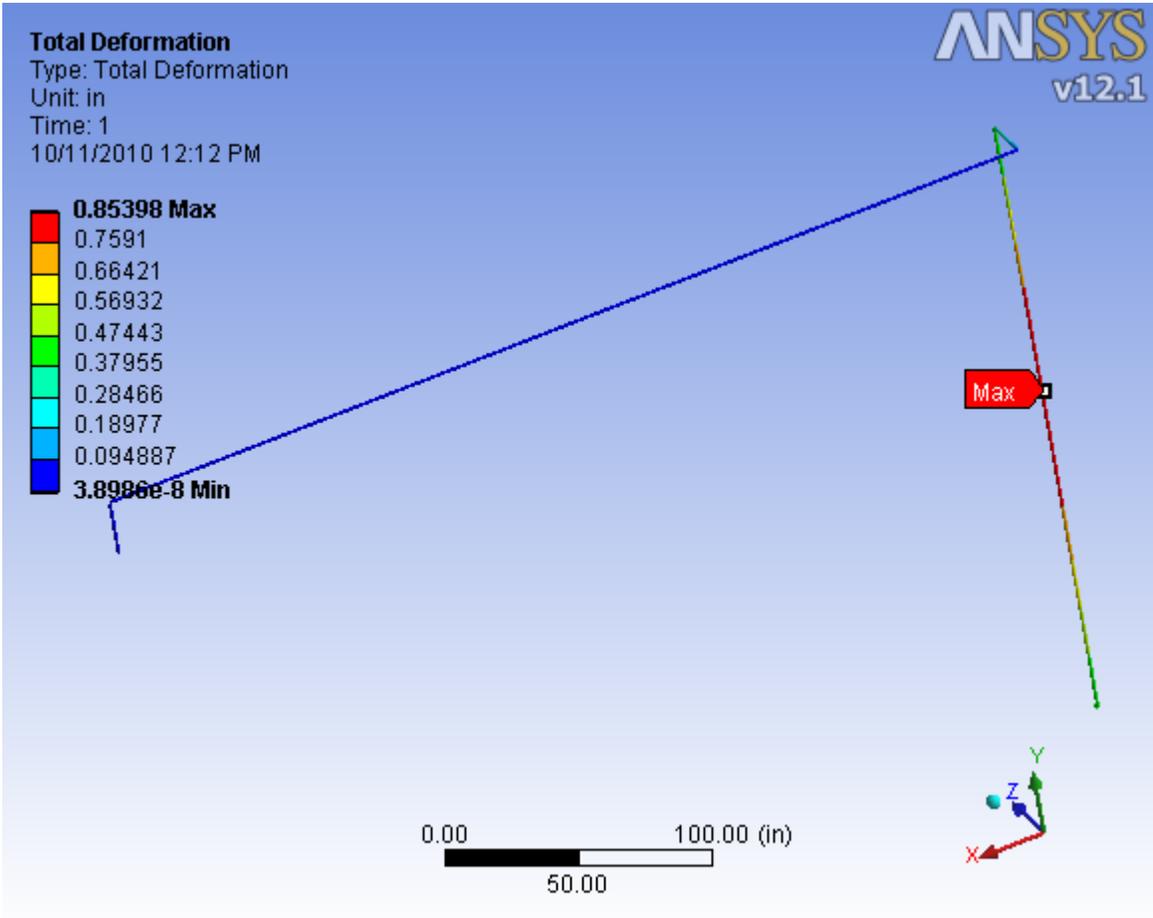
## Boundary Conditions Internal Pressure



Stress Plot



Deformation Plot



## Pipe Section 4

Pipe section 4 is two assemblies joined by a welding. The two were joined in an assembly and the model was then analyzed in Ansys with the described boundary conditions and subjected to numerous loads:

- 1.) Temperature drop from 71.6F to -110F
- 2.) Internal Pressure of 1200 psig

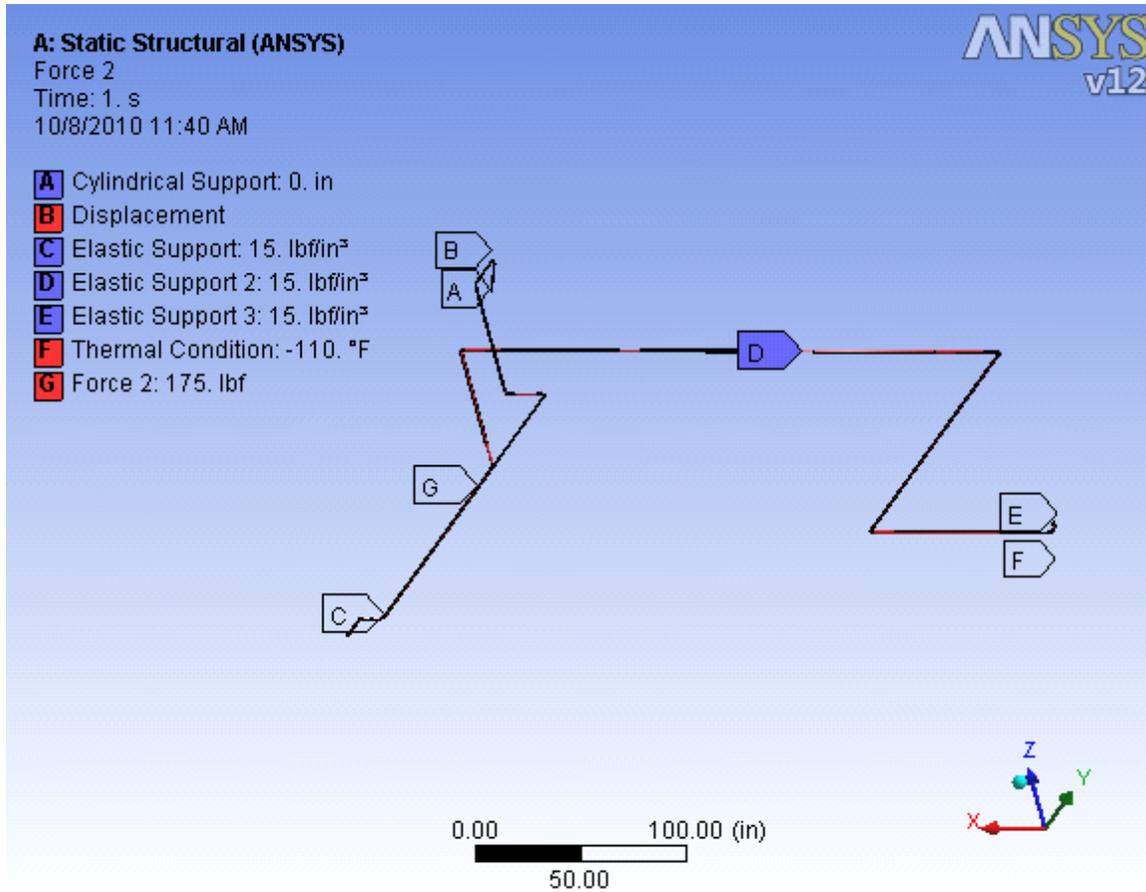
### Pipe and equipment descriptions

Assembly 3 - out of pump						
Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1.5 to 1	1	Flex Hose	16 - 5/16	Butt-Elbow		1500
	1.1	Pipe saddle 1/4"		Piece 1 reducer	tp PDT	3000
1	2	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	3	Pipe	9.06	Butt-elbow	Butt-elbow	3000
1	4	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	5	Pipe	5	Butt-elbow	SW strainer	3000
1	6	check valve	5			1480
1	7	Pipe	120.29	SW strainer	Butt-Tee	3000
	7.1	Pipe saddle 1"	~57" from CV	Piece 7	Relief valve	3000
1	7.2	relief valve				10000 psi burst
1	7.3	fitting	1			3000
1	7.4	Pipe	16	Butt Fitting	Butt elbow	3000
1	7.5	elbow	1.5	Butt-Pipe	Outside	3000
1	8	Tee	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	9	Pipe	62.54	Butt-Tee	Butt-elbow	3000
1	10	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	11	Pipe	282.16 (two pieces)	Butt-elbow	Butt-Pipe	3000
1	11.1	Pipe		Butt-Pipe	Butt-elbow	3000
1	12	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	13	Pipe	158.55	Butt-elbow	Butt-elbow	3000
1	14	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	15	Pipe	92.88	Butt-elbow	Butt-elbow	3000
1	16	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	17	Pipe	1.68	Butt-elbow	Butt-elbow	3000
1	18	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	19	Pipe	3	Butt-elbow	SW Union	3000
1	20 TE	Union TE	2.25/2	Piece 19	(to Assm 5)	3000

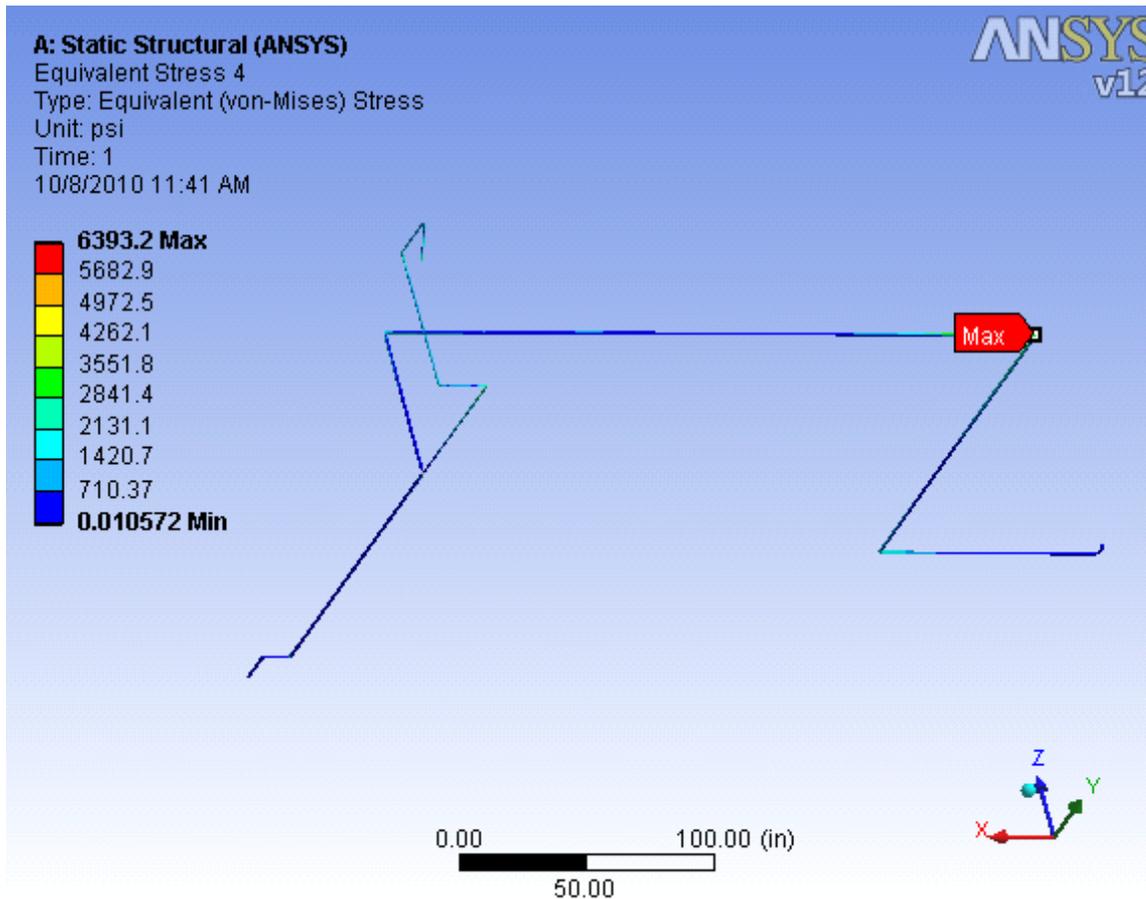
## Assembly 4 - out of Pump Pipe back to vessel dead head line

Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1 to .75	1	reducer	2	Butt T (Assm3)	Butt-reducer	3000
.75 to .5	2	reducer	1.5	Butt-reducer	Butt-Pipe	3000
0.5	3	Pipe	58.75	Butt-reducer	Butt-elbow	3000
0.5	4	elbow	r = 1.5	Butt-Pipe	Butt-Pipe	3000
0.5	5	Pipe	18.09	Butt-elbow	Butt-elbow	3000
0.5	6	elbow	r = 1.5	Butt-Pipe	Butt-Pipe	3000
0.5	7	Pipe	58.57	Butt-elbow	Butt-elbow	3000
0.5	8	elbow	r = 1.5	Butt-Pipe	Butt-Pipe	3000
0.5	9	Pipe	22.5	Butt-elbow	Butt-elbow	3000
0.5	10	elbow	r = 1.5	Butt-Pipe	Butt-elbow	3000
0.5	11	45 degree elbow	r = 1.5	Butt-elbow	Butt-Pipe	3000
0.5	12	Pipe	10	Butt-elbow	SW Union	3000
0.5	13	hart union	2			3000
0.5	14	Thrd Pipe (cut in 1/2)	2.5	SW union	Valve	3000
0.5	15	1/2" valve	2.78	Thrd Pipe	reduc nipple	1480
.5 to .75	16	reducing nipple	0.25	valve	vessel port 1	6600

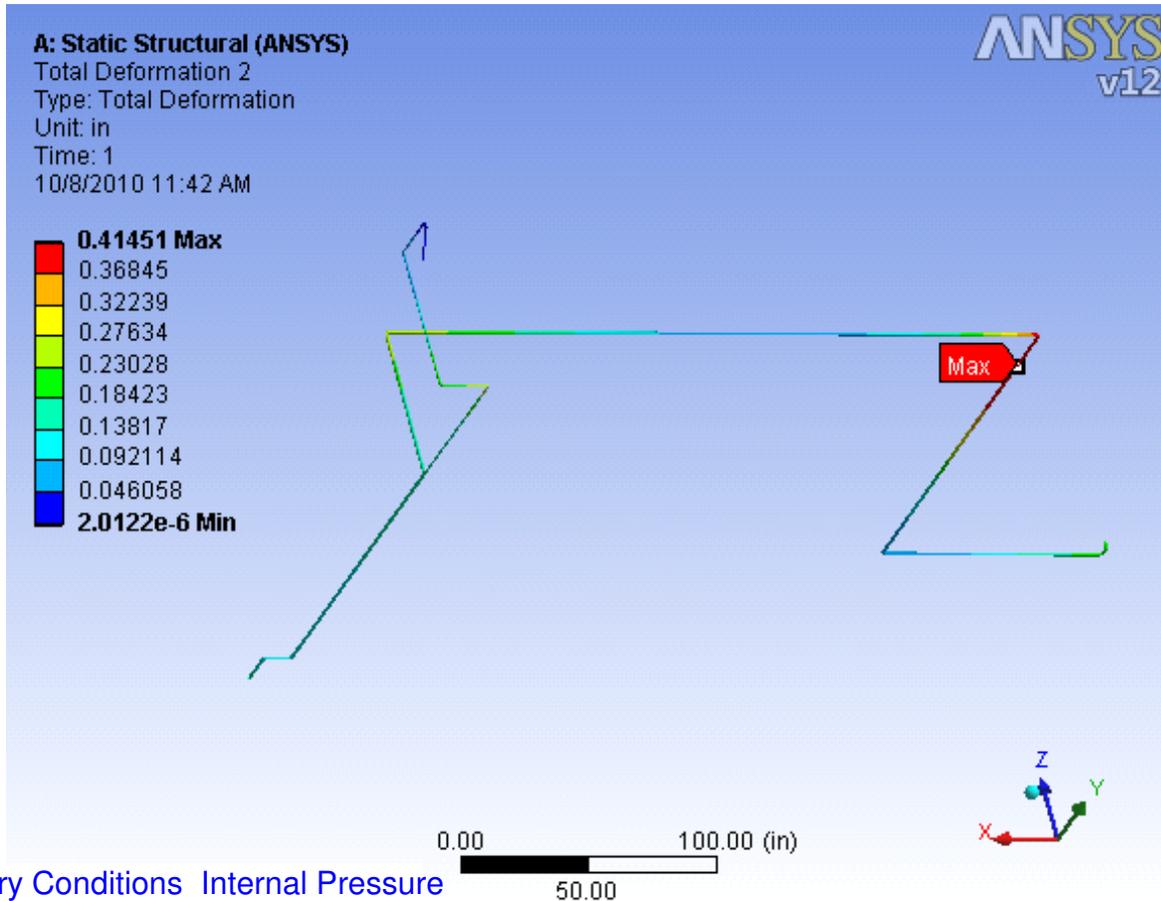
## Boundary Conditions Temperature drop to -110F



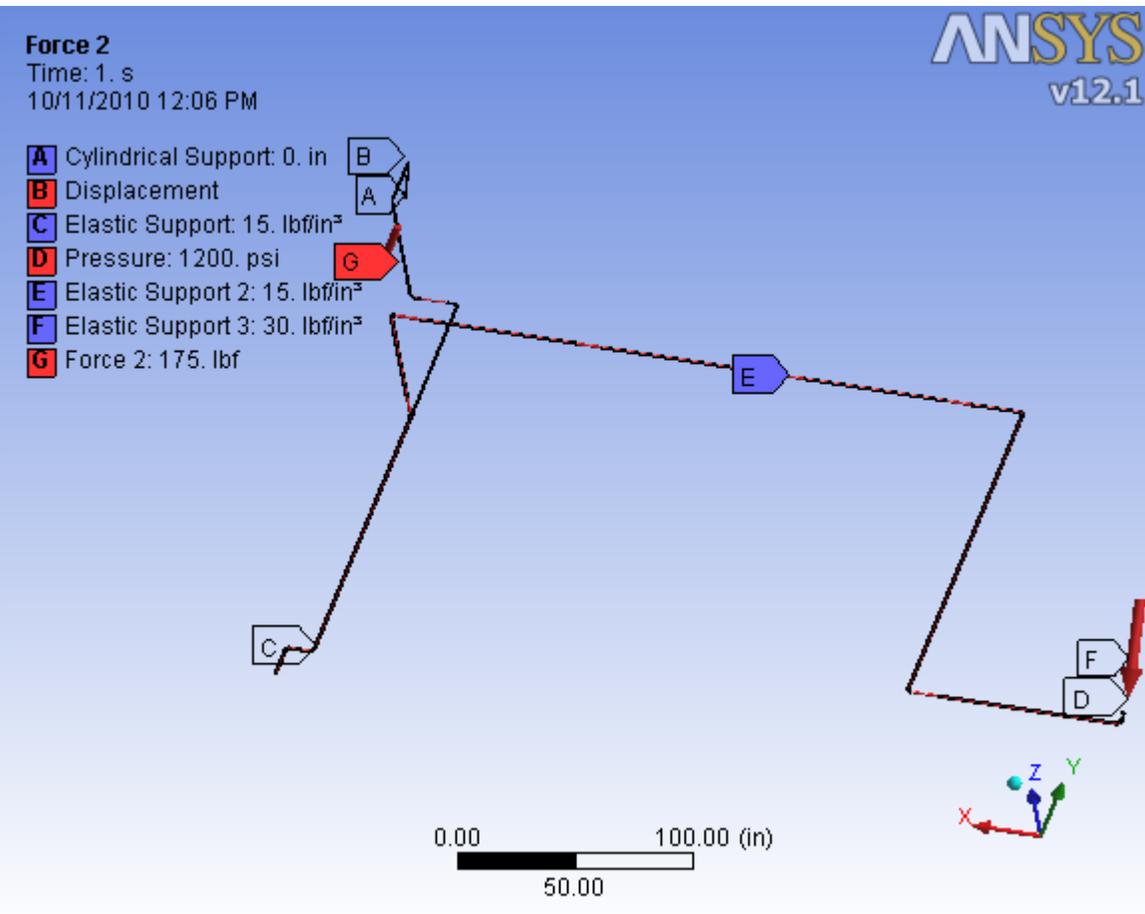
## Stress Plot



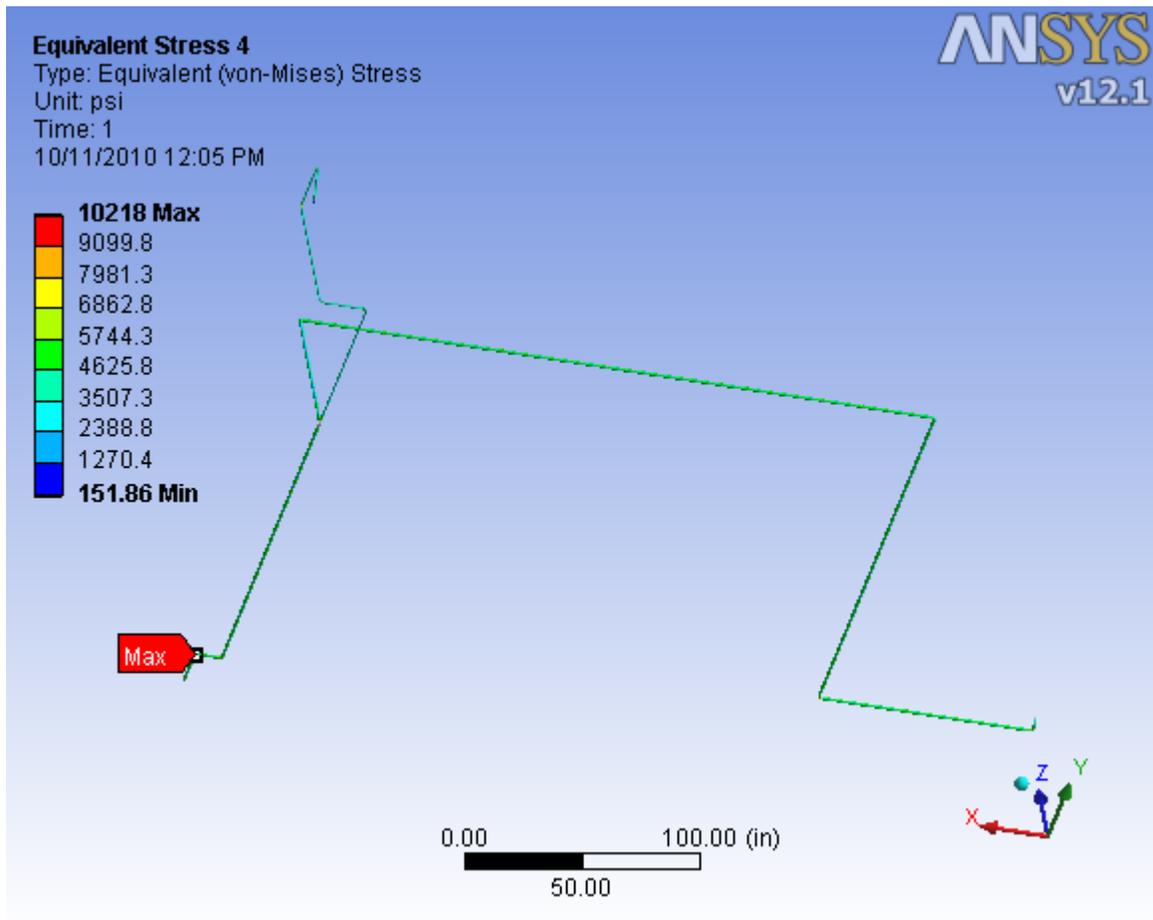
## Deformation Plot



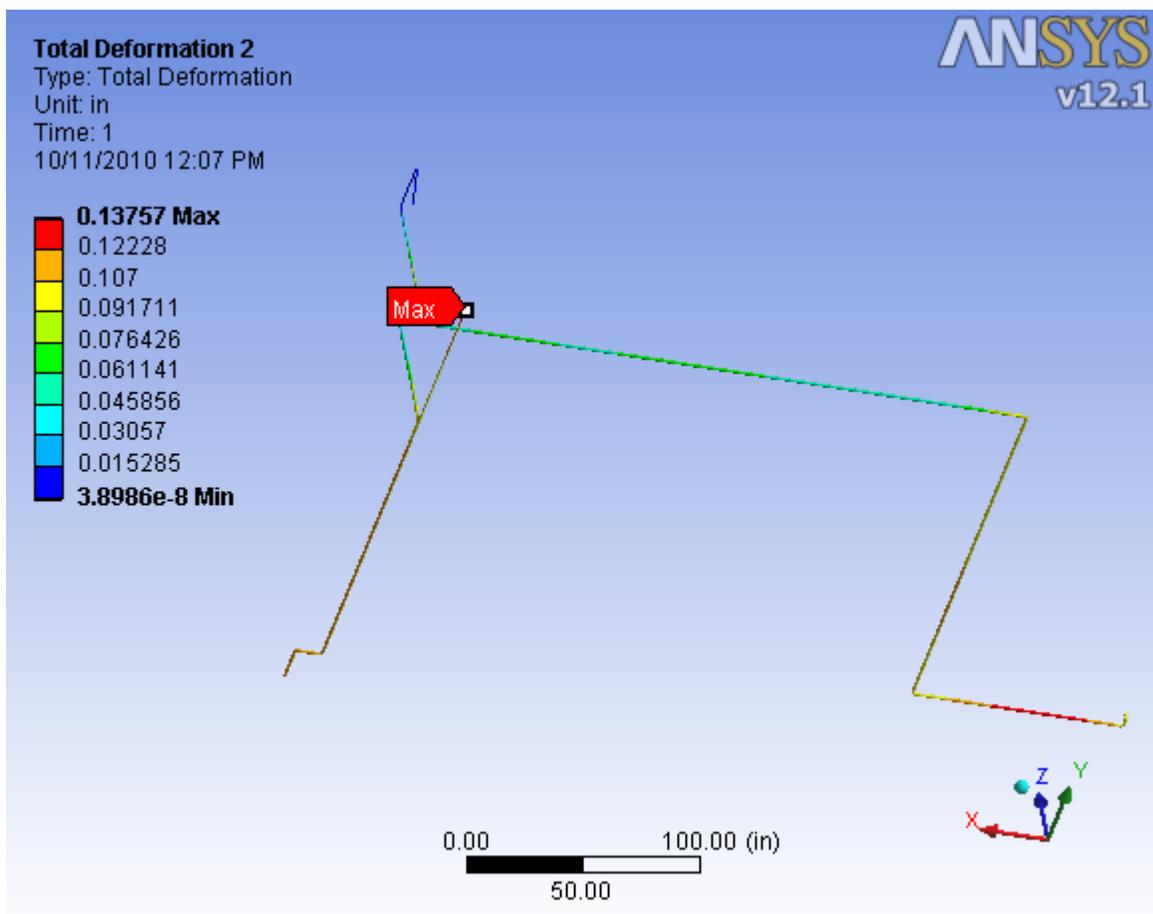
## Boundary Conditions Internal Pressure



## Stress Plot



## Deformation Plot



## Pipe Section 5

Pipe section 4 is three assemblies joined by a flanges, hart unions and welding. They were joined in an assembly and the model was then analyzed in Ansys with the described boundary conditions and subjected to numerous loads:

- 1.) Temperature drop from 71.6F to -110F
- 2.) Internal Pressure of 1200 psig

Unconstrained Extensions of the pipe were not added to the model to simplify computation as they do not effect analysis results. A small phase separation vessel was analyzed

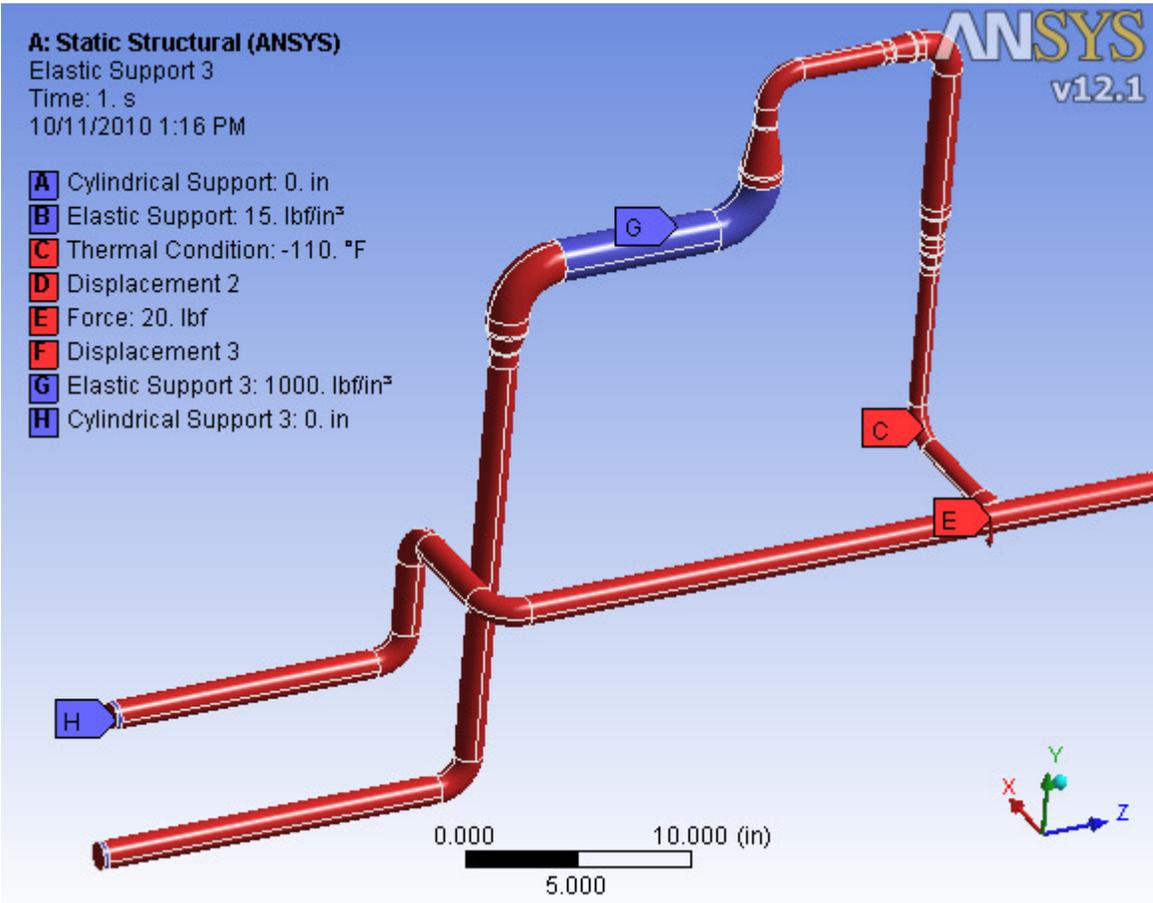
### Pipe and equipment descriptions

Assembly 5 - into cleanroom						
Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1	1	Union NUT END	2.25/2	(to Assm 3)	piece 2	3000
1	2	Pipe	12.55			3000
1	3	elbow		Butt-Pipe	Butt-Tee	3000
1	4	Tee		Butt-Elbow	Butt-Pipe	3000
1	4.1	1" Valve	4.22			1480
1	4.2	Pipe	1			3000
1	4.3	Flange				1480
1	4.4	Blind Flange				1480
1	5	Pipe	5.015	Butt-Tee	SW-Valve	3000
1	6	Valve	4.22			1480
1	7	Pipe	5.015	SW-Valve	Butt-Tee	3000
1	8	Tee	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	8.1	1" Valve	4.22			1480
1	8.2	Pipe	1			3000
1	8.3	Flange				1480
1	8.4	Blind Flange				1480
1 to 1.5	9	reducer to 1.5	L=2.5	Butt-Tee	Butt-elbow	2000
1.5	10	elbow	r=2.25	Butt-Reducer	Butt-Pipe	2000
1.5	11	Pipe	0.4	Butt-elbow	SW-flange	2000
1.5	12	600# flange	0.875"+.25"			1480
Assembly 9 - Phase Separator Top outlet (P.S.)						
Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
0.75	1	pipe nipple cut	3	threaded to P.S.	butt elbow	2000
0.75	2	pipe elbow	r = 1.5	Butt Pipe	Butt Pipe	3000
.75 to 1	3	reducer	2"	Butt-elbow	Butt Pipe	3000
1	4	Pipe	4	Butt-Reducer	Butt-elbow	3000
1	5	elbow	r = 1.5			3000
1	6	Pipe	4	Butt-elbow	SW strainer	3000
1	6.1	saddle fitting	2" from elbow			3000
1	6.11	sight glass				1450
1	6.2	saddle fitting				3000
1	6.21	sight glass				1450
1	7	Strainer	4.5			1480
1 to .75	8	reducer	2	SW-Strainer	Butt Reducer	3000
.75 to .5	9	reducer	1.5	Butt Reducer		3000
0.5	10	Check Valve	3.75			1480
0.5	11	Pipe	3 - 7/16	SW-CV	Butt elbow	3000
0.5	12	elbow				3000
0.5	13	Pipe	1	Butt-elbow	SW CV	3000
0.5	14	Control Valve				2000
0.5	15	Pipe	3	SW CV	SW-(Assm 7)	3000

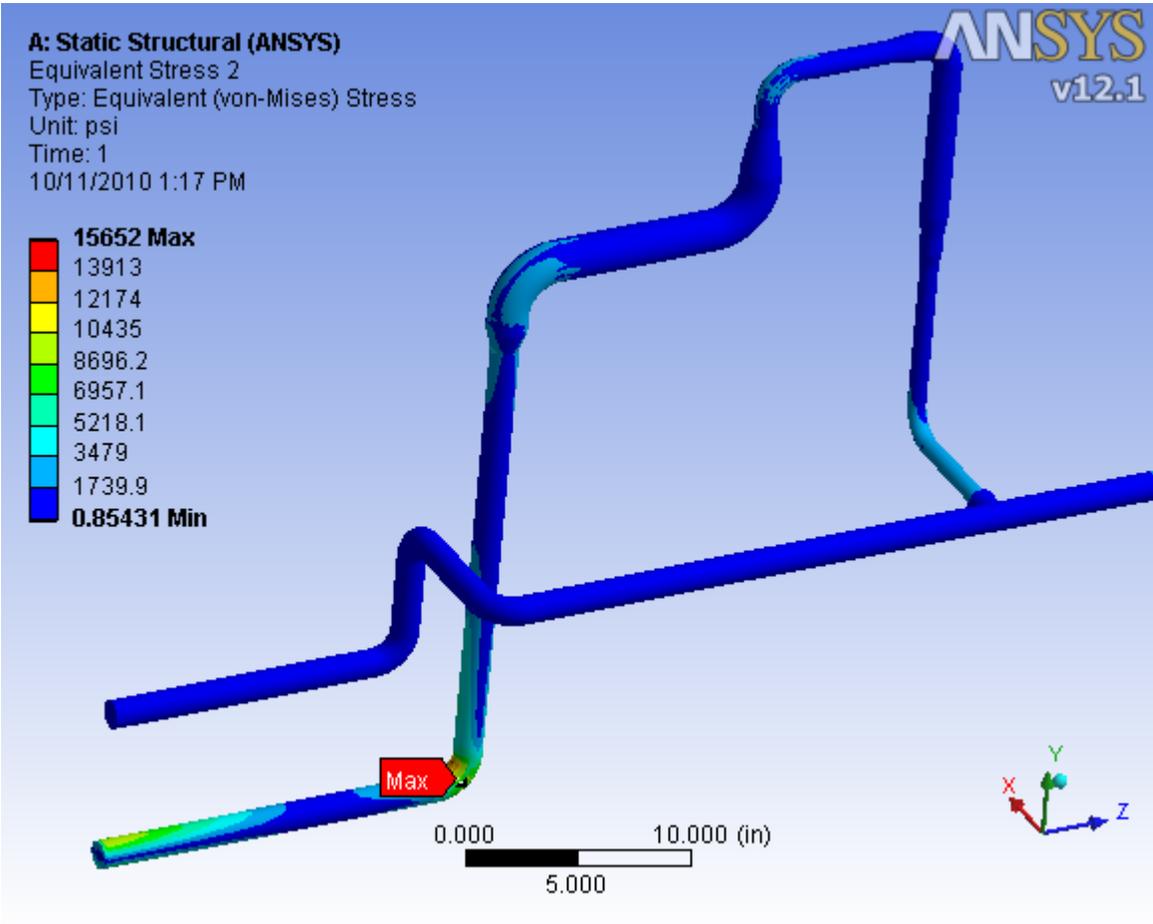
## Assembly 7 - return line in cleanroom

Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1	1	Union NE	2.25/2	Piece 19	(to Assm 8)	3000
1	2	Pipe	8.82	SW union	Butt - elbow	3000
1	3	elbow	r = 1.5	Butt-Pipe	Butt-Pipe	3000
1	4	Pipe	4.81	Butt-elbow	Butt-elbow	3000
1	5	elbow	r = 1.5	Butt-Pipe	Butt-Pipe	3000
1	6	Pipe	3.6	Butt-elbow	Butt-elbow	3000
1	7	elbow	r = 1.5	Butt-Pipe	Butt-Reducer	3000
1 to 1.5	8	Reducer	2.5 - .5	Butt-elbow	SW-CV	2000
1.5	9	Check-Valve	5	reducer	reducer	1480
1.5 to 1	10	Reducer	2.5 - .5	SW-CV	Butt-Pipe	2000
1	11	Pipe	17.05	Butt-Reducer	SW-Valve	3000
.5"	11.1	saddle fitting		pipe 11	(to assm 9)	3000
1	12	1" Valve	4.22	pipe 11	pipe13	3000
1	13	Pipe	1	SW-Valve	Butt-elbow	1480
1	14	Elbow	r = 1.5 "	Butt-Pipe	Butt-Pipe	3000
1 to 1.5	15	reducer	2.5	Butt-elbow	Butt-Pipe	2000
1.5	16	Pipe	9.375	Butt - reducer	SW-Valve	2000
1.5"	16.1	saddle fitting	2" from reducer			3000
1.5"	16.11	sight glass				1450
1.5"	16.2	saddle fitting	2" from reducer			3000
1.5"	16.21	sight glass				1450
.5"	16.3	saddle fitting	4.75" from reducer			3000
0.5	16.31	nipple				3000
0.5	16.32	Valve				1480
.5 to .25	16.33	bushing				3000
0.25	16.34	Pressure Trans				3000
.5"	16.4	saddle fitting	7.25" from reducer		relief valve	3000
0.5	16.41	relief valve				10000 psi burst
1.5	17	Valve	5	pipe 16	Pipe 18	1480
1.5	18	Pipe	1.5	SW-Valve	Butt Tee	2000
.25"	18.1	saddle fitting				3000
1.5	19	Tee		Butt pipe 18	Butt Tee 20	3000
1.5	19.1	Coupling		Tee 20	Thermowell	3000
1.5	19.11	Thermowell				20000
1.5	20	Tee		Butt Tee 19	Valve (up)	3000
1.5	20.1	Valve		Tee 19	Pipe 19.2	1480
1.5	20.11	Pipe	1	SW valve	SW flange	3000
1.5	20.12	flange		end of pipe 19.2		1480
1.5	20.13	blind flange				1480
1.5	21	45 degree elbow		Butt Tee 20		2000
1.5	22	Flex Pipe		Butt elbow	Butt Pipe	1200 (4842 Burst)
1.5	23	Pipe	2	Butt Flex	SW Flange	2000
0.375	24	saddle fitting				3000
0.375	24.1	Nipple				3000
0.375	24.11	Valve				1480
0.375	24.12	plug				3000
1.5	25	Flange				1480

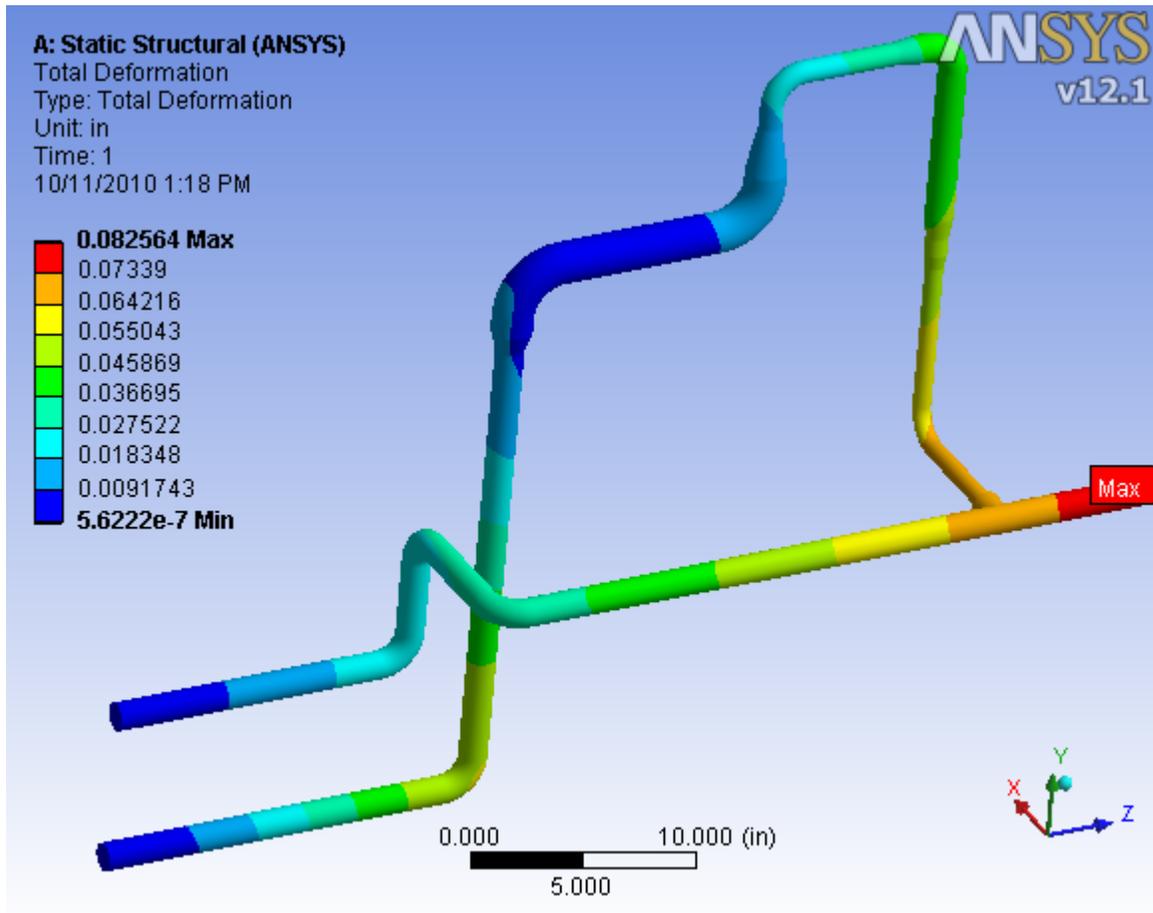
Boundary Conditions Temperature drop to -110F



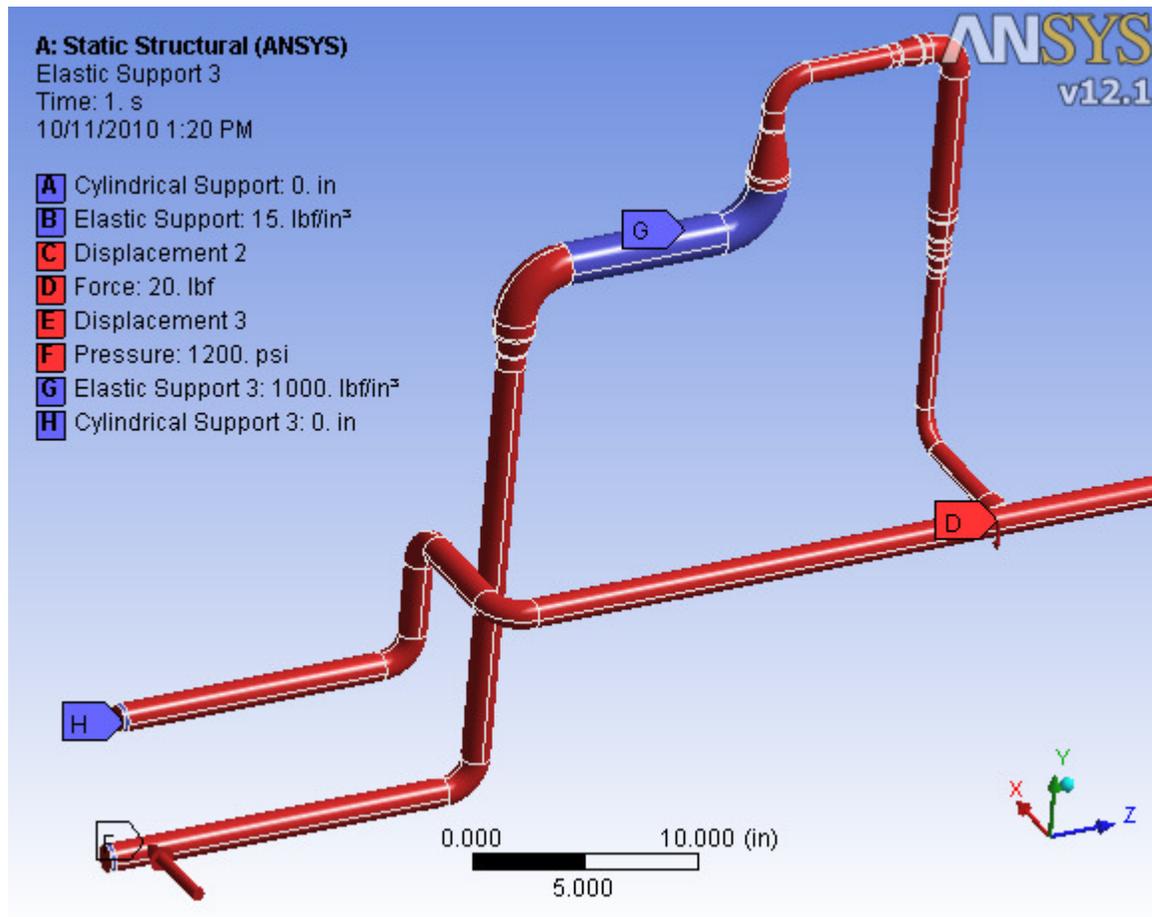
Stress Plot



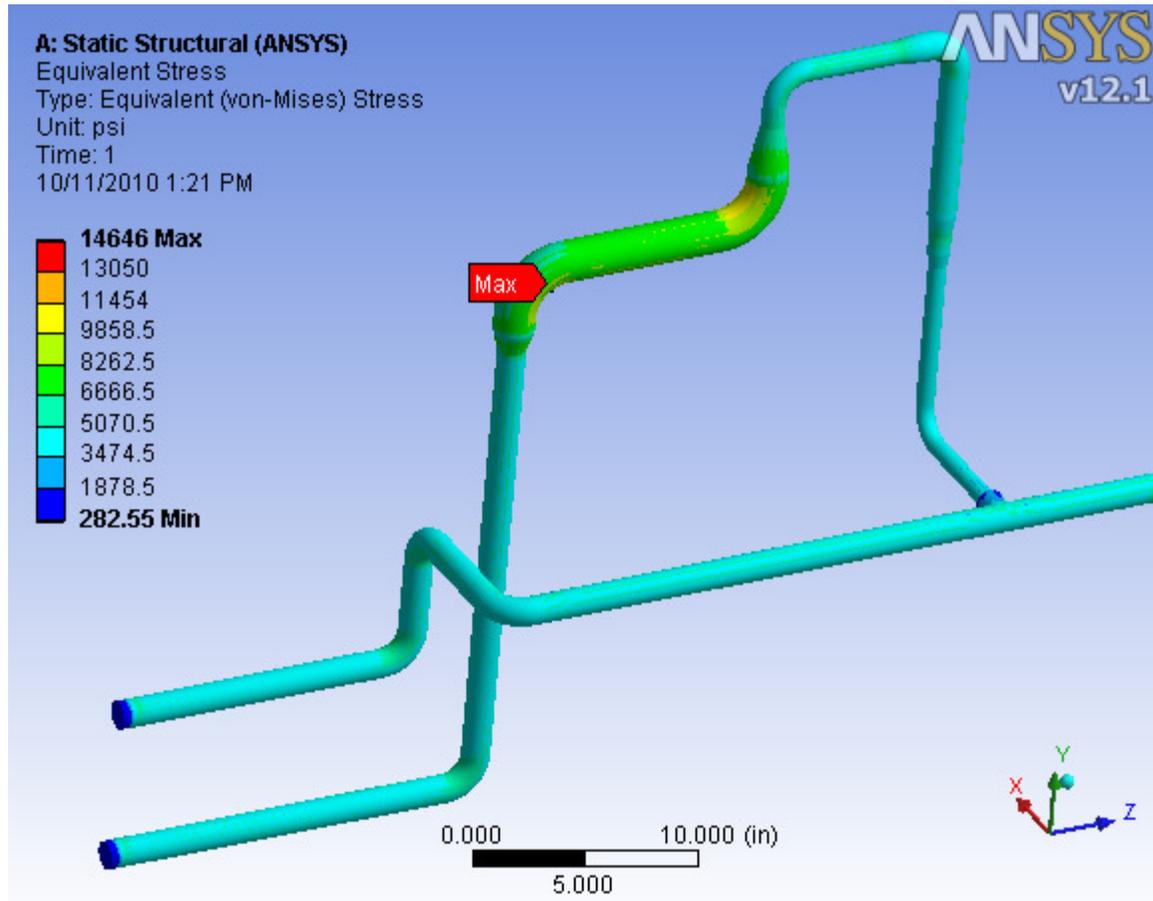
## Deformation Plot



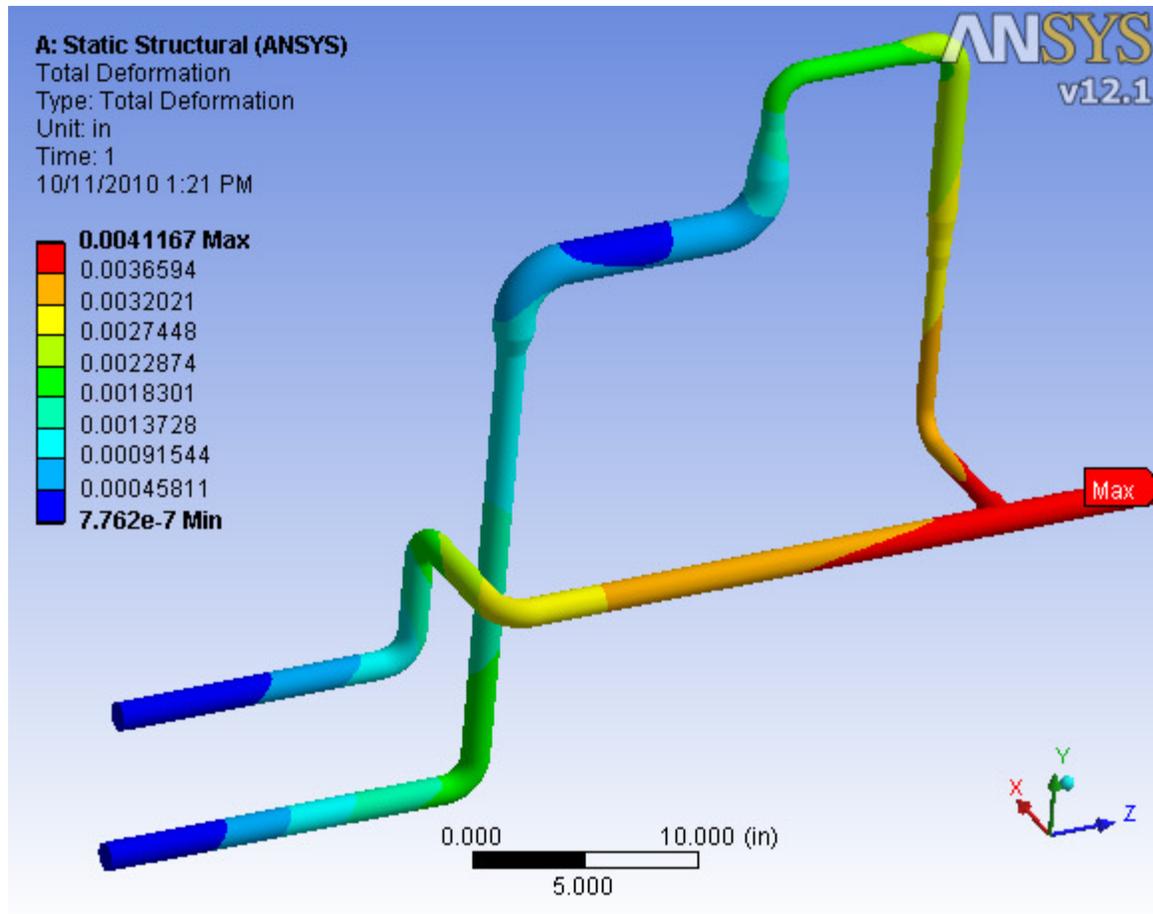
## Boundary Conditions Internal Pressure



## Stress Plot



## Deformation plot

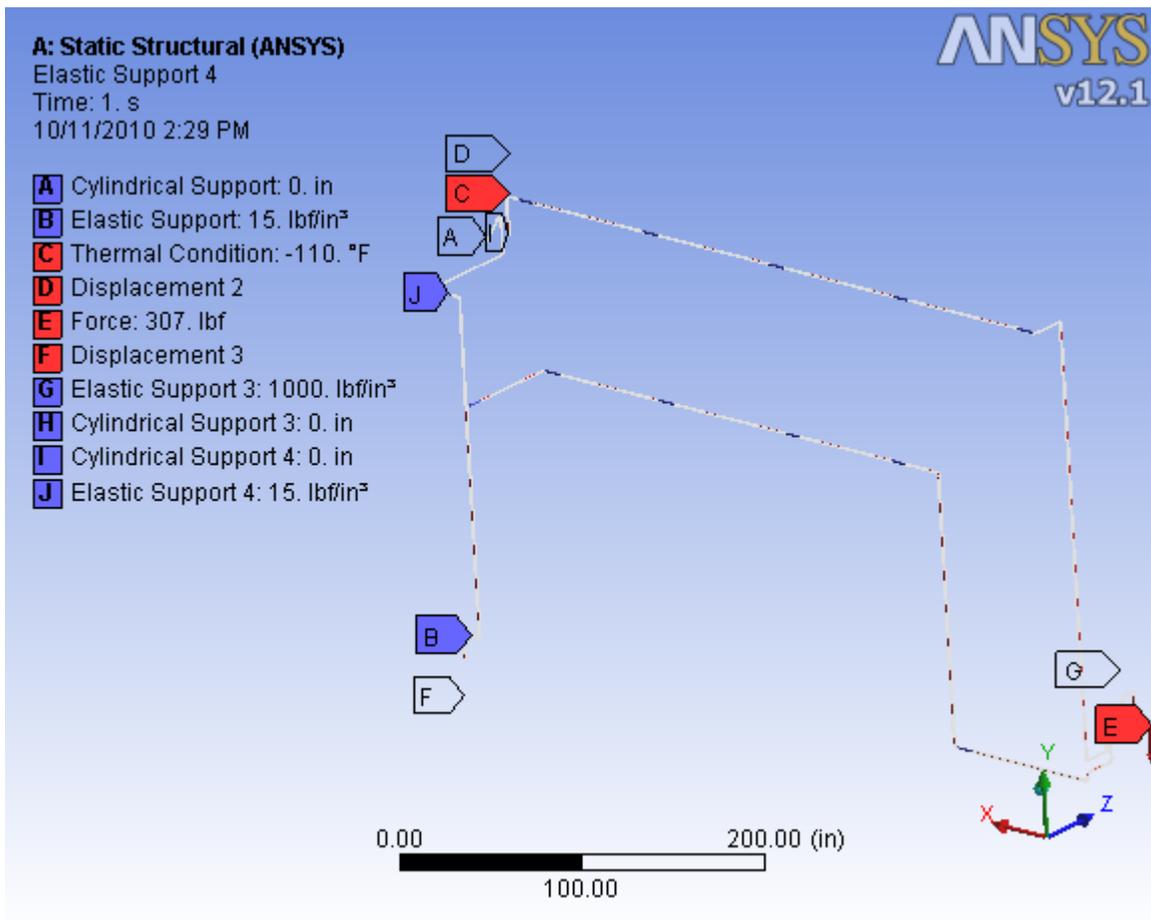


## Pipe Sections 3, 4, and 5

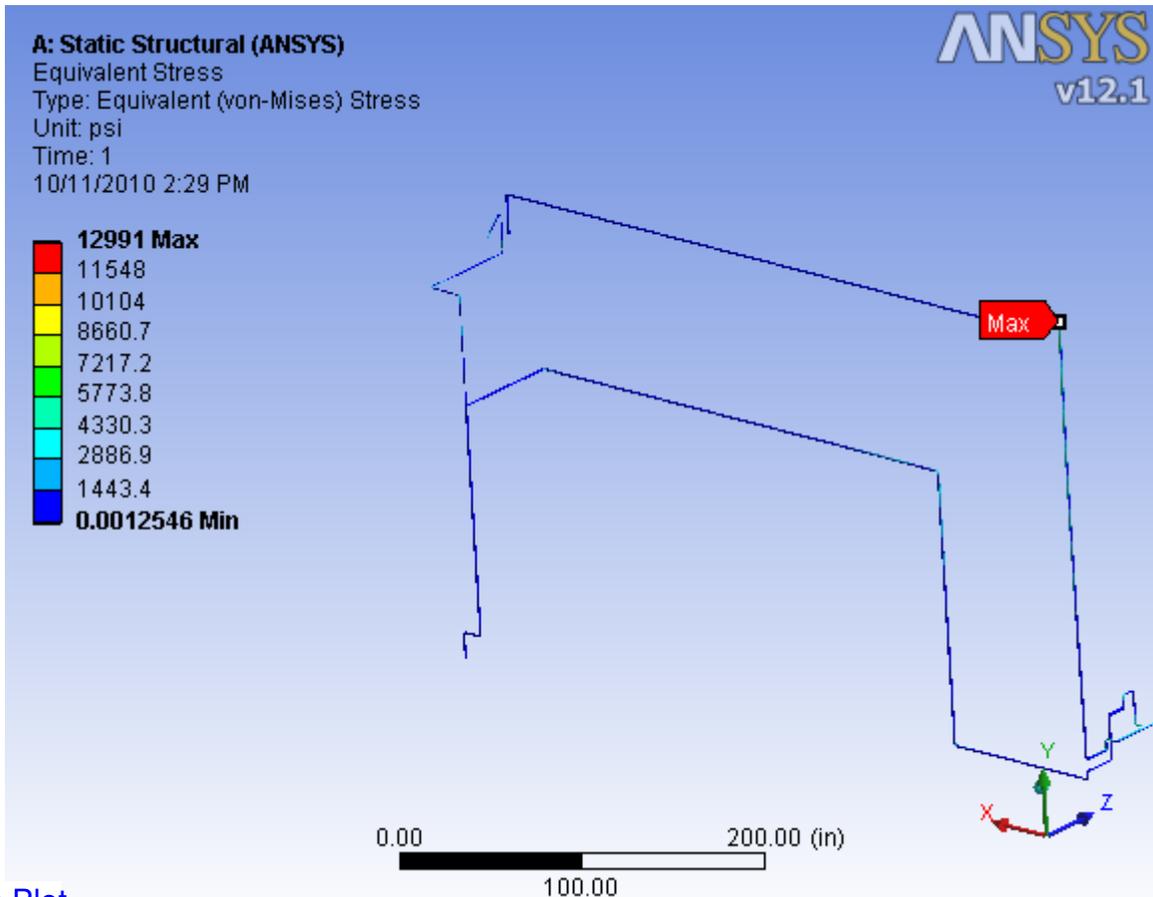
Pipe sections 3, 4, and 5 were combined as their contact points are not perfectly fixed and their displacements affect each other's stress levels. The three sections were joined in an assembly and the model was then analyzed in Ansys with the described boundary conditions (same as 3, 4, and 5) and subjected to numerous loads:

- 1.) Temperature drop from 71.6F to -110F
- 2.) Internal Pressure of 1200 psig

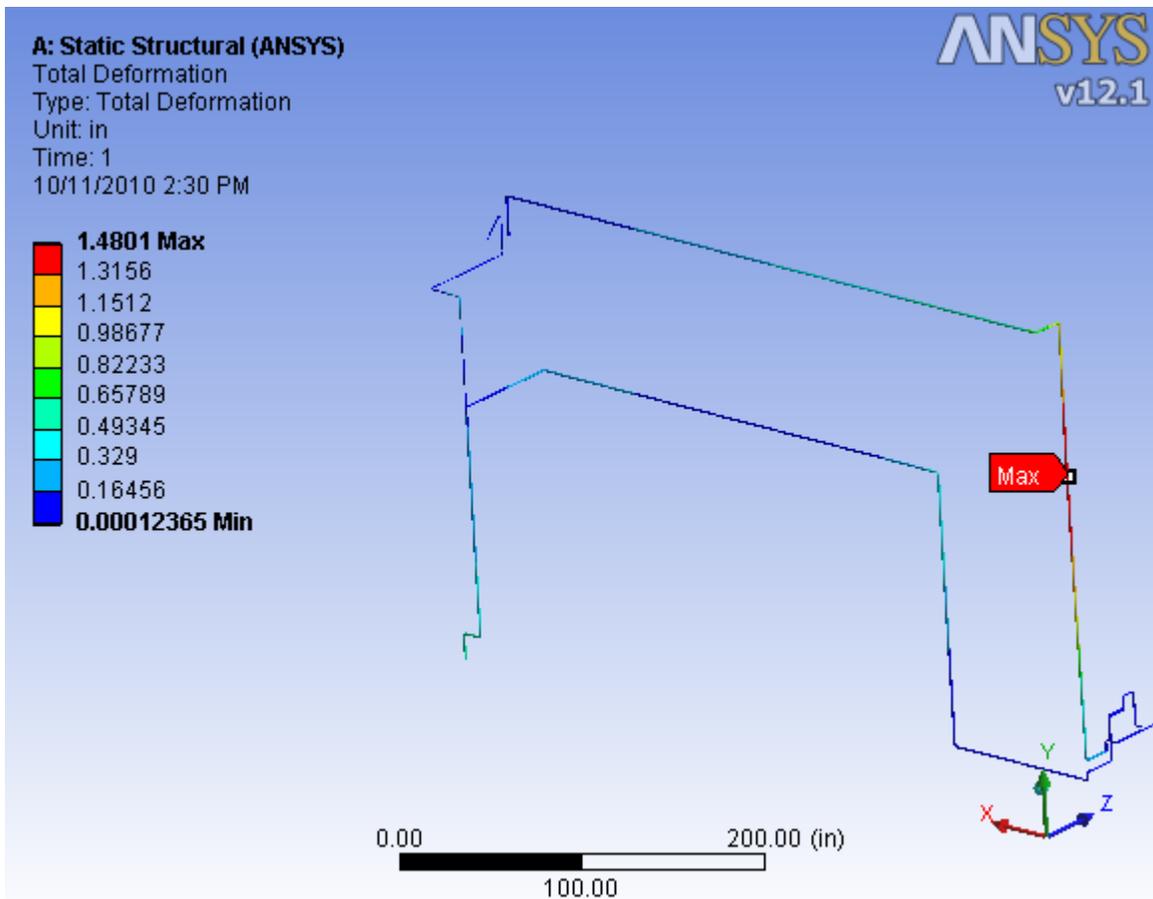
Boundary Conditions Temperature drop to -110F



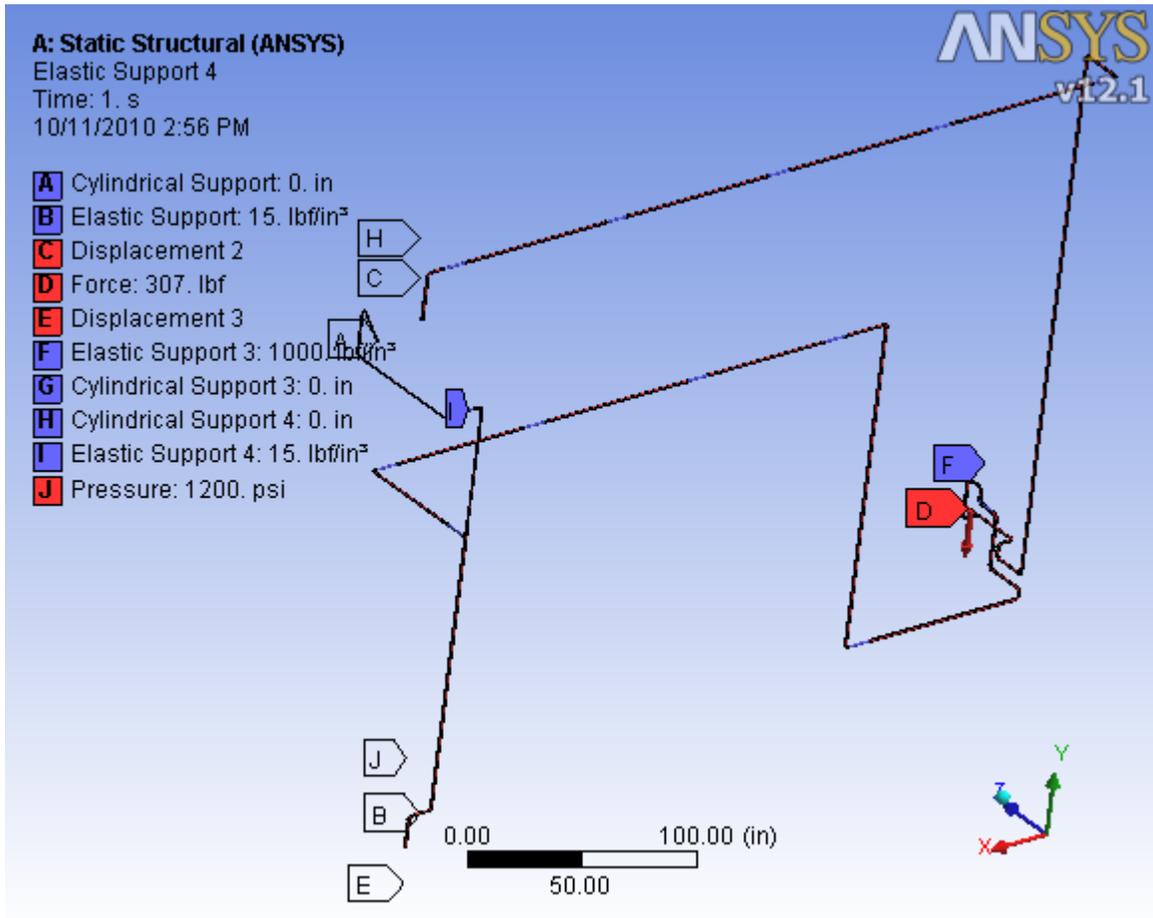
## Stress Plot



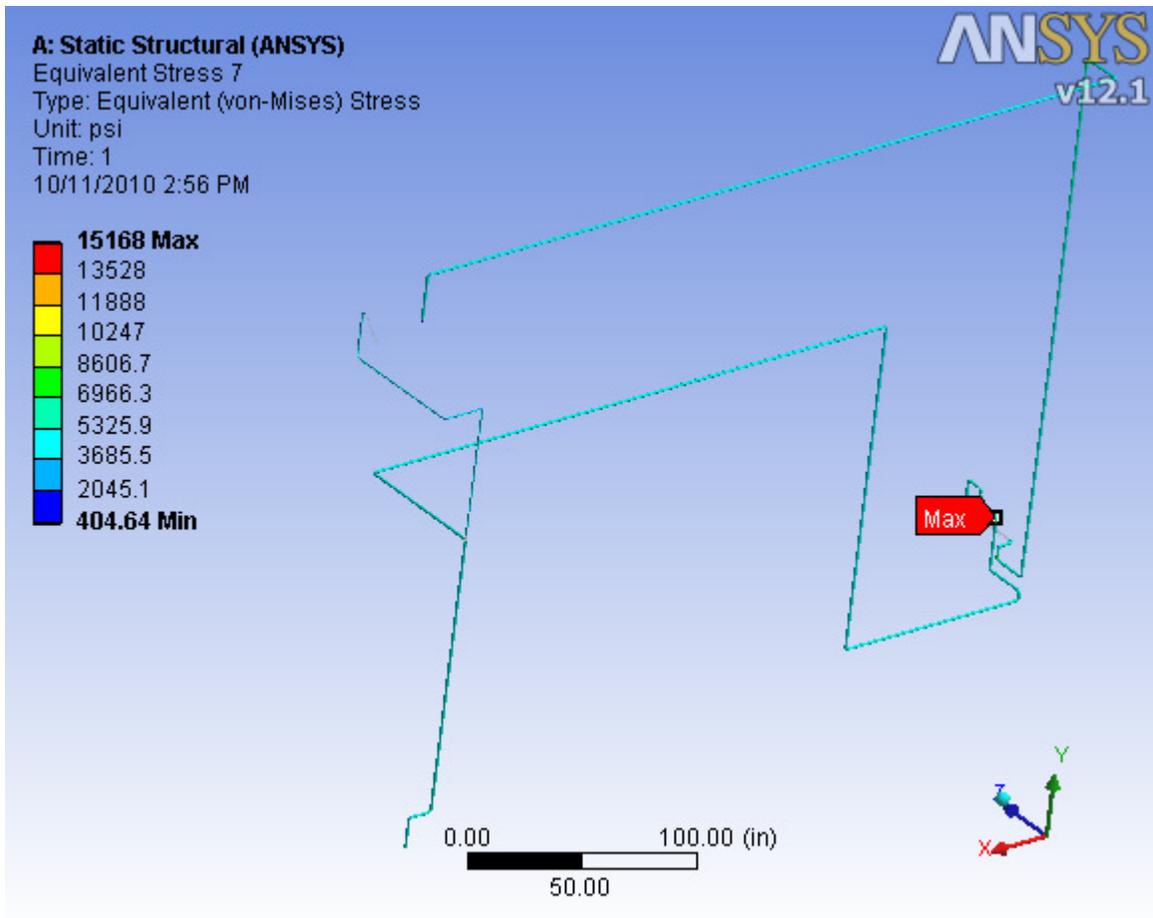
## Deformation Plot



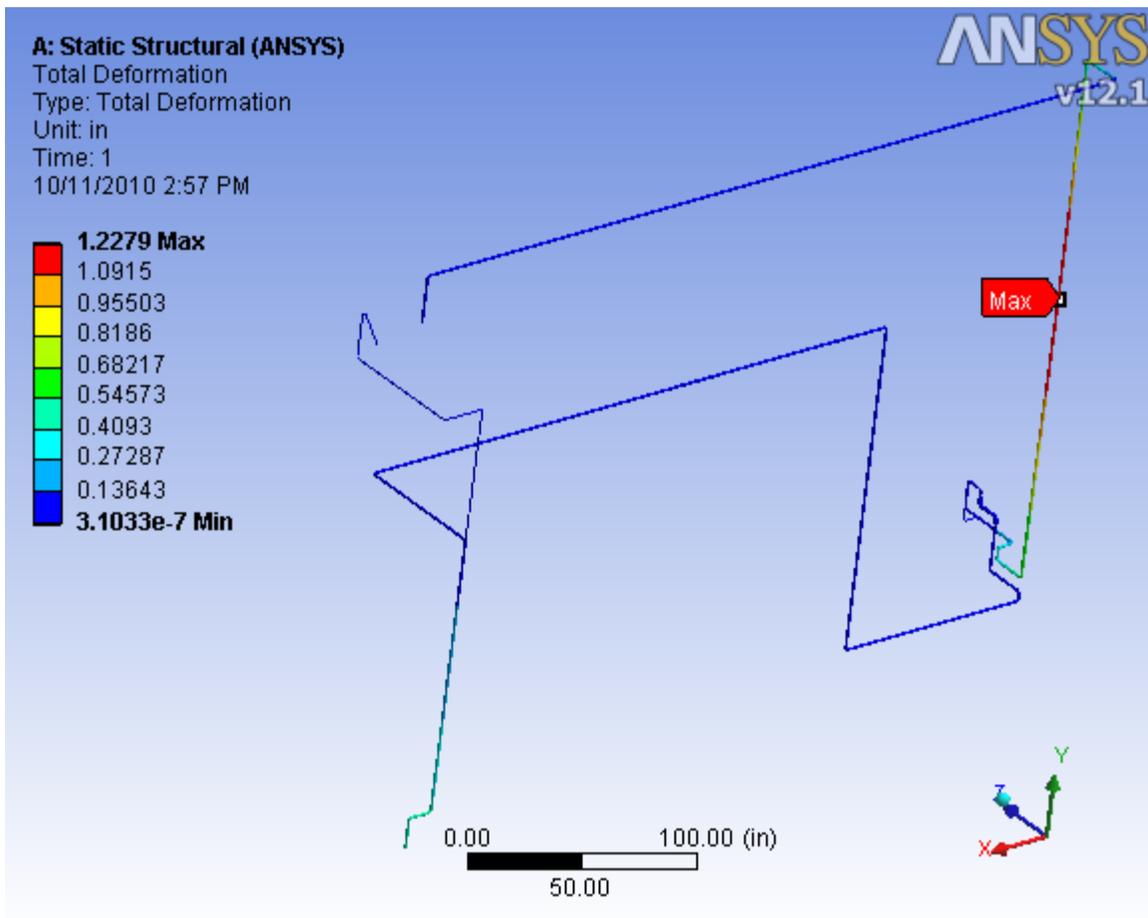
## Boundary Conditions Internal Pressure



Stress Plot



## Deformation plot



## Result Summary For sections # 3,4 and 5

The stress levels fall below the allowed 16.7 ksi in ASME 31.3 process piping code. Fittings are designed thicker than the pipe itself, and are rated for the temperature and pressure and allowed by 31.3. Stress levels the fittings should be somewhat lower than shown in the ansys model since they are modeled the same thickness as the pipe itself for a conservative approach. The pipe Tee was left out of the stress plot in the pressure analysis since it is rated to the temperature and pressure for ASME31.3. Deformation levels are reasonable and could easily be allowed by the pipe insulation and hangers without constraint.

## Pipe Section 6

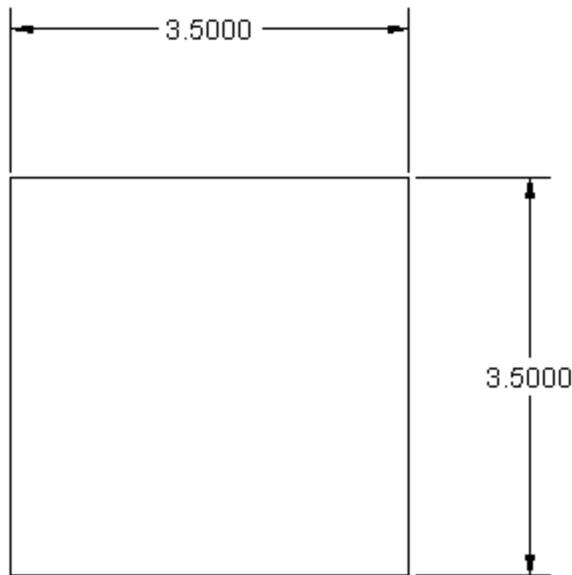
Pipe section 6 is one assembly, which comes out of the bottom of the phase separator and is unconstrained at the end. An FEA model was not performed as one end is unconstrained and is not sensitive to expansion or contraction due to temperature or pressure changes.

Pipe and equipment descriptions:

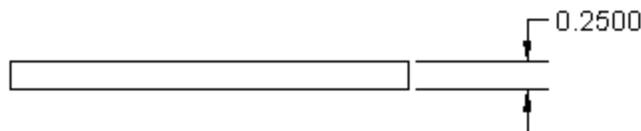
Assembly 10 - Phase Separator Bottom outlet (P.S.)						
Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1.5	1	flange	1.125			1480
1.5	2	Pipe	0.65	SW flange	SW valve	2000
1.5	3	Valve	5			1480
1.5	4	Pipe	0.25	SW Valve	Butt Elbow	2000
1.5	5	Elbow	r = 2.25	Butt Pipe	Butt Reducer	2000
1.5 to 1	6	reducer	2.5	Butt-elbow	Butt Pipe	2000
1	7	Pipe	2	Butt-Reducer	SW-flange	3000
1	8	Orifice Flanges	2.5			1480
1	9	Pipe	3.75	SW Flange	SW Valve	3000
1"	9.1	saddle fitting	SW-F end	Pipe 9	relief valve	3000
1	9.11	relief valve				10000 psi burst
1	10	Valve	4.22			1480
1	11	Pipe	8.5	SW valve	Butt-Tee	3000
1	11.1	saddle fitting				3000
1	11.11	sight glass				1450
1	11.2	saddle fitting				3000
1	11.21	sight glass				1450
1	11.4	saddle fitting			relief valve	3000
1	11.41	relief valve				10000 psi burst
0.25	11.3	saddle fitting			DPT	3000
1	12	Tee		Butt-Pipe 11	Butt-Tee	3000
1	12.1	Coupling				3000
1	12.11	Thermowell				20000
1	13	Tee		Butt Tee 12	Valve	3000
1	13.1	Valve				1480
1	13.2	Pipe	1	SW-Valve	SW flange	3000
1	13.3	Flange				1480
1	13.4	Blind Flange				3000
1	14	45 degree elbow				3000
1.5	15	flex pipe				1200 (4842 Burst)
1.5	16	strainer				1480
1.5	17	Pipe	2	SW-strainer	SW flange	2000
0.375	18	Saddle Fitting				3000
0.375	18.1	Nipple				3000
0.375	18.2	Valve				1480
0.375	18.3	Plug				3000
1.5	19	flange				1480

Pressure Testing:  
Block Off Plates For Storage Vessel

Since The Pressure Vessels have already been Hydrostatically Tested by the Manufacturer, the flanges will be blocked off with 1/4 in thick plates. This is done to avoid pressurizing the large volume of the storage tank. Plated were analyzed and capable of withstanding the test pressure of 1320 psi, with stress under code stress. Only the area which would be clamped in the face of the ring gasket is modeled, as the square extensions will not effect the analysis result. Quarter symmetry was used in the analysis as well to speed computation time. A drawing of the block of plates is below.

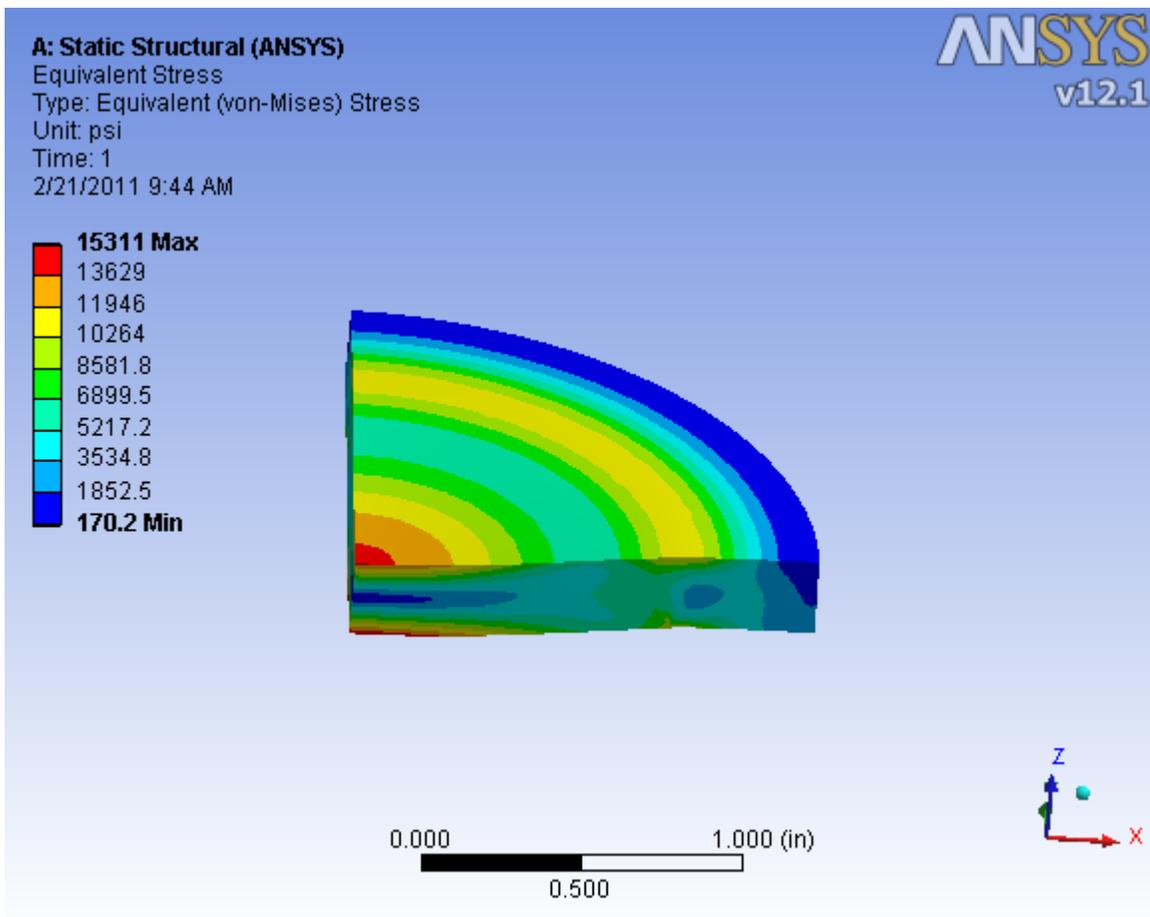
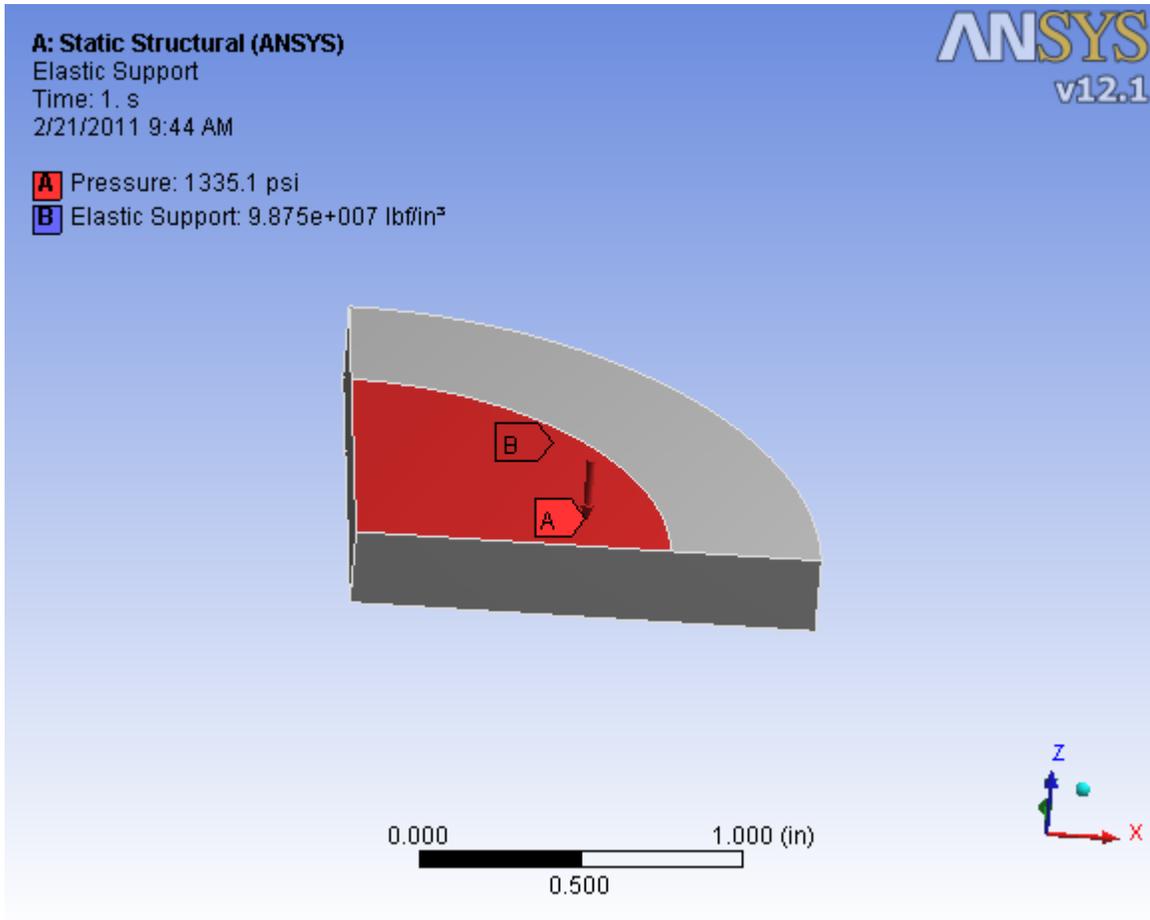


ASTM A108 Steel  
Yield Strength 45000 psi



Boundary Conditions:

Pressure in Center. Elastic support equal to flange elasticity places on bottom outside ring



#### **4. Pressure Containment / Relief System**

**Relief Valves:**

Each of the six applicable piping areas are equipped with a trapped volume relief valve. These relief valves are set to open at 1200 psig. All relief valves are Anderson Greenwood Trim KT with a size '4' orifice area equal to 0.049 in<sup>2</sup>. For specific valve numbers and locations see the [Piping and Instrument Diagram](#).

Calculations were performed which show the capacity of these valves more than meets the criteria of API 521 and ASME standards. Inlet and outlet pressure drop is below the respective allowable 3% and 10% set by API standard 521. Details of these calculations are shown in the following pages.

## **CMS Bayonet Heater Tank Relief Valve Piping and Orifice Sizing**

These MATHCAD calculations are for the Piping system relief valve, inlet, and outlet piping sizes.

Under ASME VIII-1, overpressure protection is in UG-125 to UG-136.

ASME requires that potential overpressure scenarios are identified and a method of overpressure protection be used to mitigate. Other than for fire, the larger of 10% or 3 psi overpressure is allowed. If fire exposure is possible then 21% overpressure is allowed for the fire scenario. (UG-125)

The International ISO 23251/API 521 standard is used for evaluating the overpressure scenarios and establishing a basis for design. This standard is used in conjunction with API 520 for sizing. The API 520 standard is used as a supplement to the simple capacity conversion information in ASME Sect. VIII-Div 1.

For gas flow, MATHCAD's multiple equation solving function is used to perform actual compressible flow calculations.

Per ASME, "The calculated capacity of any pressure relief system may be determined by analyzing the total system resistance to flow. This analysis shall take into consideration the flow resistance of the pipe and piping components including the exit nozzle on the vessels, elbows, tees, reducers, and valves. The calculation shall be made using accepted engineering practices for determining fluid flow through piping systems. This calculated relieving capacity shall be multiplied by a factor of 0.90 or less to allow for uncertainties inherent in this method.", UG-127(d)(1)(2), Open Flow Paths or Vents.

For evaluating the fire case, credit is taken for the fire resistant insulation and accounted for in the environment factor. The RV inlet and outlet pipe are checked with the flow that will pass through the selected orifice.

The vendor provided relief valve capacity for air will be related for Carbon Dioxide and checked against the estimated relief valve capacity.

Ref:

ASME Boiler and Pressure Vessel Code, ASME Section VIII-DIV 1, 2007

API Standard 520, Part I and II, 2008

ANSI/API Standard 521, 2007 with 2008 addendum

## **Scenario Check List (API 521)**

1. **Closed outlets** - Closed outlets are possible but are not a source of overpressure,. The available supply pressure is less than vessel design (MAWP) pressure.
2. **Coolant failure** - Not applicable.
3. **Top reflux failure** - Not applicable.
4. **Side reflux failure** - Not applicable
5. **Lean Oil failure to absorber** - Not applicable.
6. **Accumulation of noncondensables** - Not applicable,
7. **Entrance of highly volatile material** - Not applicable.
8. **Overfilling** - Overfilling is possible but is not a source of overpressure The available supply pressure less than vessel design (MAWP) pressure.
9. **Control Failure** - Heater could remain on at maximum heat input of 6000W.
10. **Abnormal heat or vapor input** - worst case would be item 9
11. **Split exchanger tube** - NA
12. **Internal explosion** - NA
13. **Chemical reaction** - NA
14. **Hydraulic expansion** - Possible and analyzed in item 8 under supercritical conditions
15. **Exterior fire** - Possible that small quantity of flammables (box/papers) are near the piping.
16. **Power failure** (steam, electric, air, other) - system stable at ambient temperatures.

Item 9, and 15 above are identified as possible sources of overpressure.

**Item 9 requires a relief rate of 330 lb/hr.**

**Item 15 requires an order of magnitude less relieving capacity, and is not the scenario of interest.**

**Vessels Anderson Greenwood relief valve is capable of venting over 7000 lb/hr of supercritical CO<sub>2</sub> and are more than adequate for safety purposes. Calculations follow:**

## Evaluation of Overpressure Scenario 9 - Heater Remains On at 6000W heat load

According to Compressed gas association, the critical temperature for which calculations should be made for relieving

a supercritical fluid are when:  $\frac{\sqrt{v}}{v \cdot \left( \frac{\delta h}{\delta v_p} \right)}$  is at a maximum. CGA states at 200 psia the maximum value for

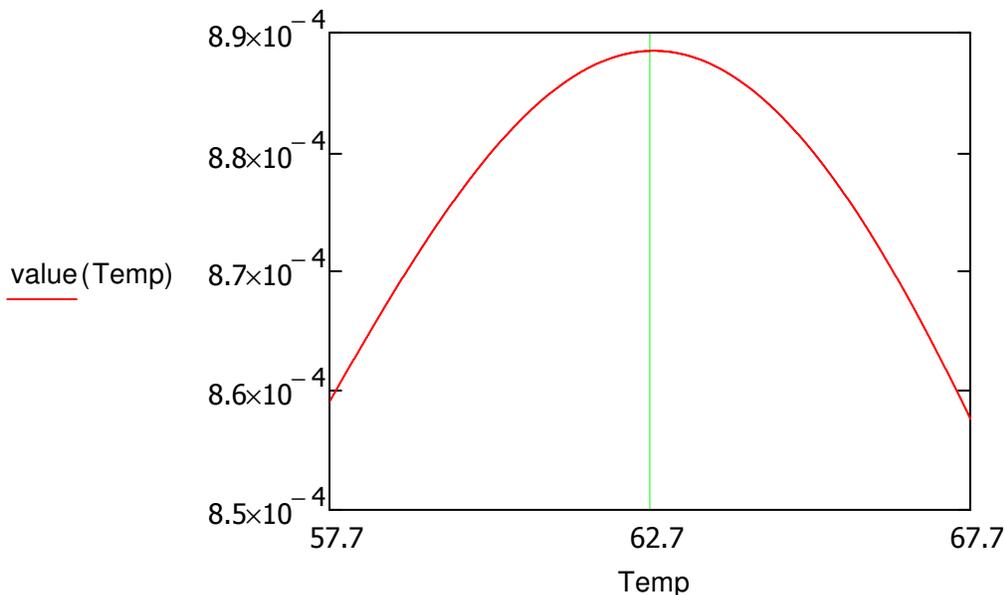
hydrogen occurs at 62.7R. A Calculation method will be tested against hydrogen's given value to test for accuracy of

the method.

$$dh_{dv}(\text{Temp}) := -0.514512683\text{Temp}^3 + 110.595964\text{Temp}^2 - 7937.122633\text{Temp} + 193723.0553$$

$$\text{rootV}(\text{Temp}) := -0.0002\text{Temp}^2 + 0.0345\text{Temp} - 1.0974$$

$$\text{value}(\text{Temp}) := \frac{1}{\left[ (dh_{dv}(\text{Temp})) \cdot (\text{rootV}(\text{Temp})) \right]}$$

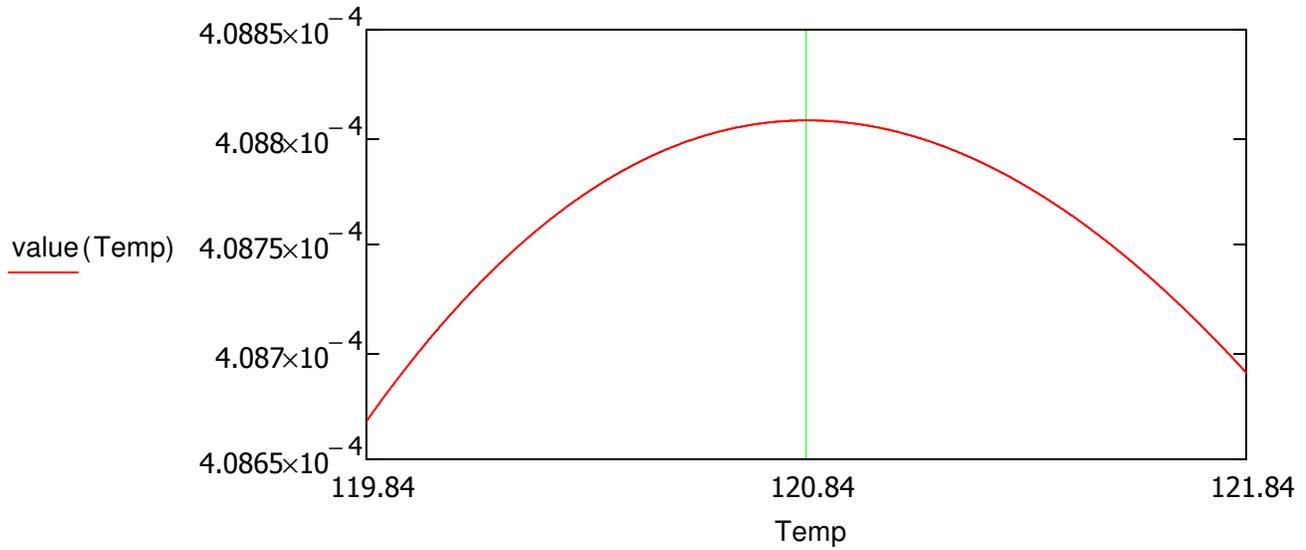
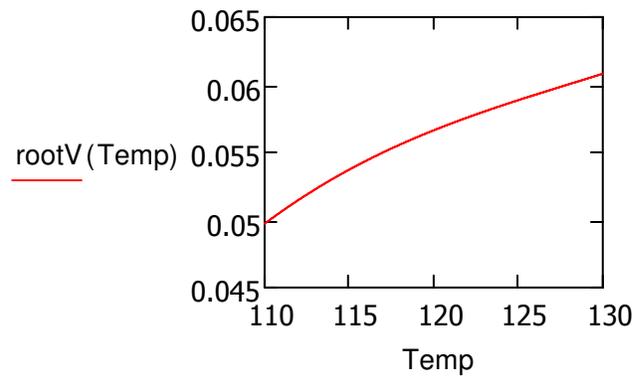
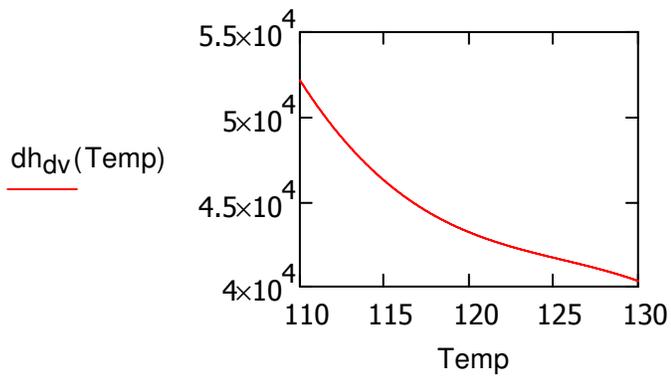


Method Works and is consistent with hydrogen gas value from Compressed gas association. The same method will be used to find the relief valve calculation Temperature of Carbon Dioxide at 1320psi

$$dh_{dv}(\text{Temp}) := -1.846799534 \cdot \text{Temp}^3 + 695.2825211\text{Temp}^2 - 87493.47076\text{Temp} + 3721622.95$$

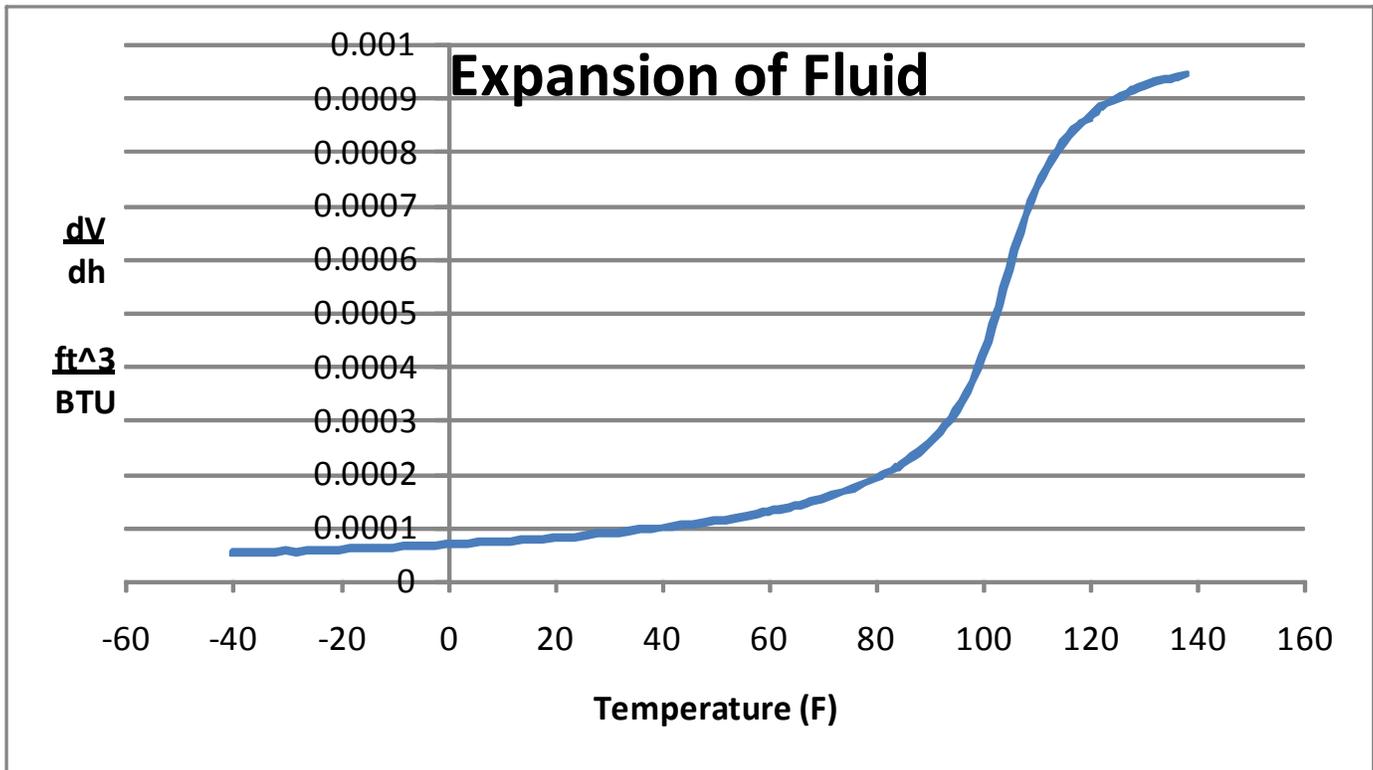
$$\text{rootV}(\text{Temp}) := 5.39422 \cdot 10^{-7}\text{Temp}^3 - 0.000207814\text{Temp}^2 + 0.027073145\text{Temp} - 1.131746719$$

$$\text{value}(\text{Temp}) := \frac{1}{\left[ (dh_{dv}(\text{Temp})) \cdot (\text{rootV}(\text{Temp})) \right]}$$



Temperature for Supercritical fluid relief calculations will be made using this temperature of 120.84 F.

This is seen as feasible when one looks at the dV/dh graph below as this derivative rises rapidly after it reaches a supercritical state then levels off quickly.



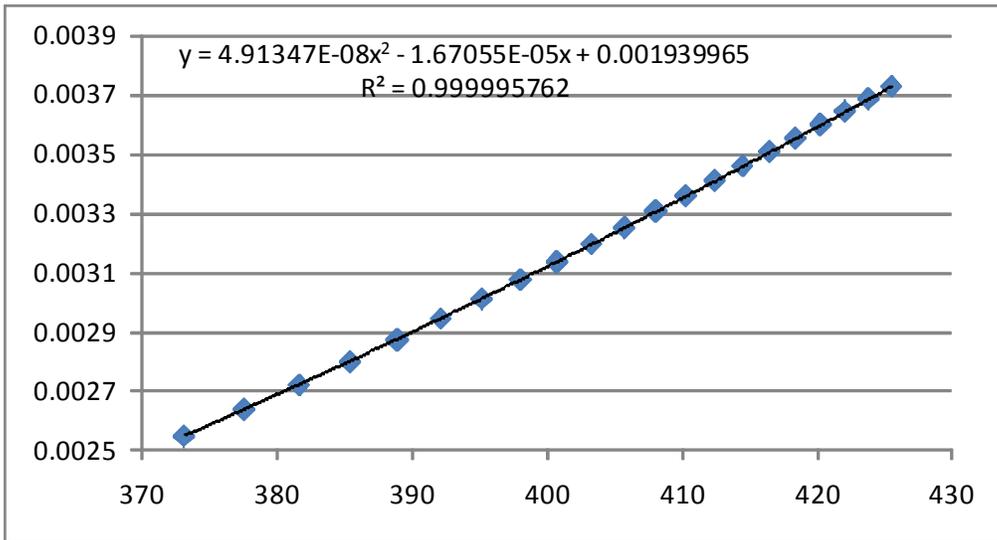
### Relief Rate Calculations

Table generated by RefProp

Temperature (°F)	Pressure (psig)	Density (kg/m <sup>3</sup> )	Volume (m <sup>3</sup> /kg)	Enthalpy (kJ/kg)	Entropy (kJ/kg-°R)	Heat of Vapor. (kJ/kg)	Viscosity (μPa-s)
108.84	1320.0	424.45	0.0023560	362.93	0.84417	Undefined	30.562
120.84	1320.0	307.50	0.0032520	405.78	0.91887	Undefined	24.165
140.84	1320.0	243.57	0.0041056	440.59	0.97792	Undefined	21.889

$$\frac{dV}{dH} \text{ is } dV_{dh} := \frac{(0.0041056 - 0.0023560) \frac{m^3}{kg}}{(440.59 - 362.93) \frac{kJ}{kg}} = 0.0008394 \cdot \frac{ft^3}{BTU} \quad dV_{dh} = 2.25 \times 10^{-5} \cdot \frac{m^3}{kJ}$$

Derivative  
approach:



$$\text{Volume}(H) := 4.91347 \cdot 10^{-8} H^2 - 1.67055 \cdot 10^{-5} H + 0.001939965$$

$$\frac{d}{dH} \text{Volume}(H) \rightarrow 9.82694e-8 \cdot H - 0.0000167055 \quad H := 405.78 \frac{\text{kJ}}{\text{kg}}$$

$$9.82694e-8 \cdot H - 0.0000167055 = 2.317 \times 10^{-5} \frac{\text{m}^3}{\text{kJ}} \quad \text{virtually the same}$$

This dV/dH value of will be used  
for relief valve sizing

$$\rho_{\text{CO}_2} := 307.50 \frac{\text{kg}}{\text{m}^3} = 19.2 \frac{\text{lb}}{\text{ft}^3}$$

$$\text{Heater}_{\text{Power}} := 6000\text{W}$$

## Required Relief Rate for scenario 9

METHOD 1 API std  
520

$$\text{ReliefRate}_{6000\text{W\_heater}} := dV_{dh} \cdot \text{HeaterPower} \cdot \rho_{\text{CO}_2} = 329.894 \cdot \frac{\text{lb}}{\text{hr}}$$

### Back Pressure Factor

$$K_b := 1.0$$

### Coefficient of discharge

$$K_d := 0.816$$

### Combination Factor

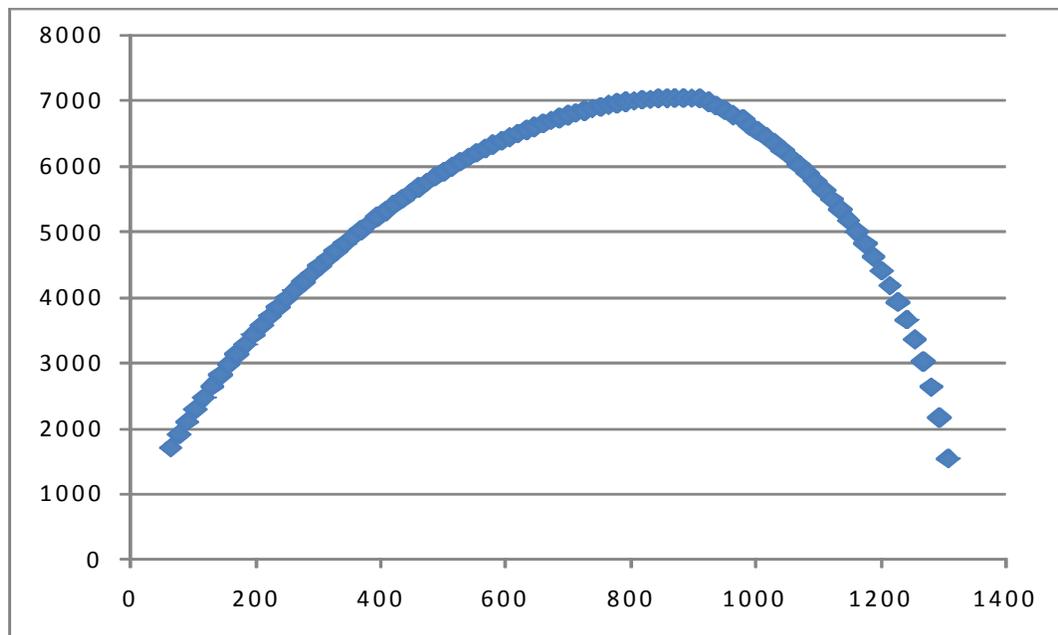
$$K_c := 1.0$$

$$IIC := K_b \cdot K_d \cdot K_c$$

$$W_R := \text{ReliefRate}_{6000\text{W\_heater}}$$

### Theoretical Mass flux rate

$$G := 7030.31 \frac{\text{lb}}{\text{s} \cdot \text{ft}^2} \quad \text{found by methods listed in API std 520}$$



### (API std 520 equation B.5)

$$W_R = G \cdot \text{Area}_{\text{orifice}} \cdot IIC$$

$$\text{Area}_{\text{orifice}} := \frac{W_R}{G \cdot IIC} = 0.0023 \cdot \text{in}^2$$

This area seems extremely small, however with a calculated relief pressure of 1320 psi the calculation may be accurate. Supercritical fluids also have a relatively low viscosity and high permeability causing them to flow quite easily, and needing only small orifice to relieve from. Subsequent orifice calculations will follow to test for consistency.

## Required Relief Rate for scenario 9

## METHOD 2

### Relief Rate

$$W_R = 329.9 \cdot \frac{\text{lb}}{\text{hr}}$$

### Unitless Relief Rate

$$W_u := \frac{W_R}{\frac{\text{lb}}{\text{hr}}}$$

### Compressibility factor

$$Z := .49103$$

### Coeff. of Discharge

$$K_1 := K_d = 0.816$$

### C Value for CO2

$$C := 345$$

### Backpressure Coefficient

$$K_b = 1$$

### Molecular weight

$$M := 44$$

### 10% Overpressure

$$P_1 := 1320$$

### Absolute

$$T := (120.8 + 460)$$

$$\text{Area} := \frac{W_u \cdot \sqrt{T} \cdot \sqrt{Z}}{C \cdot K_1 \cdot P_1 \cdot K_b \cdot \sqrt{M}} = 0.0023 \text{ in}^2 \text{ which is very consistent with the previous method}$$

## Evaluation of Overpressure Scenario 15 - Exterior Fire

Calculate relief rate based on a blocked in fire scenario

Per API 521 sec. 5.15.1.1

To determine vapor generation, it is necessary to recognize only the portion of the piping that is wetted by its internal liquid and is equal to or less than 25 ft above the flame, in this case the entire blocked in area tank and surrounding piping will be evaluated for a worst case scenario.

### Relief valve Set Pressure vessel Design P (MAWP)

$$P_{\text{set}} := 1200 \cdot \text{psi}$$

### Equivalent Length of Longest length of pipe Blocked in pipe Vessel

$$L_E := 60 \text{ft}$$

### 1" schedule 10 Pipe ID:

$$D := 1.097 \text{in}$$

### Total Wetted Surface Area:

$$\text{Pipe}_{\text{area}} := \pi \cdot D \cdot L_E = 17.23 \text{ft}^2$$

**Physical Properties of supercritical fluid @ Relieving Conditions:**

<b>Molecular Weight</b>	<b>Supercritical Temperature at relieving pressure</b>	<b>Gas Compressibility</b>	<b>Heat Capacity Ratio</b>
$M_w := 44.01 \cdot \frac{\text{kg}}{\text{kgmole}}$	$T_{in} := (120.84 + 460)R$	$Z := 0.49103$	$\gamma := 4.3081$
	<b>Heat Capacity</b>	<b>Viscosity</b>	
	$C_{pgas} := 2.3788 \cdot \frac{\text{kJ}}{\text{kg} \cdot \text{K}}$	$\mu := 24.165 \mu\text{Pa} \cdot \text{s}$	

**Determination of Insulation Credit (per API 521 5.15.5.4)**

This vessel will have either fiberglass insulation which will not burn.

Engineering Judgment:

Lab C is equipped with a fire alarm that will call the Fermilab fire department. Response time would be on the order of minutes.

Fermilab fire department is trained in dealing with cryogen containing vessels. As part of the CMS project they will receive a walkthrough of the CMS tank and associated equipment.

It is plausible that there could be a flammable box or papers near this vessel. Given the above, an insulation credit can be taken in the fire heat input calculation as specified in API 521.

The API 521 fire input rate will be used.

**Insulation Thermal Conductivity (ambient conditions)**

$$k_{ins.ambient} := 0.034 \cdot \frac{W}{m \cdot K}$$

**Insulation Thickness**

$$Insul_{Th} := 2in$$

**API Calculation for F, with units added to factor for unit consistency**

$$F := \frac{k_{ins.ambient} \cdot [(904 + 273.15)K - T_{in}]}{66570 \cdot \frac{\text{kg}}{\text{s}^3} \cdot Insul_{Th}} = 0.0086$$

API 521 eq. 13  
sect. 5.15.5.4  
The implied units of the API conversion factor are kg/sec<sup>3</sup>.

CHECK: Same calculation forcing the units choice to use the API formula in unitless fashion. The result is the same.

$$\frac{k_{\text{ins.ambient}} \cdot \frac{1}{\frac{\text{W}}{\text{m} \cdot \text{K}}} \cdot [(904 + 273.15)\text{K} - T_{\text{in}}] \cdot \frac{1}{\text{degC}}}{66570 \cdot \text{Insul}_{\text{Th}} \cdot \frac{1}{\text{m}}} = 0.0086$$

### Required Relief Rate for scenario 15 - Exterior Fire

$$Q_v := 21000 \cdot \left( \frac{\text{BTU}}{\text{hr}} \right) \cdot F \cdot \left( \frac{\text{Pipe}_{\text{area}}}{\text{ft}^2} \right)^{0.82} \quad Q_v = 1862 \cdot \frac{\text{BTU}}{\text{hr}} \quad \text{Equation from API 521}$$

$$Q_v = 545.8 \cdot W$$

$$\text{ReliefRate}_{\text{fire}} := dV_{\text{dh}} \cdot Q_v \cdot \rho_{\text{CO}_2} = 13.6 \cdot \frac{\text{kg}}{\text{hr}}$$

### Comparing Scenario Relief Rates

Rerate scenario 9 and 10 to 21% overpressure to then be comparable to fire case  
(per ASME Sect. VIII- Div.1, UG-133 (g))

Rerating is unneeded since the mass flow rate of the heater control failure is 11 times higher than the fire scenario. Heater control failure is the largest overpressure scenario and therefore will be used as the sizing basis.

$$\frac{\text{ReliefRate}_{6000\text{W\_heater}}}{\text{ReliefRate}_{\text{fire}}} = 10.99 \text{ times higher}$$

## Actual Relief Rate - Based on a selected relief valve flow chart

The following flow rate were given by the manufacturer Anderson Greenwood on their smallest orifice ("4"; 0.049in<sup>2</sup>) relief valve:  $A_s := 0.049 \cdot \text{in}^2$

### METHOD 1

$$W_{\text{Relief}} := G \cdot 0.049 \text{in}^2 \cdot \text{IIK} = 7027 \cdot \frac{\text{lb}}{\text{hr}}$$

### METHOD 2

$$W_{\text{relieved}} := \left( \frac{0.049 \cdot C \cdot K_1 \cdot P_1 \cdot K_b \cdot \sqrt{M}}{\sqrt{T} \cdot \sqrt{Z}} \right) \frac{\text{lb}}{\text{hr}} = 7152 \cdot \frac{\text{lb}}{\text{hr}}$$

### METHOD 3

$$W_{m_A} := \text{IIK} \cdot 1320 \text{psi} \cdot A_s \cdot \sqrt{\frac{\gamma \cdot M_w}{T_{\text{in}} \cdot R_g \cdot Z} \cdot \left( \frac{2}{\gamma + 1} \right)^{\frac{\gamma + 1}{\gamma - 1}}} \quad W_{m_A} = 10215 \cdot \frac{\text{lb}}{\text{hr}} \quad \text{Vol}_{\text{Relief}} := \frac{W_{m_A}}{\rho_{\text{CO}_2}}$$

Relief needed:  $W_R = 329.9 \cdot \frac{\text{lb}}{\text{hr}}$

**This shows even the smallest orifice size is 30 times oversized.  
This relief valve will be chosen for this vessel as well as all pipes**

## Check of Relief Valve Inlet Pipe Pressure Drop

Per ASME Sect. VIII- Div. 1 methods, the selected Anderson Greenwood "4" orifice relief valve has a capacity in excess of capacity estimated using the conservative methods of API 520/521.

The multiple relief valves will be mounted directly on the piping and have outlet piping which extends outdoors. the length of the longest pipe will be used as the length of the inlet pipe to be conservative.

$$\text{Length} := L_E = 60 \text{ ft}$$

$$\text{Diam} := 1.097 \text{ in} \quad \text{Area} := \frac{\pi}{4} \cdot \text{Diam}^2 = 0.9 \cdot \text{in}^2$$

$$\text{Velocity} := \frac{\text{Vol}_{\text{Relief}}}{\text{Area}}$$

$$\text{Re} := \frac{\rho_{\text{CO}_2} \cdot \text{Velocity} \cdot \text{Diam}}{\mu} = 2.4 \times 10^6$$

### Relative Roughness

$$\varepsilon := 0.046\text{mm} = 1.8 \times 10^{-3} \cdot \text{in}$$

### Colebrook Implicit equation

$$\text{Given} \quad \frac{1}{\sqrt{f}} = -2 \log \left( \frac{\varepsilon}{3.7 \text{Diam}} + \frac{2.51}{\text{Re} \cdot \sqrt{f}} \right)$$

$$f := \text{Find}(f) = 0.022359$$

### Crane 410 eq. 6-8 for head, converted to pressure

### Crane 410 eq. 6-8 (unitless to psi)

$$\Delta P := f \cdot \left( \frac{\text{Length}}{\text{Diam}} \cdot \frac{\text{Velocity}^2}{2} \cdot \rho_{\text{co2}} \right) = 15.42 \cdot \text{psi} \quad \Delta P_1 := 3.36 \cdot 10^{-6} \cdot \frac{f \cdot \frac{\text{Length}}{\text{ft}} \cdot \left( \frac{\text{Wm}_A}{\frac{\text{lb}}{\text{hr}}} \right)^2}{\frac{\rho_{\text{co2}}}{\frac{\text{lb}}{\text{ft}^3}} \cdot \left( \frac{\text{Diam}}{\text{in}} \right)^5} = 15.42$$

$$\frac{\Delta P}{1334.3 \text{psi}} = 1.1556\% \quad \text{which is less than 3\%, the inlet piping is sufficient}$$

## Check of Relief Valve Outlet Pipe Pressure Drop

Equivalent length used is conservative representation of straight pipe and fitting losses. The relief valve will be mounted on nearby piping to the vessel. Outlet piping will be routed outside. Relief valve will flash supercritical CO<sub>2</sub> into vapor/solid mixture.

Solid "snow" could plug outlet lines, therefore the largest piping size which will still yield a sonic exit velocity is desired. Properties for CO<sub>2</sub> will be used as close as possible to this relieving mixture which will be roughly 85-90% vapor quality and 10-15% solid by mass. For this calculation, 100% vapor will be analyzed to be conservative.

Temperature (°F)	Pressure (psig)	Density (lbm/ft <sup>3</sup> )	Volume (ft <sup>3</sup> /lbm)	Enthalpy (Btu/lbm)	Entropy (Btu/lbm-°R)
-68.000	5.0000	0.20624	4.8487	189.16	0.58018
-109.00	0.0000000000000037765	0.17103	5.8469	181.88	0.57381
-100.00	5.0000	0.22612	4.4225	183.16	0.56419

Comp. Factor	Heat of Vapor. (Btu/lbm)	Viscosity (lbm/ft-s)	Kin. Viscosity (ft <sup>2</sup> /s)
0.98095	Undefined	0.0000073552	0.000035663
0.97933	0.00000	Not calculated	Not calculated
0.97433	0.00000	Not calculated	Not calculated

**estimated density relieved      estimated kinematic viscosity**

$$\rho_{\text{relieved}} := 0.22612 \frac{\text{lb}}{\text{ft}^3} \quad \nu := 0.000035 \frac{\text{ft}^2}{\text{s}} \quad \text{Vol}_{\text{relieved}} := \frac{W_{m_A}}{\rho_{\text{relieved}}} = 4.5 \times 10^4 \frac{\text{ft}^3}{\text{hr}}$$

**ID of 2" schedule 10 pipe**

$$\text{Diam} := 2.157 \text{in} \quad \text{Area} := \frac{\pi}{4} \cdot \text{Diam}^2 = 3.7 \cdot \text{in}^2 \quad \text{Length} := 25 \text{ft}$$

**Comp. Factor**

$$Z := 0.97433 \quad \text{Velocity} := \frac{\text{Vol}_{\text{relieved}}}{\text{Area}} \quad \text{Re} := \frac{\text{Velocity} \cdot \text{Diam}}{\nu} = 2.5 \times 10^6$$

**Relative Roughness from Crane 410 for commercial steel pipe**

$$\epsilon := 0.00015 \text{ft}$$

### ColeBrook Implicit equation

$$\text{Given } \frac{1}{\sqrt{f}} = -2 \log \left( \frac{\epsilon}{3.7 \text{Diam}} + \frac{2.51}{\text{Re} \cdot \sqrt{f}} \right)$$

$$f := \text{Find}(f) = 0.01894$$

### mass flow rate

$$q_m := \frac{W_{m_A}}{\frac{\text{lb}}{\text{hr}}} = 10215.4$$

### diameter of outlet pipe

$$d := \frac{\text{Diam}}{\text{ft}} = 0.18$$

### outlet pressure

$$p_2 := 14.3$$

### -100F outlet temperature

$$T_{\text{outlet}} := (460 - 100)$$

### outlet piping

$$L := \frac{\text{Length}}{\text{ft}} = 25$$

### Mach number

$$\text{Ma}_2 := 1.702 \cdot 10^{-5} \cdot \left( \frac{q_m}{p_2 \cdot d^2} \right) \cdot \left( \frac{Z \cdot T_{\text{outlet}}}{M} \right)^{0.5} = 1.062$$

Using equation 26 from API std 521 to find the pressure ( $p_2$ ) just after the relief valve

$$\frac{f \cdot L}{d} = \frac{1}{\text{Ma}_2^2} \cdot \left( \frac{p_1}{p_2} \right)^2 \cdot \left[ 1 - \left( \frac{p_2}{p_1} \right)^2 \right] - \ln \left( \frac{p_1}{p_2} \right)^2$$

$$p_1 := \text{Find}(p_1) = 30.8$$

$$\Delta P := (p_1 - p_2) \text{psi} = 16.5 \text{psi}$$

$$\frac{\Delta P}{1334.3 \text{psi}} = 1.2 \cdot \%$$

### check for sonic flow speed

$$p_{\text{crit}} := 1.702 \cdot 10^{-5} \cdot \left(\frac{q_m}{d^2}\right) \cdot \left(\frac{Z \cdot T}{M}\right)^{0.5} = 19.3$$

Which is above the outlet pressure showing we have sonic flow. High velocity flow is desirable in a CO2 relieving system to be sure the outlet piping will be swept of solid CO2.

from API std 521

If the critical pressure is less than the pipe outlet pressure, the flow is subsonic. If the critical pressure is greater than the pipe outlet pressure, the flow is sonic and  $Ma_2 = 1$ . Therefore, the pipe inlet pressure,  $p_1$ , is calculated from Equation (25) with  $p_2$  equal to the critical pressure.

$$\frac{f \cdot l}{d} = \frac{1}{Ma_2^2} \left[ \left(\frac{p_1}{p_2}\right)^2 \right] \left[ 1 - \left(\frac{p_2}{p_1}\right)^2 \right] - \ln \left(\frac{p_1}{p_2}\right)^2 \quad (26)$$

### recalculated for sonic flow speed

$$Ma_2 := 1 \quad p_2 := p_{\text{crit}}$$

$$\frac{f \cdot L}{d} = \frac{1}{Ma_2^2} \cdot \left(\frac{p_1}{p_2}\right)^2 \cdot \left[ 1 - \left(\frac{p_2}{p_1}\right)^2 \right] - \ln \left(\frac{p_1}{p_2}\right)^2 \quad p_1 := \text{Find}(p_1) = 39.3$$

$$\Delta P := (p_1 - p_2) \text{psi} = 20 \text{ psi}$$

$$\frac{\Delta P}{1334.3 \text{ psi}} = 1.5\% \quad \text{which is less than 10\%, the outlet piping is sufficient}$$

This calculation was done for 25 feet of 2" pipe. Other relief valves are 1" diameter pipes, though their length is much shorter, up to only 5.5 feet.

## Check of Relief Valve Outlet Pipe Pressure Drop with shorter 1" outlet

### ID of 1" schedule 10 pipe

$$\text{Diam} := 1.097\text{in} \qquad \text{Area} := \frac{\pi}{4} \cdot \text{Diam}^2 = 0.9 \cdot \text{in}^2 \qquad \text{Length} := 5.5\text{ft}$$

### Comp. Factor

$$Z := 0.97433 \qquad \text{Velocity} := \frac{\text{Vol}_{\text{relieved}}}{\text{Area}} \qquad \text{Re} := \frac{\text{Velocity} \cdot \text{Diam}}{\nu} = 5 \times 10^6$$

### Relative Roughness from Crane 410 for commercial steel pipe

$$\epsilon := 0.00015\text{ft}$$

### Colebrook Implicit equation

$$\text{Given} \quad \frac{1}{\sqrt{f}} = -2 \log \left( \frac{\epsilon}{3.7 \text{Diam}} + \frac{2.51}{\text{Re} \cdot \sqrt{f}} \right) \qquad f := \text{Find}(f) = 0.022279$$

### mass flow rate

$$q_m := \frac{W_{mA}}{\frac{\text{lb}}{\text{hr}}} = 10215.4$$

### diameter of outlet pipe

$$d := \frac{\text{Diam}}{\text{ft}} = 0.091$$

### outlet pressure

$$p_2 := 14.3$$

### -100F outlet temperature

$$T_{\text{outlet}} := (460 - 100)$$

### outlet piping

$$L := \frac{\text{Length}}{\text{ft}} = 5.5$$

### Mach number

$$\text{Ma}_2 := 1.702 \cdot 10^{-5} \cdot \left( \frac{q_m}{p_2 \cdot d^2} \right) \cdot \left( \frac{Z \cdot T_{\text{outlet}}}{M} \right)^{0.5} = 4.108$$

Using equation 26 from API std 521 to find the pressure (p2) just after the relief valve

$$\frac{f \cdot L}{d} = \frac{1}{Ma_2^2} \cdot \left(\frac{p_1}{p_2}\right)^2 \cdot \left[1 - \left(\frac{p_2}{p_1}\right)^2\right] - \ln\left(\frac{p_1}{p_2}\right)^2$$

$$p_1 := \text{Find}(p_1) = 156.9$$

$$\Delta P := (p_1 - p_2)\text{psi} = 142.6\text{psi}$$

$$\frac{\Delta P}{1334.3\text{psi}} = 10.7\%$$

### check for sonic flow speed

$$p_{\text{crit}} := 1.702 \cdot 10^{-5} \cdot \left(\frac{q_m}{d^2}\right) \cdot \left(\frac{Z \cdot T}{M}\right)^{0.5} = 74.6$$

Which is above the outlet pressure showing we have sonic flow. High velocity flow is desirable in a CO2 relieving system to be sure the outlet piping will be swept of solid CO2.

### recalculated for sonic flow speed

$$Ma_2 := 1 \quad p_2 := p_{\text{crit}}$$

$$\frac{f \cdot L}{d} = \frac{1}{Ma_2^2} \cdot \left(\frac{p_1}{p_2}\right)^2 \cdot \left[1 - \left(\frac{p_2}{p_1}\right)^2\right] - \ln\left(\frac{p_1}{p_2}\right)^2$$

$$p_1 := \text{Find}(p_1) = 119.4$$

$$\Delta P := (p_1 - p_2)\text{psi} = 44.8\text{psi}$$

$$\frac{\Delta P}{1334.3\text{psi}} = 3.4\%$$

Which is less than 10%, the outlet piping is sufficient

## **5. Welding Information**

The transfer line was assembled in two phases due to the long lengths and bends would be impossible to move through doorways and such. Maneuverable sections of the piping were fabricated in Lab F, MAB, and PC4. These sections were then joined and connected either by welding, Hart Unions, or flanges once in place. According to B31.3 Section 341, all piping in Normal Fluid Service shall be examined. Normally radiographic examination of at least 5% of the welds is required but in certain cases where the use of radiographic examination is difficult or impossible in-process examination is allowed in lieu of radiography. The shop fabrication was done by multiple Fermilab welders. Their qualifications are in section 6. An argon gas purge was used before and while performing all piping welds.

## **6. Welders Qualifications**



# Fermi National Accelerator Laboratory

Technical Division-Machine Shop

## Welder Performance Qualification Record

<b>Welder's Name</b>	Michael Cooper			<b>FNAL #</b>	12271N	<b>ASME #</b>	W-7
<b>Welding Process:</b>	Ist	GTAW	Type	Manual	2nd	Type	
Performed in accordance with:		Fermi WPS-SS-8-001					

<b>Joint:</b>	<b>Fillet:</b>	Production Weld		Test Coupon		
<b>Groove:</b>	<b>Double Welded:</b>	Yes	No			
	<b>Single Welded:</b>	Metal Fused		Metal Non-Fused	Non-Metal	Open Root
		With Solid Backing		Without Solid Backing		

<b>Base Metal:</b>	Specification:	SA 213, Type 304/304L	TO	SA 213, Type 304/304L	ASME P #8, Gp 1	TO	ASME P # 8, Gp 1
<b>Plate</b>	<b>Pipe</b>			<b>Tube</b>			
Actual Thickness:	Nominal Diameter:		Actual Diameter		Overall Diameter: 0.250"		
Qualified Range:	Wt/Schedule:		Qualified Thickness Range		Wall: 0.035"		
	Actual Thickness		Qualified Diameter Range:		Qualified Thickness Range: 0.070" Maximum		
				Qualified Diameter Range: 0.250" Minimum			

<b>Filler:</b>	<b>1<sup>st</sup> Process</b>			<b>2<sup>nd</sup> Process</b>		
	Specification: 5.9	Class: 308/308L		Specification:	Class:	
	Diameter(s): .035, .045, 1/16			Diameter(s):		
	F #: 6			F #:		
Deposit Thickness: 0.035	Range Qualification: 0.070 Maximum			Deposit Thickness:	Range Qualification:	

<b>Welding Position:</b> 6G	<b>If Vertical:</b> Uphill Down					
<b>Gas (Type &amp; Composition):</b>	Shielding: Argon 99.9%			Root Side Backing - Argon 99.9%		
<b>Electrical Characteristics</b>	Type Current	AC	DCSP	DCEN		
	Transfer-GMAW		Spray	Globular	Pulse	Short Circuit

<b>Visual Inspection</b>					
Appearance:	Satisfactory	Undercut:	None	Piping Porosity:	None

<b>Guided Bend Test</b>					
Type and Figure	Results	Type and Figure	Results	Type and Figure	Results
Test Conducted by:			Lab Test #:	Date:	

<b>Radiographic Test</b>			
Results: Satisfactory	Per ASME IX-2007 and AWS D1.1-06		
Radiographer: Alloyweld Inspection Co., Inc.	Examiner: Jennifer Anaya-Level II	Register # 5304	Date: 6/7/2010

<b>Fillet Weld Test Results</b>			
Fracture Test:			
(Location, Nature, and size of Crack or Tear in Specimen)			
Length of Weld:	Length of Defect:		Percent of Defect
Macro Test: Fusion			
Appearance: Fillet Size	inch X	inch	<input type="checkbox"/> Convex <input type="checkbox"/> Concave
Test Conducted by:		Lab Test #:	

Test Verified by: Roger Hiller, 00362N	Verification Report #5112010-2RH		Signature
--	----------------------------------	--	-----------

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007 & AWS D1.1-06 Fermi National Accelerator Laboratory	
By: Roger Hiller 00362N	Date: 6/7/2010
Authorized Representative	



# Fermi National Accelerator Laboratory

Technical Division-Machine Shop

## Welder Performance Qualification Record

Welder's Name	Mike Cooper			FNAL #	12271N	ASME #	W-7
Welding Process:	1st	GTAW	Type	Manual	2nd	Type	
Performed in accordance with:				Fermi WPS-SS-9-002			

Joint:	Fillet:	Production Weld		Test Coupon			
Groove:	Double Welded:	Yes	No				
	Single Welded	Metal Fused		Metal Non-Fused	Non-Metal	Open Root	Consumable Insert
		With Solid Backing		Without Solid Backing			

Base Metal:	Specification:	SA 213, Type 304/304L	TO	SA 213, Type 304/304L	ASME P #8, Gp 1	TO	ASME P # 8, Gp 1
Plate		Pipe			Tube		
Actual Thickness:	Nominal Diameter:	Actual Diameter		Overall Diameter: 0.500"			
Qualified Range:	Wt/Schedule:	Qualified Thickness Range		Wall: 0.095"			
	Actual Thickness	Qualified Diameter Range		Qualified Thickness Range: 0.190" Maximum			
				Qualified Diameter Range: 0.500" Minimum			

Filler:	1 <sup>st</sup> Process			2 <sup>nd</sup> Process		
	Specification: 5.9	Class: 308/308L		Specification:	Class:	
	Diameter(s): .045, 1/16, 3/32			Diameter(s):		
	F #: 6			F #:		
	Deposit Thickness: 0.095	Range Qualification: 0.190 Maximum		Deposit Thickness:	Range Qualification:	

Welding Position: 6G	If Vertical: Uphill Down					
Gas (Type & Composition):	Shielding: Argon 99.9%		Root Side Backing - Argon 99.9%			
Electrical Characteristics	Type Current	AC	DCEP	DCEN		
	Transfer: GMAW	Spray		Globular	Pulse	Short-Circuit

Visual Inspection						
Appearance:	Satisfactory	Undercut:	None		Piping Porosity:	None

Guided Bend Test					
Type and Figure	Results	Type and Figure	Results	Type and Figure	Results
Test Conducted by:			Lab Test #:	Date:	

Radiographic Test			
Results: Satisfactory		Per ASME IX-2007 and AWS D1.1-06	
Radiographer: Alloyweld Inspection Co., Inc.	Examiner: Jennifer Anaya-Level II	Register #: 5088	Date: 5/24/2010

Fillet Weld Test Results			
Fracture Test:			
(Location, Nature, and size of Crack or Tear in Specimen)			
Length of Weld:	Length of Defect:	Percent of Defect	
Macro Test: Fusion			
Appearance: Fillet Size	inch X	inch	<input type="checkbox"/> Convex <input type="checkbox"/> Concave
Test Conducted by:		Lab Test #:	

Test Verified by: Roger Hiller 00362N	Verification Report #5272010-2	
		Signature

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007 & AWS D1.1-06 Fermi National Accelerator Laboratory	
By: Roger Hiller 00362N	Date: 6/16/2010
Authorized Representative	



# Fermi National Accelerator Laboratory

Technical Division-Machine Shop

## Welder Performance Qualification Record

<b>Welder's Name</b>	Michael Cooper			<b>FNAL #</b>	12271	<b>ASME #</b>	W-7
<b>Welding Process:</b>	1st	GTAW	Type	Manual	2nd	Type	
Performed in accordance with:		Fermi WPS SS-3,R4					

<b>Joint:</b>	<b>Fillet:</b>	<b>Production Weld</b>		<b>Test Coupon</b>			
<b>Groove:</b>	<b>Double Welded:</b>	Yes	No				
	<b>Single Welded:</b>	<b>Metal Fused</b>		<b>Metal Non Fused</b>	<b>Non-Metal</b>	<b>Open Root</b>	<b>Consumable Insert</b>
		<b>With Solid Backing</b>		<b>Without Solid Backing</b>			

<b>Base Metal:</b>	<b>Specification:</b>	SA 312, Gr 304	<b>TO</b>	SA 312, Gr 304	<b>ASME P #8</b>	<b>TO</b>	ASME P # 8
<b>Plate</b>	<b>Pipe</b>				<b>Tube</b>		
<b>Actual Thickness:</b>	<b>Nominal Diameter:</b>	4	<b>Actual Diameter:</b>	4.5"	<b>Overall Diameter:</b>		
<b>Qualified Range:</b>	<b>Wt/Schedule:</b>	Sch. 80	<b>Qualified Thickness Range:</b>		0-0.674		
	<b>Actual Thickness:</b>	0.337	<b>Qualified Diameter Range:</b>		2.875" minimum		
					<b>Qualified Thickness Range:</b>		
					<b>Qualified Diameter Range:</b>		

<b>Filler:</b>	<b>1<sup>st</sup> Process</b>			<b>2<sup>nd</sup> Process</b>		
	<b>Specification:</b>	SFA 5.9	<b>Class:</b>	ER 308/308L	<b>Specification:</b>	
	<b>Diameter(s):</b>	1/16", 3/32"			<b>Diameter(s):</b>	
	<b>F #:</b>	6			<b>F #:</b>	
	<b>Deposit Thickness:</b>	0.337"	<b>Range Qualification:</b>	0-0.674"	<b>Deposit Thickness:</b>	
					<b>Range Qualification:</b>	

<b>Welding Position:</b>	6G	<b>If Vertical:</b>	Upward	Down
<b>Gas (Type &amp; Composition):</b>		<b>Shielding:</b>	Argon 99.9%	
<b>Electrical Characteristics</b>	<b>Type Current</b>	AC	<b>DCEP</b>	DCEN
	<b>Transfer</b>	GMAW	Spray	Globular
			Pulse	Short-Circuit

<b>For Information Only</b>		<b>Machine Welding</b>		
<b>Filler Metal Trade Name:</b>		<b>Control:</b>	<input type="checkbox"/> Visual	<input type="checkbox"/> Remote Visual
<b>SAW Flux Trade Name:</b>		<b>Arc Voltage Control:</b>	<input type="checkbox"/> Auto	<input type="checkbox"/> Other:
<b>Shielding Gas Trade Name:</b>		<b>Joint Tracking:</b>	<input type="checkbox"/> Yes	<input type="checkbox"/> No

<b>Visual Inspection</b>				
<b>Appearance:</b>	Satisfactory	<b>Undercut:</b>		<b>Piping Porosity:</b>

<b>Guided Bend Test</b>					
<b>Type and Figure</b>	<b>Results</b>	<b>Type and Figure</b>	<b>Results</b>	<b>Type and Figure</b>	<b>Results</b>
<b>Test Conducted by:</b>			<b>Lab Test #:</b>	<b>Date:</b>	

<b>Radiographic Test</b>			
<b>Results:</b>	Satisfactory	Per ASME IX-2007 and AWS D1.1-06	
<b>Radiographer:</b>	Alloyweld Inspection Co., Inc.	<b>Examiner:</b>	Jennifer Anaya-Level II
		<b>Register #</b>	5304
		<b>Date:</b>	6/7/2010

<b>Fillet Weld Test Results</b>			
<b>Fracture Test:(Location, Nature, and size of Crack or Tear in Specimen)</b>			
<b>Length of Weld:</b>		<b>Length of Defect:</b>	<b>Percent of Defect</b>
<b>Macro Test: Fusion</b>			
<b>Appearance: Fillet Size</b>	inch	X	inch
			<input type="checkbox"/> Convex
			<input type="checkbox"/> Concave
<b>Test Conducted by:</b>		<b>Lab Test #:</b>	

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007 & AWS D1.1-06		Fermi National Accelerator Laboratory	
<b>By:</b>		<b>Date:</b>	6/16/2010

# FERMILAB COPY

## Welder Qualification Test Record

Welder's Name Michael Cooper Ident No. 122271 Date 03/19/99

Welding Process GTAW Type Manual

Test in Accordance With WPS # ES-155003 Root Open

Material Specification SA 53-B To Material Specification SA 53-B

P-No 1 To P-No 1 Thickness .280" Diam 6"

Filler Metal Specification SFA A5.18 Classification ER-70S-2 F-No 6

Thickness Deposited .280

Backing Argon Gas Shielding Argon

Position 6-G Progression Upward

Electrical Characteristics: Current DC Polarity Straight

Thickness Qualified .560" Max Diameter Qualified 2-7/8" O.D. and over

### GUIDED BEND TEST RESULTS

Specimen No	Type	Figure	Results
1	Face	QW-462.3a	Acceptable
2	Face	QW-462.3a	Acceptable
3	Root	QW-462.3a	Acceptable
4	Root	QW-462.3a	Acceptable

Test Conducted By IFR Engineering Test No. 008-09-01 Date 3/19/99

We certify that the statements in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

By: 

Date: 4/22/99

**FERMILAB****COPY****Welder Qualification Test Record**Welder's Name Michael Cooper Ident No. 122271 Date 03/19/99Welding Process SMAW Type ManualTest in Accordance With WPS # ES-155000 Root OpenMaterial Specification SA 53-B To Material Specification SA 53-BP-No 1 To P-No 1 Thickness .432" Diam 6"Filler Metal Specification SFA A5.1 Classification E6010/E7018 F-No F3/F4Thickness Deposited .432"Backing None Gas Shielding N/APosition 6-G Progression UpwardElectrical Characteristics: Current DC Polarity ReverseThickness Qualified .864" Max Diameter Qualified 2-7/8" O.D. and over**GUIDED BEND TEST RESULTS**

<u>Specimen No</u>	<u>Type</u>	<u>Figure</u>	<u>Results</u>
1	Side	QW-462.2	Acceptable
2	Side	QW-462.2	Acceptable
3	Side	QW-462.2	Acceptable
4	Side	QW-462.2	Acceptable

Test Conducted By IFR Engineering Test No. 008-09-01 Date 3/19/99

We certify that the statements in this record are correct and that the test welds were prepared, welded and tested in accordance with the requirements of Section IX of the ASME Code.

By: Date: 4/22/99



# Fermi National Accelerator Laboratory

Technical Division-Machine Shop

## Welder Performance Qualification Record

<b>Welder's Name</b>	Michael Jeeninga			<b>FNAL #</b>	15566N	<b>ASME #</b>	W-3
<b>Welding Process:</b>	1st	GTAW	Type	Manual	2nd	Type	
Performed in accordance with:				Fermi WPS SS-3,R4			

<b>Joint:</b>	<b>Fillet:</b>	<b>Production Weld</b>		<b>Test Coupon</b>			
<b>Groove:</b>	<b>Double-Welded:</b>	Yes	No	<b>Metal Fused</b>		<b>Metal Non-Fused</b>	<b>Non-Metal</b>
	<b>Single Welded:</b>	<b>With Solid Backing</b>		<b>Without Solid Backing</b>		<b>Open Root</b>	<b>Consumable Insert</b>

<b>Base Metal:</b>	<b>Specification:</b>	SA 312, Gr 304	TO	SA 312, Gr 304	ASME P #8, Gp. 1	TO	ASME P # 8, Gp. 1
<b>Plate</b>	<b>Pipe</b>			<b>Tube</b>			
<b>Actual Thickness:</b>	Nominal Diameter: 4		Actual Diameter: 4.5"		Overall Diameter:		
<b>Qualified Range:</b>	Wt/Schedule: Sch. 80		Qualified Thickness Range: 0-0.674		Wall:		
	Actual Thickness: 0.337		Qualified Diameter Range: 2.875" minimum		Qualified Thickness Range:		
					Qualified Diameter Range:		

<b>Filler:</b>	<b>1<sup>st</sup> Process</b>			<b>2<sup>nd</sup> Process</b>		
	Specification: SFA 5.9		Class: ER 308/308L	Specification:		Class:
	Diameter(s): 1/16"Ø, 3/32"Ø			Diameter(s):		
	F #: 6			F #:		
	Deposit Thickness: 0.0337		Range Qualification: 0-0.674"		Deposit Thickness:	
					Range Qualification:	

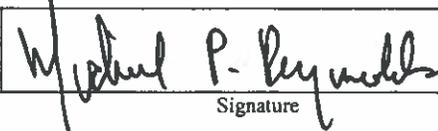
<b>Welding Position:</b>	6G	<b>If Vertical:</b>	Upward	Down			
<b>Gas (Type &amp; Composition):</b>	Shielding: Argon 99.9%		Root Side Backing		Argon 99.9%		
<b>Electrical Characteristics</b>	Type Current	AG	DCEP	DCEN			
	Transfer GMAW	Spray	Globular	Pulse	Short-Circuit		

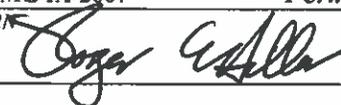
<b>Visual Inspection</b>					
<b>Appearance:</b>	Satisfactory	<b>Undercut:</b>	None Visually Observed	<b>Piping Porosity:</b>	None Visually Observed

<b>Guided Bend Test</b>					
<b>Type and Figure</b>	<b>Results</b>	<b>Type and Figure</b>	<b>Results</b>	<b>Type and Figure</b>	<b>Results</b>
<b>Test Conducted by:</b>			<b>Lab Test #:</b>	<b>Date:</b>	

<b>Radiographic Test</b>					
<b>Results:</b> Satisfactory			Per ASME IX-2007 and AWS D1.1-06		
<b>Radiographer:</b> Alloyweld Inspection Co., Inc.	<b>Examiner:</b> Jennifer Anaya-Level II	<b>Register #</b> 6469	<b>Date:</b> 8/04/2010		

<b>Fillet Weld Test Results</b>					
<b>Fracture Test:</b> (Location, Nature, and size of Crack or Tear in Specimen)					
<b>Length of Weld:</b>		<b>Length of Defect:</b>		<b>Percent of Defect</b>	
<b>Macro Test:</b> Fusion					
<b>Appearance:</b> Fillet Size		inch X	inch	<input type="checkbox"/> Convex	<input type="checkbox"/> Concave
<b>Test Conducted by:</b>			<b>Lab Test #:</b>		

<b>Test Verified by:</b> Michael Reynolds, 03993N	<b>Verification Report #</b> 7302010-1-MR	 Signature
---	---	---

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007		<b>Fermi National Accelerator Laboratory</b>	
<b>By:</b> Roger Hiller, 00362N 		<b>Date:</b> 8/04/2010	



# Fermi National Accelerator Laboratory

Technical Division-Machine Shop

## Welder Performance Qualification Record

Welder's Name	Michael Jeeninga			FNAL #	15566N	ASME #	W-3
Welding Process:	1st	GTAW	Type	Manual	2nd	Type	
Performed in accordance with:		Fermi WPS-SS-8-001					

Joint:	Fillet:	Production Weld		Test Coupon		
Groove:	Double Welded:	Yes	No			
	Single Welded:	Metal Fused	Metal Non Fused	Non-Metal	Open Root	Consumable Insert
		With Solid Backing	Without Solid Backing			

Base Metal:	Specification:	SA 213, Type 304/304L	TO	SA 213, Type 304/304L	ASME P #8, Gp 1	TO	ASME P # 8, Gp 1
Plate	Pipe			Tube			
Actual Thickness:	Nominal Diameter:	Actual Diameter		Overall Diameter: 0.250"			
Qualified Range:	Wt/Schedule:	Qualified Thickness Range		Wall: 0.035"			
	Actual Thickness	Qualified Diameter Range		Qualified Thickness Range: 0.070" Maximum			
				Qualified Diameter Range: 0.250" Minimum			

Filler:	1 <sup>st</sup> Process			2 <sup>nd</sup> Process		
	Specification: 5.9	Class: 308/308L		Specification:	Class:	
	Diameter(s): .035, .045, 1/16			Diameter(s):		
	F #: 6			F #:		
	Deposit Thickness: 0.035	Range Qualification: 0.070 Maximum		Deposit Thickness:	Range Qualification:	

Welding Position: 6G	If Vertical: Uphill Down			
Gas (Type & Composition):	Shielding: Argon 99.9%	Root Side Backing - Argon 99.9%		
Electrical Characteristics	Type Current	AG	DCEP	DCEN
	Transfer: GMAW	Spray	Globular	Pulse

Visual Inspection			
Appearance: Satisfactory	Undercut: None	Piping Porosity: None	

Guided Bend Test					
Type and Figure	Results	Type and Figure	Results	Type and Figure	Results
Test Conducted by:		Lab Test #:		Date:	

Radiographic Test			
Results: Satisfactory	Per ASME IX-2007		
Radiographer: Alloyweld Inspection Co., Inc.	Examiner: Jennifer Anaya-Level II	Register # 6469	Date: 8/4/2010

Fillet Weld Test Results			
Fracture Test:			
(Location, Nature, and size of Crack or Tear in Specimen)			
Length of Weld:	Length of Defect:	Percent of Defect	
Macro Test: Fusion			
Appearance: Fillet Size	inch X	inch	<input type="checkbox"/> Convex <input type="checkbox"/> Concave
Test Conducted by:		Lab Test #:	

Test Verified by: Roger Hiller, 00362N	Verification Report #7302010-3RH		Signature
--	----------------------------------	--	-----------

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007 & AWS D1.1-06 Fermi National Accelerator Laboratory	
By: Roger Hiller 00362N	Date: 8/04/2010
Authorized Representative	



# Fermi National Accelerator Laboratory

Technical Division-Machine Shop

## Welder Performance Qualification Record

Welder's Name	Mike Jeeninga			FNAL #	15566N	ASME #	W-3
Welding Process:	1st	GTAW	Type	Manual	2nd	Type	
Performed in accordance with:	Fermi WPS-SS-9-002						

Joint:	Fillet:	Production Weld		Test Coupon			
Groove:	Double Welded:	Yes	No				
	Single Welded	Metal Fused	Metal Non-Fused	Non-Metal	Open Root	Consumable Insert	
		With Solid Backing	Without Solid Backing				

Base Metal:	Specification:	SA 213, Type 304/304L	TO	SA 213, Type 304/304L	ASME P #8, Gp 1	TO	ASME P # 8, Gp 1
Plate	Pipe			Tube			
Actual Thickness:	Nominal Diameter:	Actual Diameter		Overall Diameter: 0.500"			
Qualified Range:	Wt/Schedule:	Qualified Thickness Range		Wall: 0.095"			
	Actual Thickness	Qualified Diameter Range		Qualified Thickness Range: 0.190" Maximum			
				Qualified Diameter Range: 0.500" Minimum			

Filler:	1 <sup>st</sup> Process			2 <sup>nd</sup> Process		
	Specification: 5.9	Class: 308/308L		Specification:	Class:	
	Diameter(s): .045, 1/16, 3/32			Diameter(s):		
	F #: 6			F #:		
	Deposit Thickness: 0.095	Range Qualification: 0.190 Maximum		Deposit Thickness:	Range Qualification:	

Welding Position: 6G	If Vertical: Uphill		Down				
Gas (Type & Composition):	Shielding: Argon 99.9%		Root Side Backing - Argon 99.9%				
Electrical Characteristics	Type Current	AC	DCEP	DCEN			
	Transfer: GMAW	Spray	Globular	Pulse	Short Circuit		

Visual Inspection						
Appearance:	Satisfactory	Undercut:	None		Piping Porosity:	None

Guided Bend Test					
Type and Figure	Results	Type and Figure	Results	Type and Figure	Results
Test Conducted by:			Lab Test #:	Date:	

Radiographic Test			
Results: Satisfactory	Per ASME IX-2007 and AWS D1.1-06		
Radiographer: Alloyweld Inspection Co., Inc.	Examiner: Jennifer Anaya-Level II	Register #: 6469	Date: 8/4/2010

Fillet Weld Test Results			
Fracture Test:			
(Location, Nature, and size of Crack or Tear in Specimen)			
Length of Weld:	Length of Defect:	Percent of Defect	
Macro Test: Fusion			
Appearance: Fillet Size	inch X	inch	<input type="checkbox"/> Convex <input type="checkbox"/> Concave
Test Conducted by:		Lab Test #:	

Test Verified by: Roger Hiller 00362N	Verification Report #7272010-2RH		Signature
---------------------------------------	----------------------------------	--	-----------

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007 & AWS D1.1-06 Fermi National Accelerator Laboratory	
By: Roger Hiller 00362N	Date: 8/04/2010
Authorized Representative	



# Fermi National Accelerator Laboratory

Technical Division-Machine Shop

## Welder Performance Qualification Record

Welder's Name	Ryan Mahoney			FNAL #	15470N	ASME #	W-2
Welding Process:	1st	GTAW	Type	Manual	2nd	Type	
Performed in accordance with:				Fermi WPS CS-5-001			

Joint:	Fillet:	Production Weld		Test Coupon			
Groove:	Double-Welded:	Yes	No	Metal Fused		Metal Non-Fused	Non-Metal
	Single V Groove:	With Solid Backing		Without Solid Backing		Open Root	Consumable Insert

Base Metal:	Specification:	ASME P # 1, Group 1	TO	ASME P # 1, Group 1
Plate	Pipe		Tube	
Actual Thickness:	Nominal Diameter:	Actual Diameter:	Overall Diameter:	2.75" Ø
Qualified Range:	Wt/Schedule:	Qualified Thickness Range:	Wall:	0.625"
	Actual Thickness:	Qualified Diameter Range:	Qualified Thickness Range:	All Thickness
			Qualified Diameter Range:	1" Ø minimum

Filler:	1 <sup>st</sup> Process			2 <sup>nd</sup> Process	
	Specification: SFA 5.18	Class: ER 70S-2	Specification:	Class:	
	Diameter(s): 1/16Ø, 3/32Ø, 1/8Ø		Diameter(s):		
	F #: 6	A #: 1	F #:		
	Deposit Thickness: 0.625"	Range Qualification: All Thickness	Deposit Thickness:	Range Qualification:	

Welding Position: 6G	If Vertical: Upward	Root Side Backing		Argon 99.99%
Gas (Type & Composition):	Shielding: Argon 99.99%	DCEN		
Electrical Characteristics	Type Current	AG	DCEP	
	Transfer: GMAW	Spray	Globular	Pulse
				Short-Circuit

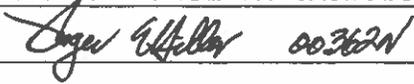
For Information Only		Machine Welding		
Filler Metal Trade Name:		Control:	<input type="checkbox"/> Visual	<input type="checkbox"/> Remote Visual
SAW Flux Trade Name:		Arc Voltage Control:	<input type="checkbox"/> Auto	<input type="checkbox"/> Other:
Shielding Gas Trade Name:		Joint Tracking:	<input type="checkbox"/> Yes	<input type="checkbox"/> No

Visual Inspection					
Appearance:	Satisfactory	Undercut:	None Visible	Piping Porosity:	None Visible

Guided Bend Test					
Type and Figure	Results	Type and Figure	Results	Type and Figure	Results
Test Conducted by:			Lab Test #:	Date:	

Radiographic Test				
Results: Satisfactory	Per ASME IX-2007 and AWS D1.1-06			
Radiographer: Alloyweld Inspection Co., Inc.	Examiner: Jennifer Anaya-Level II	Register #: 6760	Date: 8/20/2010	

Fillet Weld Test Results				
Fracture Test:				
(Location, Nature, and size of Crack or Tear in Specimen)				
Length of Weld:	Length of Defect:	Percent of Defect		
Macro Test: Fusion				
Appearance: Fillet Size	inch	X	inch	<input type="checkbox"/> Convex <input type="checkbox"/> Concave
Test Conducted by:			Lab Test #:	

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007 & AWS D1.1-06		Fermi National Accelerator Laboratory	
By:		Date:	9/01/2010

## Welder Performance Qualification Record

<b>Welder's Name</b>		<i>Ryan Mahoney</i>			<b>FNAL #</b>	<i>15470N</i>	<b>ASME #</b>	<i>W-2</i>
<b>Welding Process:</b>		<b>1st</b>	<i>GTAW</i>	<b>Type</b>	<i>Manual</i>	<b>2nd</b>	<b>Type</b>	
Performed in accordance with:		<i>Fermi WPS SS-3,R4</i>						

<b>Joint:</b>	<b>Fillet:</b>		<b>Production Weld</b>		<b>Test Coupon</b>		
<b>Groove:</b>	<b>Double Welded:</b>	<b>Yes</b>	<b>No</b>				
	<b>Single Welded:</b>	<b>Metal Fused</b>		<b>Metal Non-Fused</b>	<b>Non-Metal</b>	<b>Open Root</b>	<b>Consumable-Insert</b>
		<b>With Solid Backing</b>		<b>Without Solid Backing</b>			

<b>Base Metal:</b>	<b>Specification:</b>	<i>SA 312, Gr 304</i>	<b>TO</b>	<i>SA 312, Gr 304</i>	<b>ASME P #8</b>	<b>TO</b>	<b>ASME P # 8</b>
<b>Plate</b>		<b>Pipe</b>			<b>Tube</b>		
<b>Actual Thickness:</b>	Nominal Diameter: <i>4</i>		Actual Diameter: <i>4.5"</i>		Overall Diameter:		
<b>Qualified Range:</b>	Wt/Schedule: <i>Sch. 80</i>		Qualified Thickness Range: <i>0-0.674</i>		Wall:		
	Actual Thickness: <i>0.337</i>		Qualified Diameter Range: <i>2.875" minimum</i>		Qualified Thickness Range:		
		Qualified Diameter Range:					

<b>Filler:</b>	<b>1<sup>st</sup> Process</b>			<b>2<sup>nd</sup> Process</b>		
	Specification: <i>SFA 5.9</i>		Class: <i>ER 308/308L</i>		Specification:	
	Diameter(s): <i>1/16" Ø, 3/32" Ø</i>				Diameter(s):	
	F #: <i>6</i>				F #:	
	Deposit Thickness: <i>0.0337</i>		Range Qualification: <i>0-0.674"</i>		Deposit Thickness:	
				Range Qualification:		

<b>Welding Position:</b>	<i>6G</i>	<b>If Vertical:</b> <i>Upward</i> <b>Down</b>					
<b>Gas (Type &amp; Composition):</b>	Shielding: <i>Argon 99.9%</i>			<b>Root Side Backing</b>		<i>Argon 99.9%</i>	
<b>Electrical Characteristics</b>		<b>Type Current</b>	<b>AC</b>	<b>DCEP</b>	<b>DCEN</b>		
		<b>Transfer</b> <i>GMAW</i>		<b>Spray</b>	<b>Globular</b>	<b>Pulse</b>	<b>Short-Circuit</b>

<b>For Information Only</b>		<b>Machine Welding</b>			
<b>Filler Metal Trade Name:</b>		<b>Control:</b>	<input type="checkbox"/> <b>Visual</b>	<input type="checkbox"/> <b>Remote Visual</b>	
<b>SAW Flux Trade Name:</b>		<b>Arc Voltage Control:</b>	<input type="checkbox"/> <b>Auto</b>	<input type="checkbox"/> <b>Other:</b>	
<b>Shielding Gas Trade Name:</b>		<b>Joint Tracking:</b>	<input type="checkbox"/> <b>Yes</b>	<input type="checkbox"/> <b>No</b>	

<b>Visual Inspection</b>			
<b>Appearance:</b>	<i>Satisfactory</i>	<b>Undercut:</b>	<b>Piping Porosity:</b>

<b>Guided Bend Test</b>					
<b>Type and Figure</b>	<b>Results</b>	<b>Type and Figure</b>	<b>Results</b>	<b>Type and Figure</b>	<b>Results</b>
<b>Test Conducted by:</b>			<b>Lab Test #:</b>	<b>Date:</b>	

<b>Radiographic Test</b>			
<b>Results:</b> <i>Satisfactory</i>		Per ASME IX-2007 and AWS D1.1-06	
<b>Radiographer:</b> <i>Alloyweld Inspection Co., Inc.</i>	<b>Examiner:</b> <i>Jennifer Anaya-Level II</i>	<b>Register #</b> <i>5615</i>	<b>Date:</b> <i>6/18/2010</i>

<b>Fillet Weld Test Results</b>			
<b>Fracture Test:</b> (Location, Nature, and size of Crack or Tear in Specimen)			
<b>Length of Weld:</b>		<b>Length of Defect:</b>	<b>Percent of Defect</b>
<b>Macro Test:</b> <i>Fusion</i>			
<b>Appearance:</b> <b>Fillet Size</b>		<b>inch</b> <b>X</b> <b>inch</b>	<input type="checkbox"/> <b>Convex</b> <input type="checkbox"/> <b>Concave</b>
<b>Test Conducted by:</b>		<b>Lab Test #:</b>	

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of **ASME IX-2007** *Fermi National Accelerator Laboratory*

<b>By:</b>		<b>Date:</b>	<i>6/18/2010</i>
------------	---	--------------	------------------



# Fermi National Accelerator Laboratory

Technical Division-Machine Shop

## Welder Performance Qualification Record

Welder's Name	Ryan Mahoney			FNAL #	15470N	ASME #	W-2
Welding Process:	1st	GTAW	Type	Manual	2nd	Type	
Performed in accordance with:		Fermi WPS-SS-8-001					

Joint:	Fillet:	Production Weld		Test Coupon			
Groove:	Double Welded:	Yes	No	Metal Fused		Metal Non-Fused	Non-Metal
	Single Welded:	With Solid Backing		Without Solid Backing		Open Root	Consumable Insert

Base Metal:	Specification:	SA 213, Type 304/304L	TO	SA 213, Type 304/304L	ASME P #8, Gp 1	TO	ASME P # 8, Gp 1
Plate	Pipe			Tube			
Actual Thickness:	Nominal Diameter:	Actual Diameter		Overall Diameter: 0.250"			
Qualified Range:	Wt/Schedule:	Qualified Thickness Range		Wall: 0.035"			
	Actual Thickness	Qualified Diameter Range:		Qualified Thickness Range: 0.070" Maximum			
				Qualified Diameter Range: 0.250" Minimum			

Filler:	1 <sup>st</sup> Process			2 <sup>nd</sup> Process		
	Specification: 5.9	Class: 308/308L		Specification:	Class:	
	Diameter(s): .035, .045, 1/16			Diameter(s):		
	F #: 6			F #:		
	Deposit Thickness: 0.035	Range Qualification: 0.070 Maximum		Deposit Thickness:	Range Qualification:	

Welding Position: 6G	If Vertical: Uphill Down	
Gas (Type & Composition):	Shielding: Argon 99.9%	Root Side Backing - Argon 99.9%
Electrical Characteristics	Type Current	AC DCSP DCEN
	Transfer GMAW	Spray Globular Pulse Short Circuit

Visual Inspection			
Appearance: Satisfactory	Undercut: None	Piping Porosity: None	

Guided Bend Test					
Type and Figure	Results	Type and Figure	Results	Type and Figure	Results
Test Conducted by:			Lab Test #:	Date:	

Radiographic Test			
Results: Satisfactory		Per ASME IX-2007	
Radiographer: Alloyweld Inspection Co., Inc.	Examiner: Jennifer Anaya-Level II	Register # 5615	Date: 6/18/2010

Fillet Weld Test Results			
Fracture Test:			
(Location, Nature, and size of Crack or Tear in Specimen)			
Length of Weld:	Length of Defect:	Percent of Defect	
Macro Test: Fusion			
Appearance: Fillet Size	inch X	inch	<input type="checkbox"/> Convex <input type="checkbox"/> Concave
Test Conducted by:			Lab Test #:

Test Verified by: Roger Hiller, 00362N	Verification Report #5112010-2RH	Signature
--	----------------------------------	-----------

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007 & AWS D1.1-06 Fermi National Accelerator Laboratory	
By: Roger Hiller 00362N	Date: 6/18/2010
Authorized Representative	



# Fermi National Accelerator Laboratory

Technical Division-Machine Shop

## Welder Performance Qualification Record

<b>Welder's Name</b>	Ryan Mahoney			<b>FNAL #</b>	15470N	<b>ASME #</b>	W-2
<b>Welding Process:</b>	1st	GTAW	Type	Manual	2nd	Type	
Performed in accordance with:				Fermi WPS-SS-9-002			

<b>Joint:</b>	<b>Fillet:</b>		<b>Production Weld</b>		<b>Test Coupon</b>		
<b>Groove:</b>	Double Welded:	Yes	No				
	Single Welded	Metal Fused		Metal Non-Fused	Non-Metal	Open Root	Consumable Insert
		With Solid Backing		Without Solid Backing			

<b>Base Metal:</b>	<b>Specification:</b>	SA 213, Type 304/304L	TO	SA 213, Type 304/304L	<b>ASME P #8, Gp 1</b>	TO	<b>ASME P # 8, Gp 1</b>
<b>Plate</b>		<b>Pipe</b>			<b>Tube</b>		
Actual Thickness:	Nominal Diameter:	Actual Diameter		Overall Diameter: 0.500"			
Qualified Range:	Wt/Schedule:	Qualified Thickness Range		Wall: 0.095"			
	Actual Thickness	Qualified Diameter Range		Qualified Thickness Range: 0.190" Maximum			
				Qualified Diameter Range: 0.500" Minimum			

<b>Filler:</b>	<b>1<sup>st</sup> Process</b>			<b>2<sup>nd</sup> Process</b>		
	Specification: 5.9	Class: 308/308L		Specification:	Class:	
	Diameter(s): .045, 1/16, 3/32			Diameter(s):		
	F #: 6			F #:		
Deposit Thickness: 0.095	Range Qualification: 0.190 Maximum		Deposit Thickness:	Range Qualification:		

<b>Welding Position:</b> 6G	If Vertical: Uphill Down					
<b>Gas (Type &amp; Composition):</b>	Shielding: Argon 99.9%		Root Side Backing - Argon 99.9%			
<b>Electrical Characteristics</b>	Type Current	AC	DCEP	DCEN		
	Transfer GMAW	Spray	Globular	Pulse	Short-Circuit	

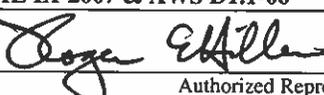
<b>Visual Inspection</b>					
Appearance:	Satisfactory	Undercut:	None	Piping Porosity:	None

<b>Guided Bend Test</b>					
Type and Figure	Results	Type and Figure	Results	Type and Figure	Results
Test Conducted by:			Lab Test #:	Date:	

<b>Radiographic Test</b>			
Results: Satisfactory		Per ASME IX-2007 and AWS D1.1-06	
Radiographer: Alloyweld Inspection Co., Inc.	Examiner: Jennifer Anaya-Level II	Register # 5615	Date: 6/18/2010

<b>Fillet Weld Test Results</b>			
Fracture Test:			
(Location, Nature, and size of Crack or Tear in Specimen)			
Length of Weld:	Length of Defect:	Percent of Defect	
Macro Test: Fusion			
Appearance: Fillet Size	inch X	inch	<input type="checkbox"/> Convex <input type="checkbox"/> Concave
Test Conducted by:	Lab Test #:		

Test Verified by: Roger Hiller 00362N	Verification Report #5272010-2	Signature
---------------------------------------	--------------------------------	-----------

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX-2007 & AWS D1.1-06 <b>Fermi National Accelerator Laboratory</b>	
By: Roger Hiller 00362N 	Date: 6/18/2010
Authorized Representative	

## **7. Inspection Plan / Examiners Report**

In accordance with ASME 31.3 code for process piping, in process weld inspection was performed on a minimum of 5% of all circumferential welds performed by each welder. The “in process weld inspection” forms are appended in the following pages.

# PPD Mechanical In-Process Weld Inspection Form

(as per In-Process Weld Inspection Guidelines, AD Cryogenics, Nov 3, 2006)

Date 12-7-10 Project: PIXELS UPGRADE CO2 COOLING

Pipe Section: A1 Weld Number: 6, 7, 8, 10, 12

Weld location: MAB

Welder: MIKE JEENINGA Inspector: OTTO BLVDREZ

**FNAL  
W-3**

WELDS  
ITEM ⑥ TO ⑦  
ITEM ⑦ TO ⑧  
ITEM ⑫ TO ⑪

### Before Welding:

Type of weld: (butt) X (other) \_\_\_\_\_

(1) Pipe #1 Size, Schedule and material: 1 1/2" SCH 10S PIPE

(2) Pipe #2 Size, Schedule and material: 1 1/2" SCH 10S ELBOW

### (1) Joint Preparation and Cleanliness

Joint Preparation and Cleanliness acceptable? YES

### (2) Welding Machine

(a) Remote foot pedal? YES

(b) DC straight machine? YES

### (3) Joint Fit-up, and Internal Alignment.

(a) Internal alignment acceptable? YES

(b) Joint Clearance acceptable? YES

(c) End Preparation acceptable? YES

### (4) Filler Rod

(a) AWS A5.9 stainless steel filler rod? YES

(b) Filler rod: Class 30BL Diameter .045" AND 1/16"

### (5) Purge Gas.

(a) type of purge gas : ARGON

(b) time length of purge: AS NEEDED purge flow rate: 10 SCFH

(b) (if done) O2 reading: 0.7 O2 Monitor manf/model : CHECK-WELD

### (6) Inspection After Root Pass

(a) No visible cracks. ✓

(b) No suck holes, which are small holes in middle of weld. ✓

(c) No porosity or obvious imperfections. ✓

(d) Filler material fused along edges of weld. ✓

(8) Repeat inspection after every pass: ✓

(9) Final Inspection: GOOD

# PPD Mechanical In-Process Weld Inspection Form

(as per In-Process Weld Inspection Guidelines, AD Cryogenics, Nov 3, 2006)

Date 12-17-10 Project: PIXELS UPGRADE CO<sub>2</sub> COOLING  
Pipe Section: A-10 Weld Number: 4, 5, 6, 7, 11, 12, 13, 14  
Weld location: MAB  
Welder: MIKE JEENIAGA Inspector: OHONLYPEZ



WELDS  
ITEM (4) TO (5)  
(5) TO (6)  
(6) TO (7)  
(11) TO (12)  
(12) TO (13)  
(13) TO (14)

Before Welding:

Type of weld: (butt) X (other) \_\_\_\_\_  
(1) Pipe #1 Size, Schedule and material: 1" SCH 10S  
(2) Pipe #2 Size, Schedule and material: 1 1/2" SCH 10S

(1) Joint Preparation and Cleanliness

Joint Preparation and Cleanliness acceptable? YES

(2) Welding Machine

(a) Remote foot pedal? YES  
(b) DC straight machine? YES

(3) Joint Fit-up, and Internal Alignment.

(a) Internal alignment acceptable? YES  
(b) Joint Clearance acceptable? YES  
(c) End Preparation acceptable? YES

(4) Filler Rod

(a) AWS A5.9 stainless steel filler rod? YES  
(b) Filler rod: Class 308L Diameter .045" + 1/16"

(5) Purge Gas.

(a) type of purge gas : ARGON  
(b) time length of purge: AS NEEDED purge flow rate: 10 SCFH  
(b) (if done) O2 reading: .07 O2 Monitor manf/model : CHECK - WELD

(6) Inspection After Root Pass

(a) No visible cracks. ✓  
(b) No suck holes, which are small holes in middle of weld. ✓  
(c) No porosity or obvious imperfections. ✓  
(d) Filler material fused along edges of weld. ✓

(8) Repeat inspection after every pass: ✓

(9) Final Inspection: GOOD

# PPD Mechanical In-Process Weld Inspection Form

(as per In-Process Weld Inspection Guidelines, AD Cryogenics, Nov 3, 2006)

Date 12-14-10 Project: PIXELS UPGRADE CO<sub>2</sub> COOLING LINES  
Pipe Section: A7 Weld Number: 22, 23, 20, 21, 18, 19  
Weld location: MAB  
Welder: MIKE JEEUNGA Inspector: OTTO DLYNDEZ

ITEM (18) TO (19)  
(20) TO (21)  
(22) TO (23)

FNAL  
W-3

Before Welding:

Type of weld: (butt) X (other) \_\_\_\_\_  
(1) Pipe #1 Size, Schedule and material: 1 1/2" SCH 10S  
(2) Pipe #2 Size, Schedule and material: 1 1/2" SCH 10S

(1) Joint Preparation and Cleanliness

Joint Preparation and Cleanliness acceptable? YES

(2) Welding Machine

(a) Remote foot pedal? YES  
(b) DC straight machine? YES

(3) Joint Fit-up, and Internal Alignment.

(a) Internal alignment acceptable? YES  
(b) Joint Clearance acceptable? YES  
(c) End Preparation acceptable? YES

(4) Filler Rod

(a) AWS A5.9 stainless steel filler rod? YES  
(b) Filler rod: Class 308L Diameter .045" + 1/16"

(5) Purge Gas.

(a) type of purge gas : ARGON  
(b) time length of purge: AS NEEDED purge flow rate: 10 SCFH  
(b) (if done) O2 reading: .06 O2 Monitor manf/model : CHECK-WE20

(6) Inspection After Root Pass

(a) No visible cracks. ✓  
(b) No suck holes, which are small holes in middle of weld. ✓  
(c) No porosity or obvious imperfections. ✓  
(d) Filler material fused along edges of weld. ✓

(8) Repeat inspection after every pass: YES

(9) Final Inspection: GOOD

# PPD Mechanical In-Process Weld Inspection Form

(as per In-Process Weld Inspection Guidelines, AD Cryogenics, Nov 3, 2006)

Date 12-13-10 Project: PIXELS UPGRADE CO<sub>2</sub> COOLING  
Pipe Section: A7 Weld Number: 2,3,6,7,8  
Weld location: MAB  
Welder: MIKE JEENINGA Inspector: OTTO OLIVER  
W-3

WELDS  
ITEM (2) TO (3)  
(6) TO (7)  
(7) TO (8)

**FNAL  
W-3**

### Before Welding:

Type of weld: (butt) X (other) \_\_\_\_\_  
(1) Pipe #1 Size, Schedule and material: 1" SCH 10S  
(2) Pipe #2 Size, Schedule and material: 1" SCH 10S

### (1) Joint Preparation and Cleanliness

Joint Preparation and Cleanliness acceptable? YES

### (2) Welding Machine

(a) Remote foot pedal? YES  
(b) DC straight machine? YES

### (3) Joint Fit-up, and Internal Alignment

(a) Internal alignment acceptable? YES  
(b) Joint Clearance acceptable? YES  
(c) End Preparation acceptable? YES

### (4) Filler Rod

(a) AWS A5.9 stainless steel filler rod? YES  
(b) Filler rod: Class 308L Diameter .045" + 1/16"

### (5) Purge Gas

(a) type of purge gas : ARGON  
(b) time length of purge: AS NEEDED purge flow rate: 10 SCFH  
(b) (if done) O2 reading: .08 O2 Monitor manf/model : CHECK - WELD

### (6) Inspection After Root Pass

(a) No visible cracks. ✓  
(b) No suck holes, which are small holes in middle of weld. ✓  
(c) No porosity or obvious imperfections. ✓  
(d) Filler material fused along edges of weld. ✓

(8) Repeat inspection after every pass: ✓

(9) Final Inspection: GOOD

# PPD Mechanical In-Process Weld Inspection Form

(as per In-Process Weld Inspection Guidelines, AD Cryogenics, Nov 3, 2006)

Date 12-8-10 Project: PIXELS UPGRADE CO<sup>2</sup> COOLING

Pipe Section: A2 Weld Number: 8, 9, 10, 11

Weld location: MAB

Welder: MIKE JEBUNGA Inspector: OTO ALVAREZ

**FNAL  
W-3**

WELDS  
ITEM (8) TO (9)  
(9) TO (10)  
(10) TO (11)

Before Welding:

Type of weld: (butt) X (other) \_\_\_\_\_

(1) Pipe #1 Size, Schedule and material: 1 1/2" SCH 10S PIPE

(2) Pipe #2 Size, Schedule and material: 1 1/2" SCH 10S ELBOW + TEE

(1) Joint Preparation and Cleanliness

Joint Preparation and Cleanliness acceptable? YES

(2) Welding Machine

(a) Remote foot pedal? YES

(b) DC straight machine? YES

(3) Joint Fit-up, and Internal Alignment.

(a) Internal alignment acceptable? YES

(b) Joint Clearance acceptable? YES

(c) End Preparation acceptable? YES

(4) Filler Rod

(a) AWS A5.9 stainless steel filler rod? YES

(b) Filler rod: Class 308L Diameter .045" + 1/16"

(5) Purge Gas.

(a) type of purge gas : ARGON

(b) time length of purge: AS NEEDED purge flow rate: 10 SCFH

(b) (if done) O2 reading: .08 O2 Monitor manf/model : CHECK - WELD

(6) Inspection After Root Pass

(a) No visible cracks. ✓

(b) No suck holes, which are small holes in middle of weld. ✓

(c) No porosity or obvious imperfections. ✓

(d) Filler material fused along edges of weld. ✓

(8) Repeat inspection after every pass: ✓

(9) Final Inspection: GOOD

**CMS CO<sub>2</sub> Test Stand  
In-Process Weld Inspection Form**

(as per In-Process Weld Inspection Guidelines, NML Cryogenic System, 9/29/06)

Date: 2/9/11

Project: CMS CO<sub>2</sub> Test Stand

Pipe Section: A3

Weld Number: A3-13 to A3-14

Weld Location:

Welder: Mike Cooper

Inspector: Abraham Diaz

Before Welding:

Type of weld: (butt)  (other) \_\_\_\_\_

(1) Pipe #1 Size, Schedule and Material: Stainless 1"

(2) Pipe #2 Size, Schedule and Material: Stainless 1"

(1) Joint Preparation and Cleanliness

Joint Preparation and Cleanliness acceptable? Yes

(2) Welding Machine

(a) Remote foot pedal?

(b) DC straight machine? \_\_\_\_\_

(3) Joint Fit-up, and Internal Alignment

(a) Internal alignment acceptable? yes

(b) Joint clearance acceptable? yes

(c) End preparation acceptable? yes

(4) Filler Rod

(a) AWS A5.9 stainless steel filler rod?

(b) Filler rod: Class 308L Diameter 1/16"

(5) Purge Gas

(a) type of purge gas: Argon

(b) time length of purge: 2min purge flow rate: 10PSI

(6) Inspection After Root Pass

(a) No visible cracks. NO

(b) No suck holes, which are small holes in middle of weld. NO

(c) No porosity or obvious imperfections: NO

(d) Filler material fused along edges of weld.

(7) Repeat inspection after every pass: yes

(8) Final Inspection: [Signature]

**CMS CO<sub>2</sub> Test Stand  
In-Process Weld Inspection Form**

(as per In-Process Weld Inspection Guidelines, NML Cryogenic System, 9/29/06)

Date: 2/22/11

Project: CMS CO<sub>2</sub> Test Stand

Pipe Section: A3

Weld Number: #7 - #10 #8 to 9  
#9 to #10  
#10 to #11

Weld Location: LAB F / Lab C

Welder: Mike Cooper

Inspector: Shah Jia

Before Welding:

- Type of weld: (butt) ✓ (other) \_\_\_\_\_  
(1) Pipe #1 Size, Schedule and Material: 1" Schedule 10  
(2) Pipe #2 Size, Schedule and Material: 1" Schedule 10 Elbow

(1) Joint Preparation and Cleanliness

Joint Preparation and Cleanliness acceptable? yes

(2) Welding Machine

- (a) Remote foot pedal? Yes  
(b) DC straight machine? Yes

(3) Joint Fit-up, and Internal Alignment

- (a) Internal alignment acceptable? yes  
(b) Joint clearance acceptable? yes  
(c) End preparation acceptable? yes

(4) Filler Rod

- (a) AWS A5.9 stainless steel filler rod? yes  
(b) Filler rod: Class 308 L Diameter 1/16"

(5) Purge Gas

- (a) type of purge gas: Argon  
(b) time length of purge: 2 min purge flow rate: 20 psig

(6) Inspection After Root Pass

- (a) No visible cracks. NO  
(b) No suck holes, which are small holes in middle of weld. NO  
(c) No porosity or obvious imperfections: NO  
(d) Filler material fused along edges of weld. ✓

(7) Repeat inspection after every pass: yes

(8) Final Inspection: Shah Jia

# CMS CO<sub>2</sub> Test Stand In-Process Weld Inspection Form

(as per In-Process Weld Inspection Guidelines, NML Cryogenic System, 9/29/06)

Date: 2/22/11

Project: CMS CO<sub>2</sub> Test Stand

Pipe Section: A-6

Weld Number: \_\_\_\_\_

*Items*  
#5 to #6  
#6 to #7

Weld Location: LAB F/LABC

Welder: Mike Cooper

Inspector: Abraham Diaz

### Before Welding:

Type of weld: (butt)  (other) \_\_\_\_\_

(1) Pipe #1 Size, Schedule and Material: 1" schedule 10

(2) Pipe #2 Size, Schedule and Material: 1" Schedule 10 Elbow

#### (1) Joint Preparation and Cleanliness

Joint Preparation and Cleanliness acceptable? yes

#### (2) Welding Machine

(a) Remote foot pedal? yes

(b) DC straight machine? no

#### (3) Joint Fit-up, and Internal Alignment

(a) Internal alignment acceptable? yes

(b) Joint clearance acceptable? yes

(c) End preparation acceptable? yes

#### (4) Filler Rod

(a) AWS A5.9 stainless steel filler rod? yes

(b) Filler rod: Class 308L Diameter 1/16"

#### (5) Purge Gas

(a) type of purge gas: Argon

(b) time length of purge: 2min purge flow rate: 20 psig

#### (6) Inspection After Root Pass

(a) No visible cracks. NO

(b) No suck holes, which are small holes in middle of weld. NO

(c) No porosity or obvious imperfections: NO

(d) Filler material fused along edges of weld. ✓

(7) Repeat inspection after every pass: yes

(8) Final Inspection: Abraham Diaz

**CMS CO<sub>2</sub> Test Stand  
In-Process Weld Inspection Form**

(as per In-Process Weld Inspection Guidelines, NML Cryogenic System, 9/29/06)

Date: 12-7-2011

Project: CMS CO<sub>2</sub> Test Stand

Pipe Section: Assm - 5

Weld Number: #10 to #9

Weld Location: PC 4

Welder: Ryan (W-2)

Inspector: Erik Vairin

Before Welding:

Type of weld: (butt) X (other) \_\_\_\_\_

(1) Pipe #1 Size, Schedule and Material: schedule 10 1.5" 90° elbow

(2) Pipe #2 Size, Schedule and Material: schedule 10 1.5" to 1" reducer

(1) Joint Preparation and Cleanliness

Joint Preparation and Cleanliness acceptable? Yes

(2) Welding Machine

(a) Remote foot pedal? Yes

(b) DC straight machine? Yes

(3) Joint Fit-up, and Internal Alignment

(a) Internal alignment acceptable? Yes

(b) Joint clearance acceptable? Yes

(c) End preparation acceptable? Yes

(4) Filler Rod

(a) AWS A5.9 stainless steel filler rod? Yes

(b) Filler rod: Class 308L Diameter 1/16"

(5) Purge Gas

(a) type of purge gas: Ar

(b) time length of purge: 2 min purge flow rate: 10 scfh

(6) Inspection After Root Pass

(a) No visible cracks. No

(b) No suck holes, which are small holes in middle of weld. No

(c) No porosity or obvious imperfections: No

(d) Filler material fused along edges of weld. ✓

(7) Repeat inspection after every pass: Yes

(8) Final Inspection: [Signature]

**CMS CO<sub>2</sub> Test Stand  
In-Process Weld Inspection Form**

(as per In-Process Weld Inspection Guidelines, NML Cryogenic System, 9/29/06)

Date: 12-7-2011

Project: CMS CO<sub>2</sub> Test Stand

Pipe Section: Assem-4

Weld Number: #10 to #11

Weld Location: PC4

Welder: Ryan (W-2)

Inspector: Erik Vöirin

Before Welding:

Type of weld: (butt) X (other) \_\_\_\_\_

(1) Pipe #1 Size, Schedule and Material: 1/2" schedule 10 45° elbow

(2) Pipe #2 Size, Schedule and Material: 1/2" schedule 10 90° elbow

(1) Joint Preparation and Cleanliness

Joint Preparation and Cleanliness acceptable? Yes

(2) Welding Machine

(a) Remote foot pedal? Yes

(b) DC straight machine? Yes

(3) Joint Fit-up, and Internal Alignment

(a) Internal alignment acceptable? Yes

(b) Joint clearance acceptable? Yes

(c) End preparation acceptable? Yes

(4) Filler Rod

(a) AWS A5.9 stainless steel filler rod? Yes

(b) Filler rod: Class 308L Diameter 1/16"

(5) Purge Gas

(a) type of purge gas: Ar

(b) time length of purge: 2 minutes purge flow rate: 10 scfh

(6) Inspection After Root Pass

(a) No visible cracks. NO

(b) No suck holes, which are small holes in middle of weld. NO

(c) No porosity or obvious imperfections: NO

(d) Filler material fused along edges of weld. ✓

(7) Repeat inspection after every pass: Yes

(8) Final Inspection: [Signature]

## **8. Component Identification**

**Process and Instrument diagram:**

The process and instrument diagram is on drawing 9212.750-ME-466879, and also included on the following page. This diagram is followed by the valve and instrument list.

**Piping components:**

Drawings and lists of each piping run including all fittings and their pressure ratings are included following the valve and instrument list. Purchase requisition forms are included as well.

- The system contains 4 flex hoses rated to a minimum of 1200 psi. The purpose of these hoses is to allow the pump to vibrate more freely, and attached to unknown detector attachments. The braided hoses are two at 1.5” x 60” (to and from detector), one at 1.5 x 12” (pump inlet), and one at 1.5 x 16” (pump outlet). The hoses were purchased from Janco Process Control.
- The Valves used in the system are stainless steel valves rated to 1480 psi. The valves are Sharpe series 99 valves.
- Strainers are class 600 strainers manufactured by Keckley, they are rated for 1480 psi
- The check valves are cryogenic swing type check valves class 600 rated
- The manual control valve is a Triad valve rated to 2000 psi
- Flanges are class 600 rated
- Hart Unions are rated to 3000 psi

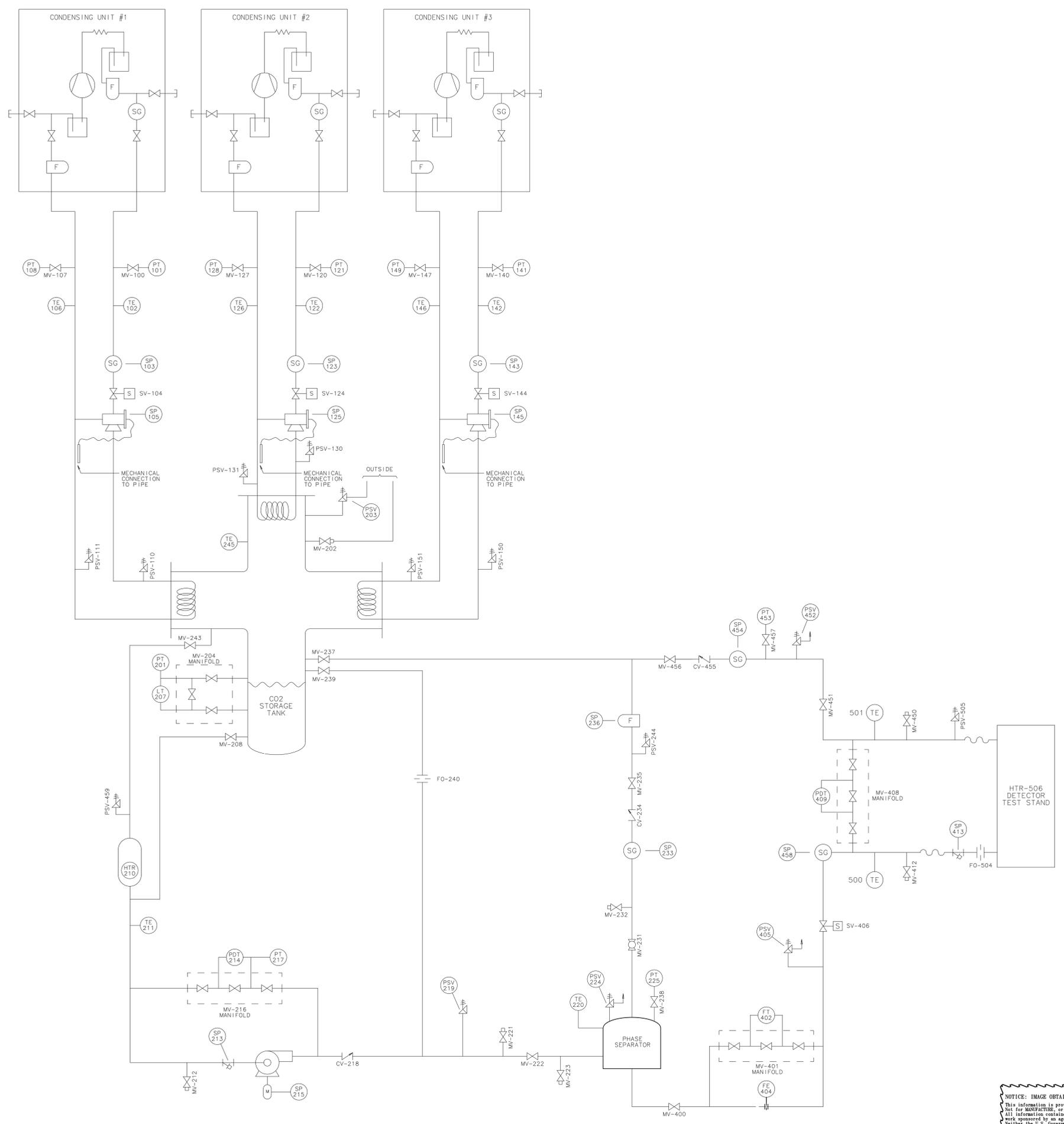
*Descriptions / specifications follow the piping drawings.*

## Appendix B

### Equipment Documentation

- Flex Hoses (Req Attached)
  - Pressure Flex hoses have a MAWP of 1200 psi, and a burst pressure of 4842 psi.
    - <http://www.hosemaster.com/products/corrugatedmetalhoses/hose.php?id=7>
  - Hydra Flex hoses have a MAWP of at least 1500 psi, and a burst pressure of at least 6000 psi.
    - <http://www.hosemaster.com/products/corrugatedmetalhoses/hose.php?id=11>
- Sharpe Valves (Req Attached)
  - The 99 series Sharpe Valves have a pressure rating of at least 1480 psi
    - [http://www.sharpevalves.com/pdfs/series\\_99.pdf](http://www.sharpevalves.com/pdfs/series_99.pdf)
- ½” Control Valve (Req Attached)
  - This Valve has a pressure rating of 2000 psi.
    - <http://www.triadprocess.com/pdf/Triad66FD.pdf>
- Strainers (Req Attached)
  - The Keckley Brand Strainers have a class rating of 600 (1480 psi)
    - <http://www.keckley.com/pdf/downloads/Style%20SSB-7.pdf>
- Check Valves (Req Attached)
  - The Velan Brand Check Valves are Class 600 rated (1480 psi)
    - [http://www.velan.com/velan/en/products/16/31/?product\\_id=64](http://www.velan.com/velan/en/products/16/31/?product_id=64)
- Flanges (Req Attached)
  - Flanges are all ASME Class 600 rated (1480 psi)
    - Purchased from Janco Process Control
    - Orifice Flange purchased from Specialty Flange and Fitting
- Sight Glasses (Req Attached)
  - MetaGlass sight glasses are rated to 1450 psi per Distributor. This value is stated on purchase requisition as well.
    - Purchased from Chemray
- Instruments (Req Attached)
  - Fuji Differential Pressure Transmitters are rated for at least 1450 psi
    - [http://www.instrumart.com/assets/108/FKCnew\\_datasheet.pdf](http://www.instrumart.com/assets/108/FKCnew_datasheet.pdf)
  - Setra SC207 Pressure Transmitters have a range of 0-3000 psig, which shows their MAWP is at least 3000 psi.

- Unions (Req Attached)
  - Unions are Rated at 3000 psi and were purchased from Hart Industries
    - [http://www.hartindustries.com/images/HART%203333%20Union%20Technical%20Data%20Sheet\\_1.pdf](http://www.hartindustries.com/images/HART%203333%20Union%20Technical%20Data%20Sheet_1.pdf)
- Pipe (Req Attached)
  - Piping is all 304/304L Schedule 10 Stainless and which complies with ASTM Standards. Piping was purchased from RJ Keck.
    - Material mill reports are available.
- Studs and Nuts (Req Attached)
  - Grade A320 Grade B7 studs are used throughout the system. They comply with the temperature range and pressures involved. They were purchased from Fastenal.
    - Heavey Hex Nuts used with all studs.
- Gaskets (Req Attached)
  - High Quality Dual solid metal ring gaskets are used throughout the system. They were Purchased from Flexitallic



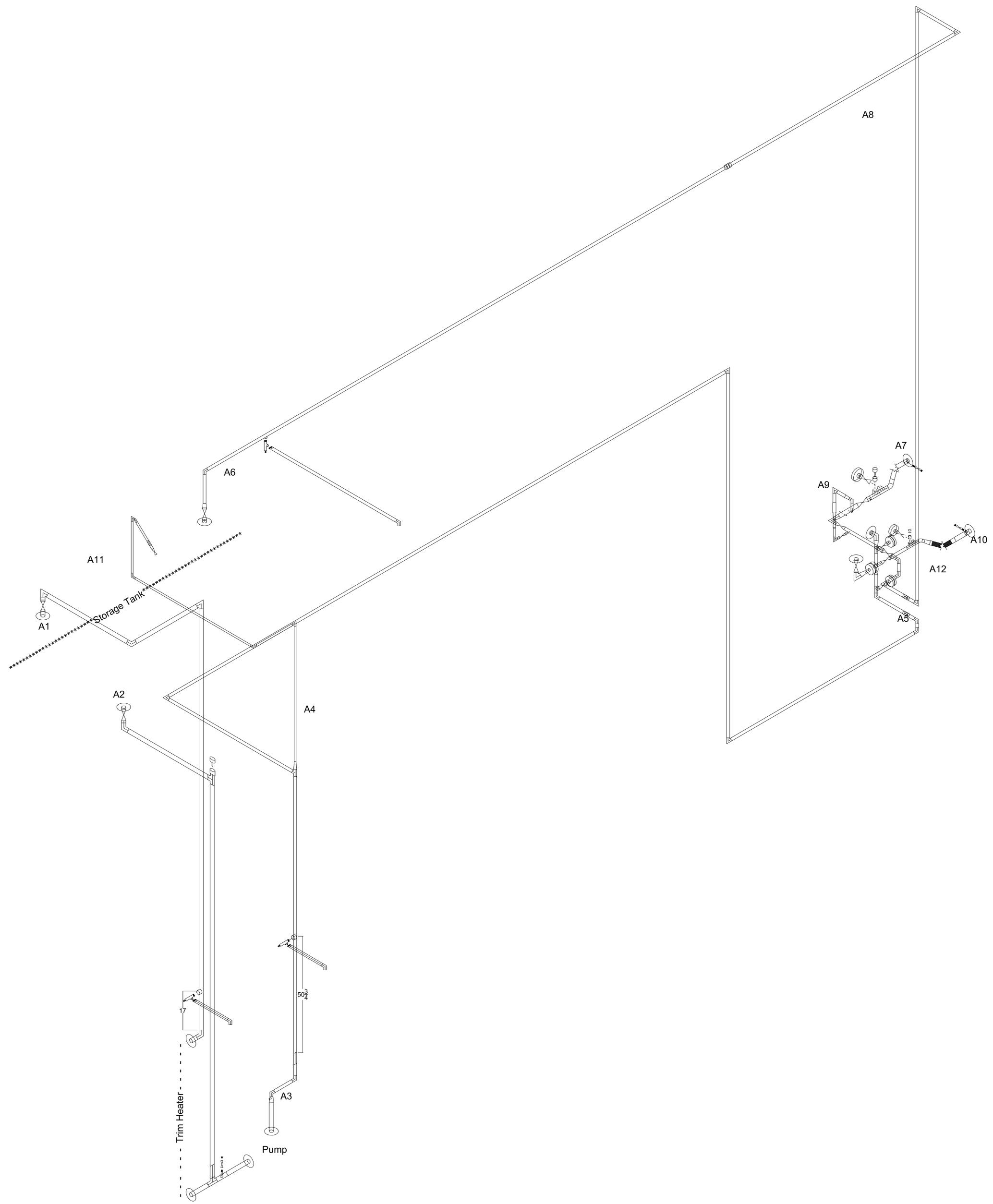
UNLESS OTHERWISE SPECIFIED	ORIGINATOR	M. ADAMOWSKI	04-FEB-2010
±	DRAWN	J. CATALANELLO	09-FEB-2010
±	CHECKED	E. VOIRIN	02-AUG-2010
±	APPROVED	E. VOIRIN	02-AUG-2010
1. BREAK ALL SHARP EDGES	USED ON		
2. DO NOT SCALE DRAWING.			
3. DIMENSIONS BASED UPON			
4. MAX. ALL MACH. SURFACES	MATERIAL		
5. DRAWING UNITS:			

FERMI NATIONAL ACCELERATOR LABORATORY  
UNITED STATES DEPARTMENT OF ENERGY

CMS/DETECTORS  
PIXEL  
CMS CO2 COOLING P&ID

SCALE	DRAWING NUMBER	SHEET	REV
NONE	9212.750-ME-466879	1 OF 1	

NOTICE: IMAGE OBTAINED FROM FERMILAB WEB SITE  
This information is provided for REFERENCE use only.  
Not for MANUFACTURE, or DESIGN INFORMATION.  
All information contained in this document represents  
work sponsored by an agency of the U.S. Government.  
Neither the U.S. Government nor any agency thereof,  
nor Universities Research Association, Inc., nor any of  
their employees or officers, makes any warranty, express  
or implied, or assumes any legal liability or  
responsibility for the accuracy, completeness, or  
usefulness of any information, apparatus, product or  
process disclosed, or represents that its use would not  
infringe privately owned rights.



## Assembly 1

Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1.5	1	600# flange	0.875"			1480
1.5	2	Pipe	1.88	SW-flange	SW- valve	2000
1.5	3	Valve	5			1480
1.5	4	Pipe	1	SW- valve	Butt-elbow	2000
1.5	5	elbow	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	6	Pipe	40.44	Butt-elbow	Butt-elbow	2000
1.5	7	elbow	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	8	Pipe	30.85	Butt-elbow	Butt-elbow	2000
1.5	9	elbow	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	10	Pipe	183.35	Butt-elbow	Butt-elbow	2000
1	10.1	Saddle fitting				3000
1	10.2	relief valve				10000 psi burst
1	10.3	fitting	1			3000
1	10.4	Pipe	16	Butt Fitting	Butt elbow	3000
1	10.5	elbow	1.5	Butt-Pipe		3000
1.5	11	elbow	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	12	Pipe	2.88	Butt-elbow	SW-flange	2000
1.5	13	600# flange	0.875"			1480

## Assembly 2

Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1.5	1	600# flange	0.875"			2000
1.5	2	Pipe	8.52	SW-flange	Butt-Tee	2000
1.5	3	Tee	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	4	Pipe	5.19	Butt-Tee	Butt-Flex	2000
0.5	4.1	Pipe saddle 1/2"		FW to piece 4	.5" Threaded	3000
0.5	4.2	threaded nipple		4.1	4.3	3000
0.5	4.3	1/2" valve		4.2	4.4	1480
0.5	4.4	1/2" pipe plug		4.3		3000
0.25	4.5	Pipe saddle 1/4"		FW to piece 4	for PDT	3000
1.5	5	Flex Hose	12	Butt-Pipe		1500
1.5	6	Strainer	5.5 inches			1480
1.5	7	Pipe	166.125	Butt-Tee	Butt-Pipe	2000
1.5	8	Tee	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	8.1	SW coupling		SW Tee	Thermowell	3000
1.5	8.2	thermowell	TW30-1-1/2-L4-SS316			20000
1.5	9	Pipe	40.44	Butt-elbow	Butt-elbow	2000
1.5	10	elbow	r=2.25	Butt-Pipe	Butt-Pipe	2000
1.5	11	Pipe	1	Butt-elbow	SW- valve	2000
1.5	12	Valve	5			1480
1.5	13	Pipe	0.9	SW- valve	SW-flange	2000
1.5	14	600# flange	0.875"			1480

### Assembly 3 - out of pump

Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1.5 to 1	1	Flex Hose	16 - 5/16	Butt-Elbow		1500
	1.1	Pipe saddle 1/4"		Piece 1 reducer	tp PDT	3000
1	2	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	3	Pipe	9.06	Butt-elbow	Butt-elbow	3000
1	4	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	5	Pipe	5	Butt-elbow	SW strainer	3000
1	6	check valve	5			1480
1	7	Pipe	120.29	SW strainer	Butt-Tee	3000
	7.1	Pipe saddle 1"	~57" from CV	Piece 7	Relief valve	3000
1	7.2	relief valve				10000 psi burst
1	7.3	fitting	1			3000
1	7.4	Pipe	16	Butt Fitting	Butt elbow	3000
1	7.5	elbow	1.5	Butt-Pipe	Outside	3000
1	8	Tee	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	9	Pipe	62.54	Butt-Tee	Butt-elbow	3000
1	10	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	11	Pipe	282.16 (two pieces)	Butt-elbow	Butt-Pipe	3000
1	11.1	Pipe		Butt-Pipe	Butt-elbow	3000
1	12	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	13	Pipe	158.55	Butt-elbow	Butt-elbow	3000
1	14	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	15	Pipe	92.88	Butt-elbow	Butt-elbow	3000
1	16	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	17	Pipe	1.68	Butt-elbow	Butt-elbow	3000
1	18	elbow	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	19	Pipe	3	Butt-elbow	SW Union	3000
1	20 TE	Union TE	2.25/2	Piece 19	(to Assm 5)	3000

### Assembly 4 - out of Pump Pipe back to vessel dead head line

Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1 to .75	1	reducer	2	Butt T (Assm3)	Butt-reducer	3000
.75 to .5	2	reducer	1.5	Butt-reducer	Butt-Pipe	3000
0.5	3	Pipe	58.75	Butt-reducer	Butt-elbow	3000
0.5	4	elbow	r = 1.5	Butt-Pipe	Butt-Pipe	3000
0.5	5	Pipe	18.09	Butt-elbow	Butt-elbow	3000
0.5	6	elbow	r = 1.5	Butt-Pipe	Butt-Pipe	3000
0.5	7	Pipe	58.57	Butt-elbow	Butt-elbow	3000
0.5	8	elbow	r = 1.5	Butt-Pipe	Butt-Pipe	3000
0.5	9	Pipe	22.5	Butt-elbow	Butt-elbow	3000
0.5	10	elbow	r = 1.5	Butt-Pipe	Butt-elbow	3000
0.5	11	45 degree elbow	r = 1.5	Butt-elbow	Butt-Pipe	3000
0.5	12	Pipe	10	Butt-elbow	SW Union	3000
0.5	13	hart union	2			3000
0.5	14	Thrd Pipe (cut in 1/2) 2.5		SW union	Valve	3000
0.5	15	1/2" valve	2.78	Thrd Pipe	reduc nipple	1480
.5 to .75	16	reducing nipple	0.25	valve	vessel port 1	6600

## Assembly 5 - into cleanroom

Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1	1	Union NUT END	2.25/2	(to Assm 3)	piece 2	3000
1	2	Pipe	12.55			3000
1	3	elbow		Butt-Pipe	Butt-Tee	3000
1	4	Tee		Butt-Elbow	Butt-Pipe	3000
1	4.1	1" Valve	4.22			1480
1	4.2	Pipe	1			3000
1	4.3	Flange				1480
1	4.4	Blind Flange				1480
1	5	Pipe	5.015	Butt-Tee	SW-Valve	3000
1	6	Valve	4.22			1480
1	7	Pipe	5.015	SW-Valve	Butt-Tee	3000
1	8	Tee	r=1.5	Butt-Pipe	Butt-Pipe	3000
1	8.1	1" Valve	4.22			1480
1	8.2	Pipe	1			3000
1	8.3	Flange				1480
1	8.4	Blind Flange				1480
1 to 1.5	9	reducer to 1.5	L=2.5	Butt-Tee	Butt-elbow	2000
1.5	10	elbow	r=2.25	Butt-Reducer	Butt-Pipe	2000
1.5	11	Pipe	0.4	Butt-elbow	SW-flange	2000
1.5	12	600# flange	0.875"+.25"			1480

## Assembly 6 - return line 1

Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1.5	1	flange	1.125	Vessel		1480
1.5	2	Pipe	1	SW flange	SW valve	2000
5	3	valve	5			1480
1.5 to 1	4	reducer	2.5	SW Valve	Butt-Pipe	2000
1	5	Pipe	12.625	Butt-Reducer	Butt-elbow	3000
1	6	elbow	1.5			3000
1	7	Pipe	263	Butt-elbow	SW Union	3000
1 to 3/4	7.1	saddle ftng (3/4)			relief Valve	3000
.75	7.2	relief valve				2000
1	7.3	fitting	1			3000
1	7.4	Pipe	63	Butt Fitting	Butt elbow	3000
1	7.5	elbow	1.5	Butt-Pipe	Outside	3000
1	8	SW union Thrd End			(Assm 8)	3000

## Assembly 7 - return line in cleanroom

Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1	1	Union NE	2.25/2	Piece 19	(to Assm 8)	3000
1	2	Pipe	8.82	SW union	Butt - elbow	3000
1	3	elbow	r = 1.5	Butt-Pipe	Butt-Pipe	3000
1	4	Pipe	4.81	Butt-elbow	Butt-elbow	3000
1	5	elbow	r = 1.5	Butt-Pipe	Butt-Pipe	3000
1	6	Pipe	3.6	Butt-elbow	Butt-elbow	3000
1	7	elbow	r = 1.5	Butt-Pipe	Butt-Reducer	3000
1 to 1.5	8	Reducer	2.5 - .5	Butt-elbow	SW-CV	2000
1.5	9	Check-Valve	5	reducer	reducer	1480
1.5 to 1	10	Reducer	2.5 - .5	SW-CV	Butt-Pipe	2000
1	11	Pipe	17.05	Butt-Reducer	SW-Valve	3000
.5"	11.1	saddle fitting		pipe 11	(to assm 9)	3000
1	12	1" Valve	4.22	pipe 11	pipe13	3000
1	13	Pipe	1	SW-Valve	Butt-elbow	1480
1	14	Elbow	r = 1.5 "	Butt-Pipe	Butt-Pipe	3000
1 to 1.5	15	reducer	2.5	Butt-elbow	Butt-Pipe	2000
1.5	16	Pipe	9.375	Butt - reducer	SW-Valve	2000
1.5"	16.1	saddle fitting	2" from reducer			3000
1.5"	16.11	sight glass				1450
1.5"	16.2	saddle fitting	2" from reducer			3000
1.5"	16.21	sight glass				1450
.5"	16.3	saddle fitting	4.75" from reducer			3000
0.5	16.31	nipple				3000
0.5	16.32	Valve				1480
.5 to .25	16.33	bushing				3000
0.25	16.34	Pressure Trans				3000
.5"	16.4	saddle fitting	7.25" from reducer		relief valve	3000
0.5	16.41	relief valve				10000 psi burst
1.5	17	Valve	5	pipe 16	Pipe 18	1480
1.5	18	Pipe	1.5	SW-Valve	Butt Tee	2000
.25"	18.1	saddle fitting				3000
1.5	19	Tee		Butt pipe 18	Butt Tee 20	3000
1.5	19.1	Coupling		Tee 20	Thermowell	3000

1.5	19.11	Thermowell				20000
1.5	20	Tee		Butt Tee 19	Valve (up)	3000
1.5	20.1	Valve		Tee 19	Pipe 19.2	1480
1.5	20.11	Pipe	1	SW valve	SW flange	3000
1.5	20.12	flange		end of pipe 19.2		1480
1.5	20.13	blind flange				1480
1.5	21	45 degree elbow		Butt Tee 20		2000
1.5	22	Flex Pipe		Butt elbow	Butt Pipe	1200 (4842 Burst)
1.5	23	Pipe	2	Butt Flex	SW Flange	2000
0.375	24	saddle fitting				3000
0.375	24.1	Nipple				3000
0.375	24.11	Valve				1480
0.375	24.12	plug				3000
1.5	25	Flange				1480

### Assembly 8 - return line

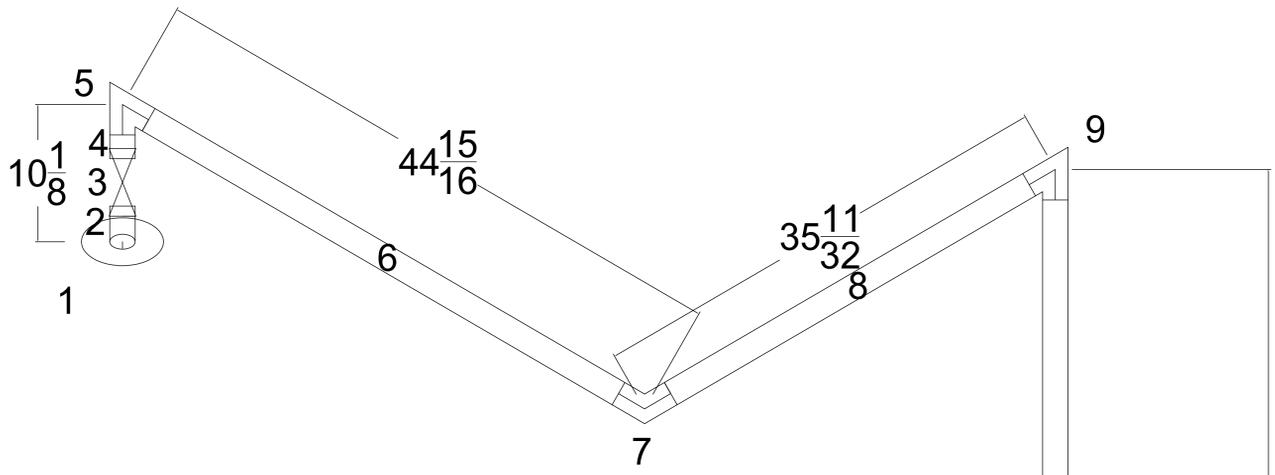
Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1	1	Union Nut End		(Assm 6)		3000
1	2	Pipe	113.87	Butt-pipe	Butt-elbow	3000
1	3	elbow		Butt-Pipe	Butt-Pipe	3000
1	4	Pipe	17.5	Butt-elbow	Butt-elbow	3000
1	5	elbow		Butt-Pipe	Butt-Pipe	3000
1	6	Pipe	256	Butt-elbow	Butt-elbow	3000
1	7	elbow		Butt-Pipe	Butt-Pipe	3000
1	8	Pipe	3	Butt-elbow	SW Union	3000
1	9	Union TE	2.25/2	Piece 19	(to Assm 7)	3000

## Assembly 9 - Phase Separator Top outlet (P.S.)

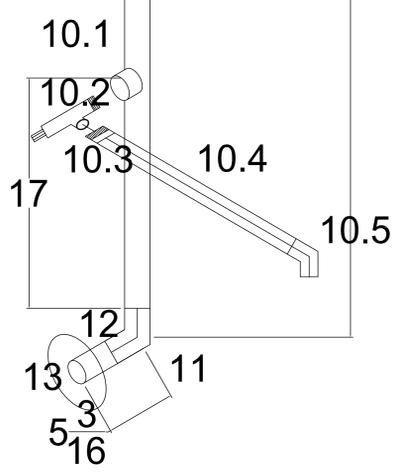
Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
0.75	1	pipe nipple cut	3	threaded to P.S.	butt elbow	2000
0.75	2	pipe elbow	r = 1.5	Butt Pipe	Butt Pipe	3000
.75 to 1	3	reducer	2"	Butt-elbow	Butt Pipe	3000
1	4	Flex Pipe	12	Butt-Reducer	Butt-elbow	1500
1	4.1	elbow	1.5	Butt-Flex	Butt Pipe	3000
1	4.2	Pipe	4	Butt-elbow	Butt-elbow	3000
1	4.3	elbow	1.5	Butt Pipe	Butt Pipe	3000
1	4.4	Pipe	12	Butt-elbow	Butt-elbow	3000
1	5	elbow	r = 1.5	Butt Pipe	Butt Pipe	3000
1	6	Pipe	4	Butt-elbow	SW strainer	3000
1	6.1	saddle fitting	2" from elbow			3000
1	6.11	sight glass				1450
1	6.2	saddle fitting				3000
1	6.21	sight glass				1450
1	7	Strainer	4.5			1480
1 to .75	8	reducer	2	SW-Strainer	Butt Reducer	3000
.75 to .5	9	reducer	1.5	Butt Reducer		3000
0.5	10	Check Valve	3.75			1480
0.5	11	Pipe	3 - 7/16	SW-CV	Butt elbow	3000
0.5	12	elbow				3000
0.5	13	Pipe	1	Butt-elbow	SW CV	3000
0.5	14	Control Valve				2000
0.5	15	Pipe	3	SW CV	SW-(Assm 7)	3000

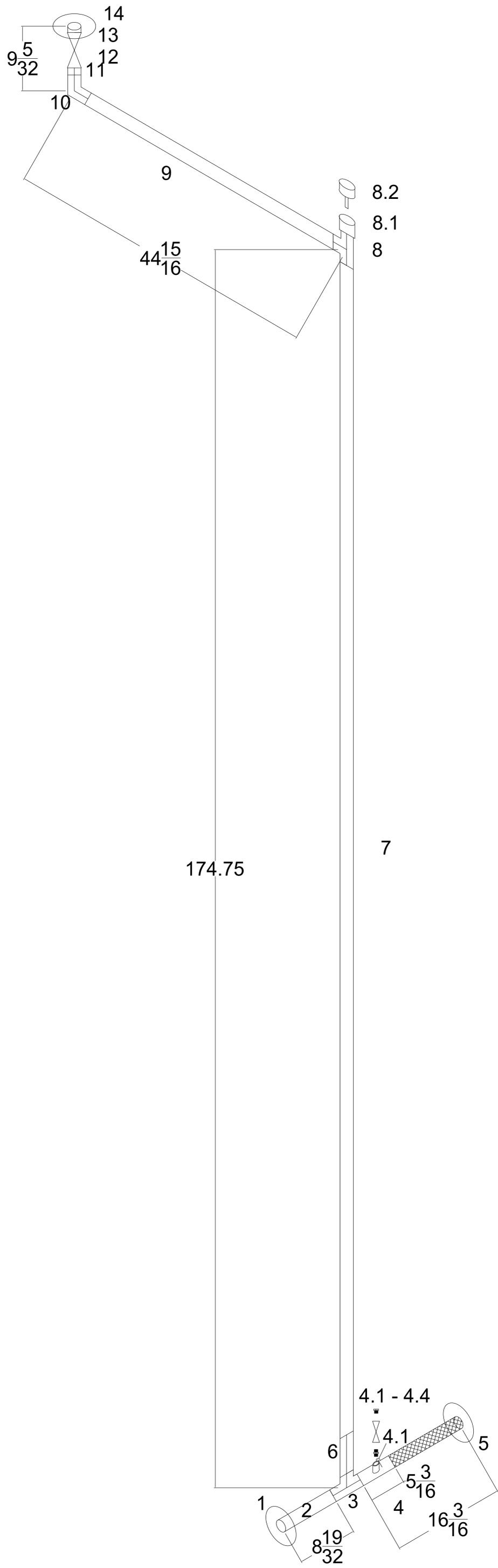
## Assembly 10 - Phase Separator Bottom outlet (P.S.)

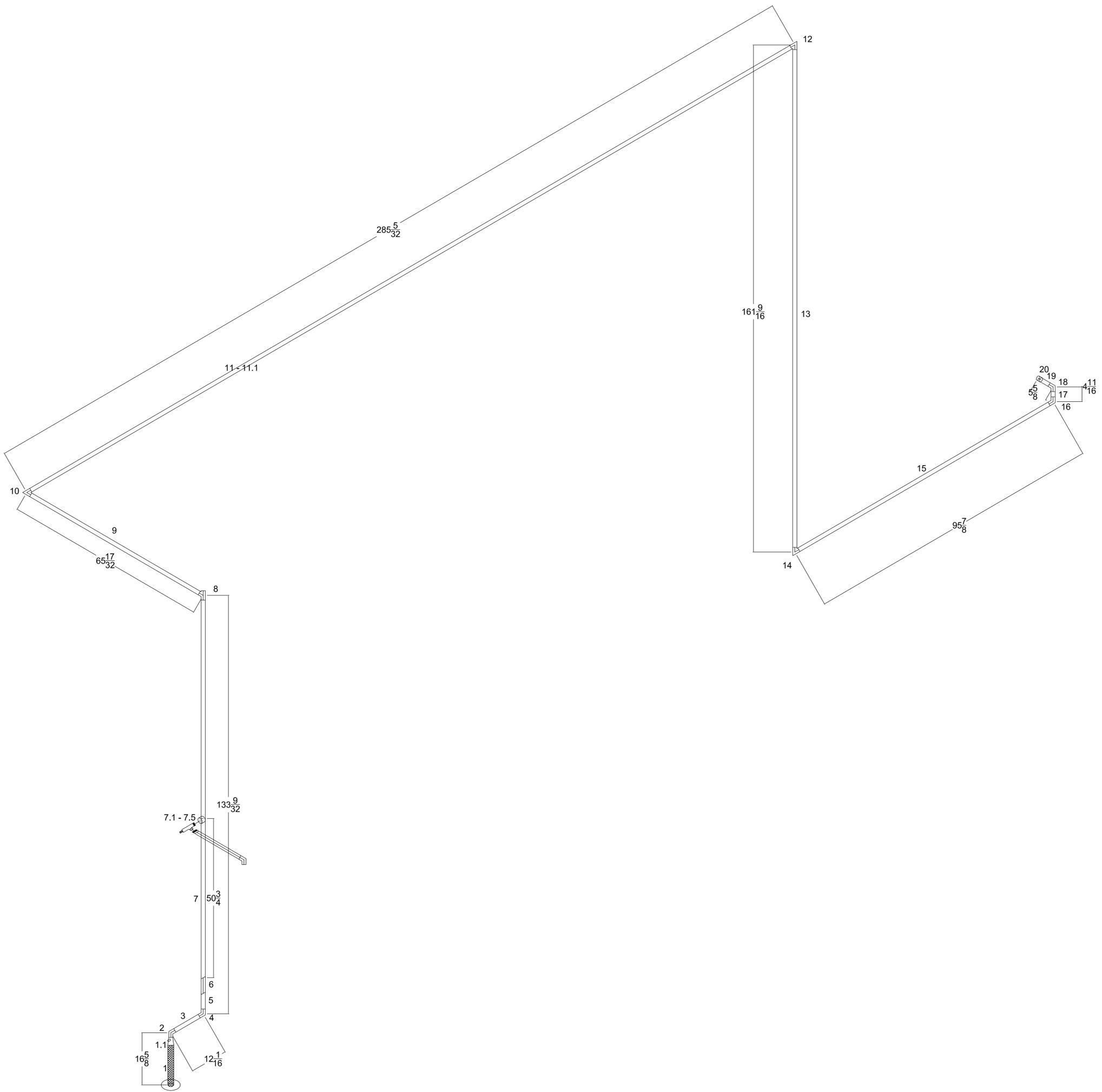
Pipe size	Piece#	Description	Length shown	end 1	end 2	MAWP (psi)
1.5	1	flange	1.125			1480
1.5	2	Pipe	0.65	SW flange	SW valve	2000
1.5	3	Valve	5			1480
1.5	4	Pipe	0.25	SW Valve	Butt Elbow	2000
1.5	5	Elbow	r = 2.25	Butt Pipe	Butt Reducer	2000
1.5 to 1	6	reducer	2.5	Butt-elbow	Butt Pipe	2000
1	7	Pipe	2	Butt-Reducer	SW-flange	3000
1	8	Orifice Flanges	2.5			1480
1	9	Pipe	3.75	SW Flange	SW Valve	3000
1"	9.1	saddle fitting	SW-F end	Pipe 9	relief valve	3000
1	9.11	relief valve				10000 psi burst
1	10	Valve	4.22			1480
1	11	Pipe	8.5	SW valve	Butt-Tee	3000
1	11.1	saddle fitting				3000
1	11.11	sight glass				1450
1	11.2	saddle fitting				3000
1	11.21	sight glass				1450
1	11.4	saddle fitting			relief valve	3000
1	11.41	relief valve				10000 psi burst
0.25	11.3	saddle fitting			DPT	3000
1	12	Tee		Butt-Pipe 11	Butt-Tee	3000
1	12.1	Coupling				3000
1	12.11	Thermowell				20000
1	13	Tee		Butt Tee 12	Valve	3000
1	13.1	Valve				1480
1	13.2	Pipe	1	SW-Valve	SW flange	3000
1	13.3	Flange				1480
1	13.4	Blind Flange				3000
1	14	45 degree elbow				3000
1.5	15	flex pipe				1200 (4842 Burst)
1.5	16	strainer				1480
1.5	17	Pipe	2	SW-strainer	SW flange	2000
0.375	18	Saddle Fitting				3000
0.375	18.1	Nipple				3000
0.375	18.2	Valve				1480
0.375	18.3	Plug				3000
1.5	19	flange				1480

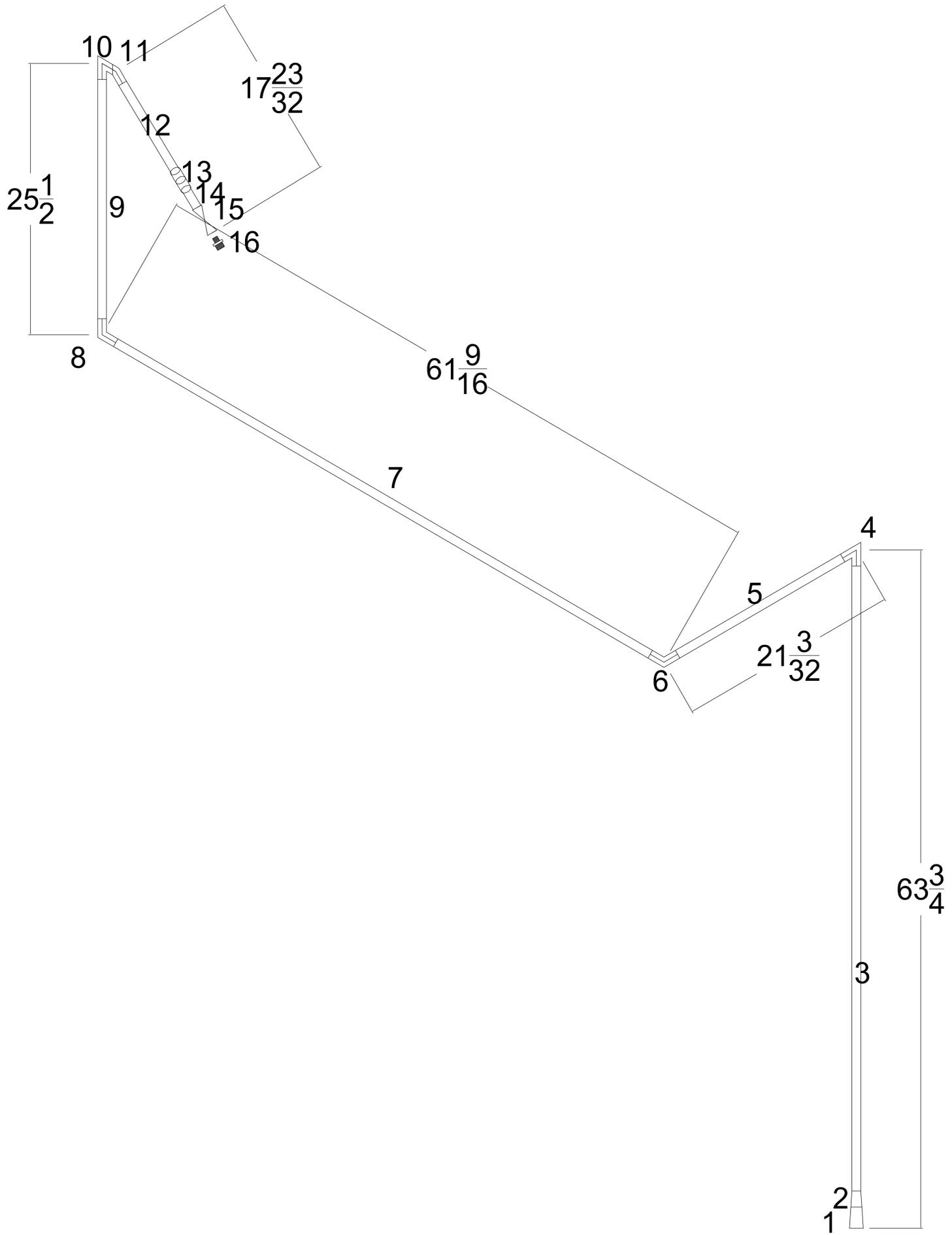


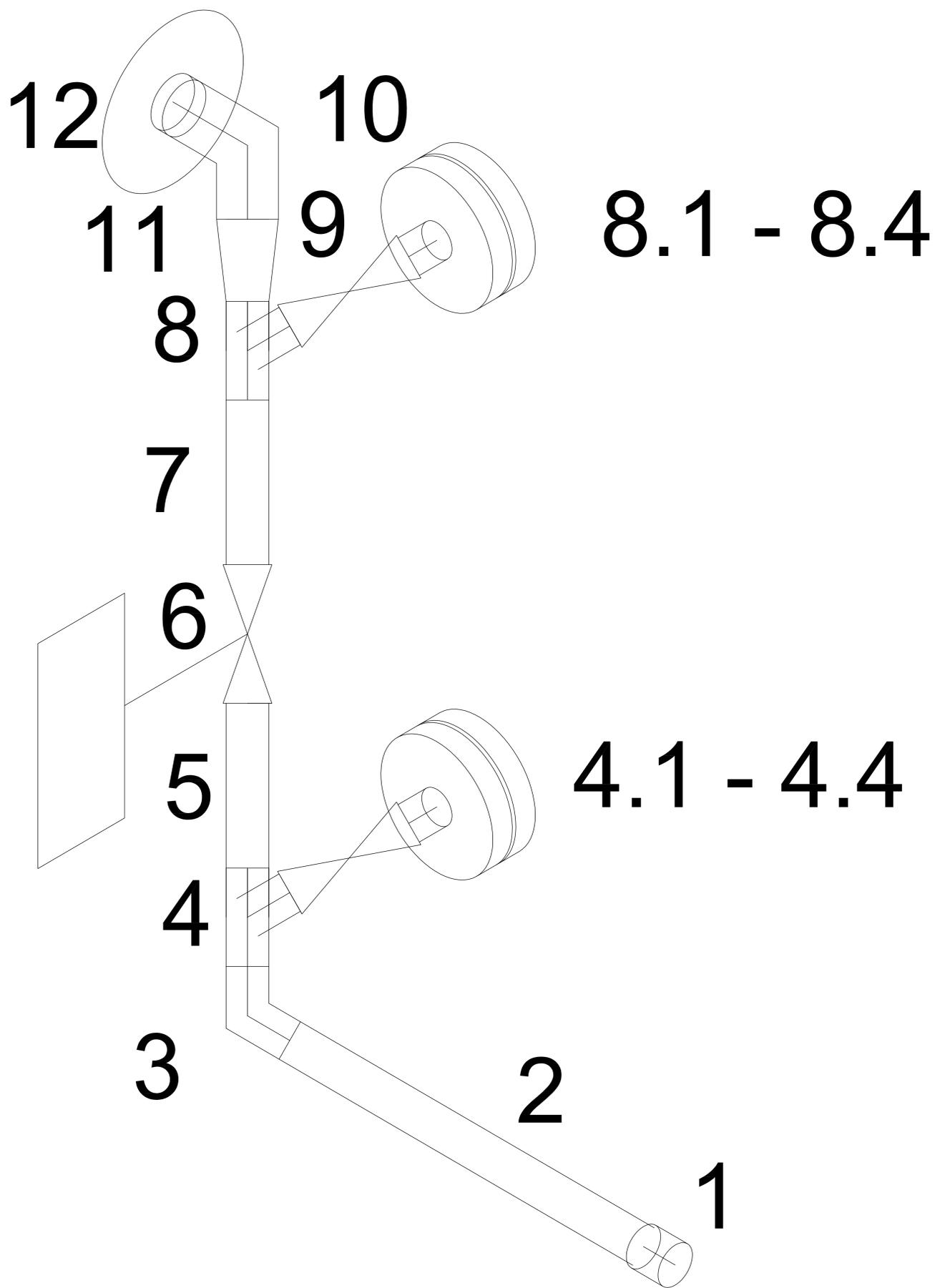
11187 - 7/32

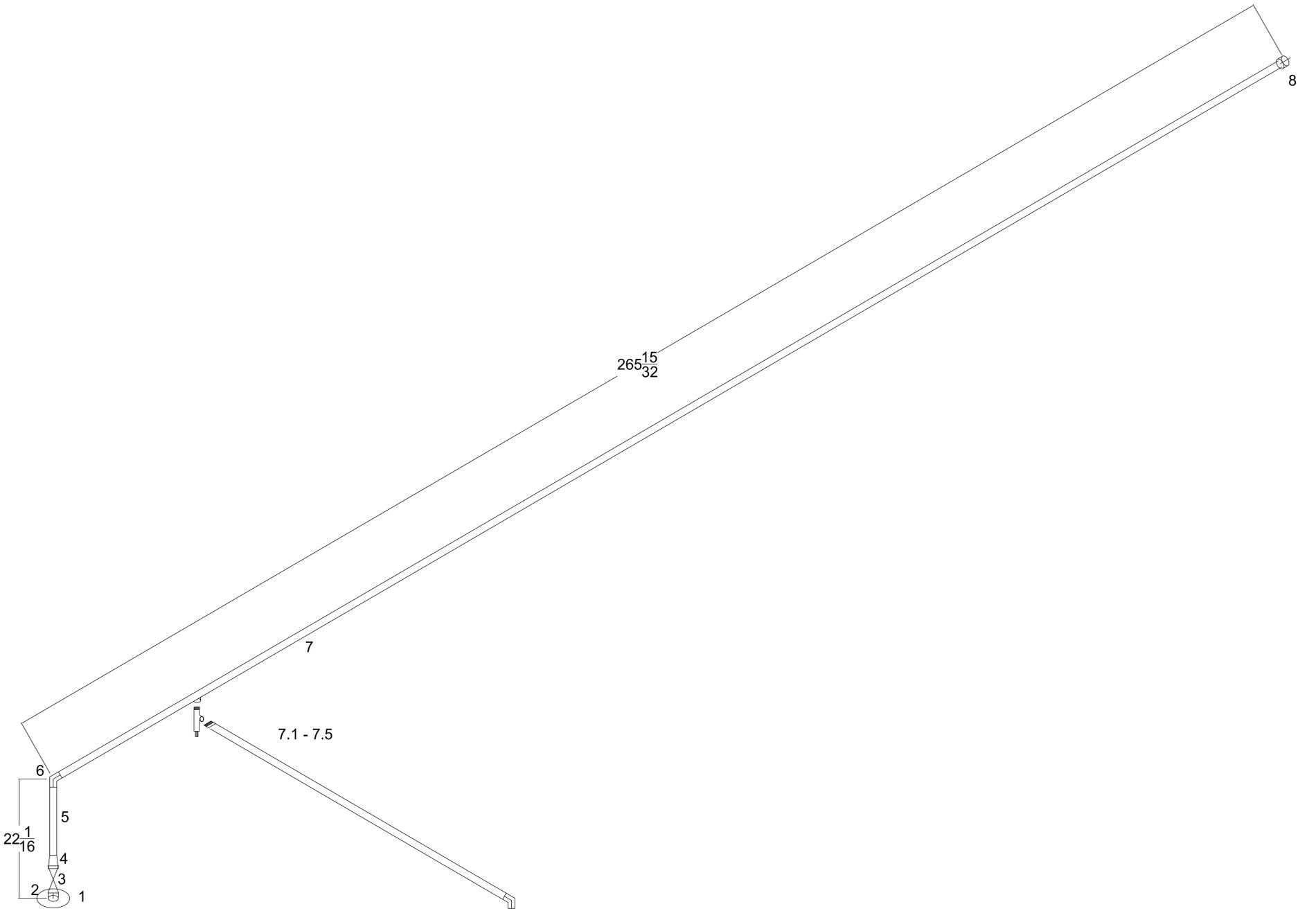


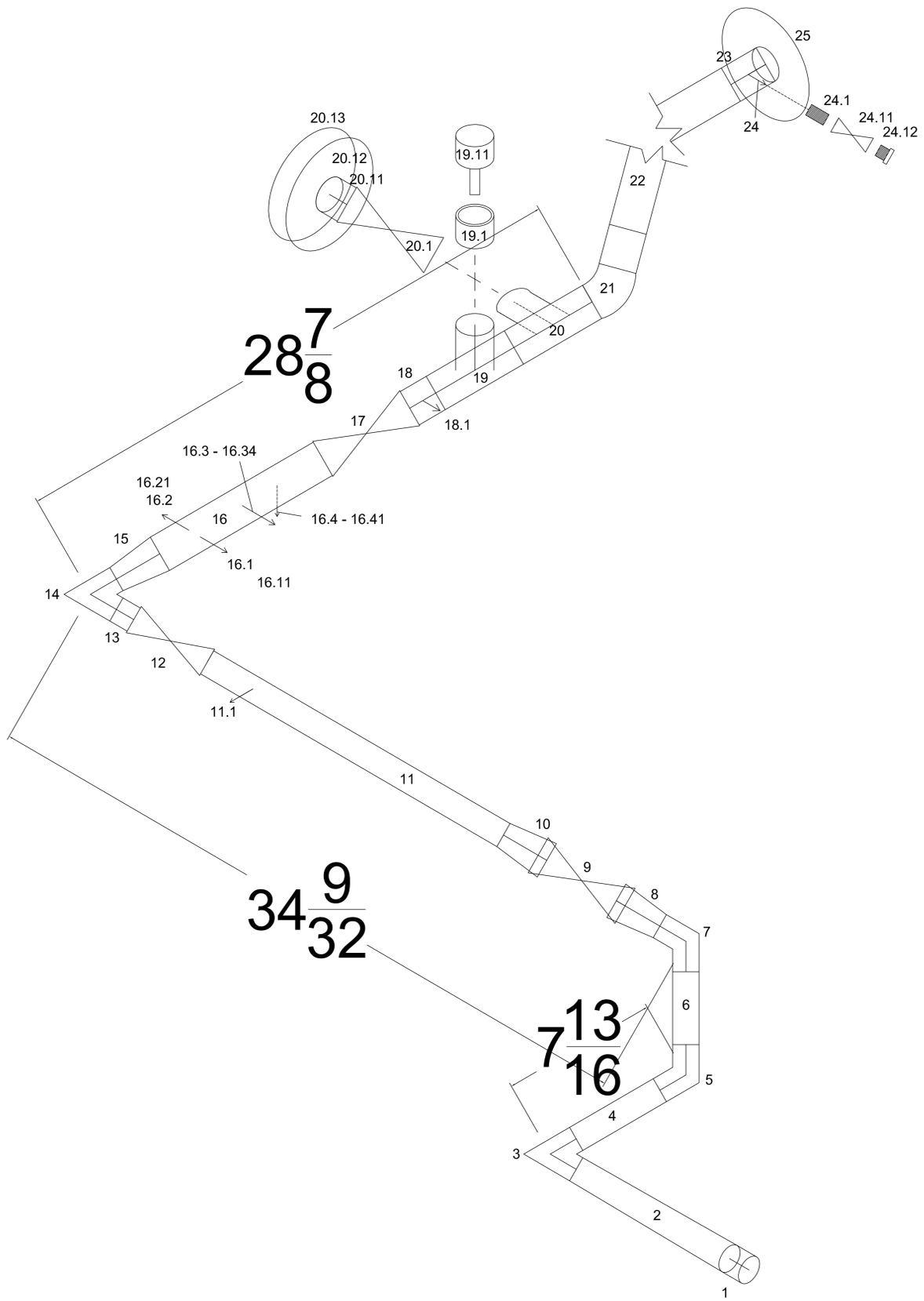


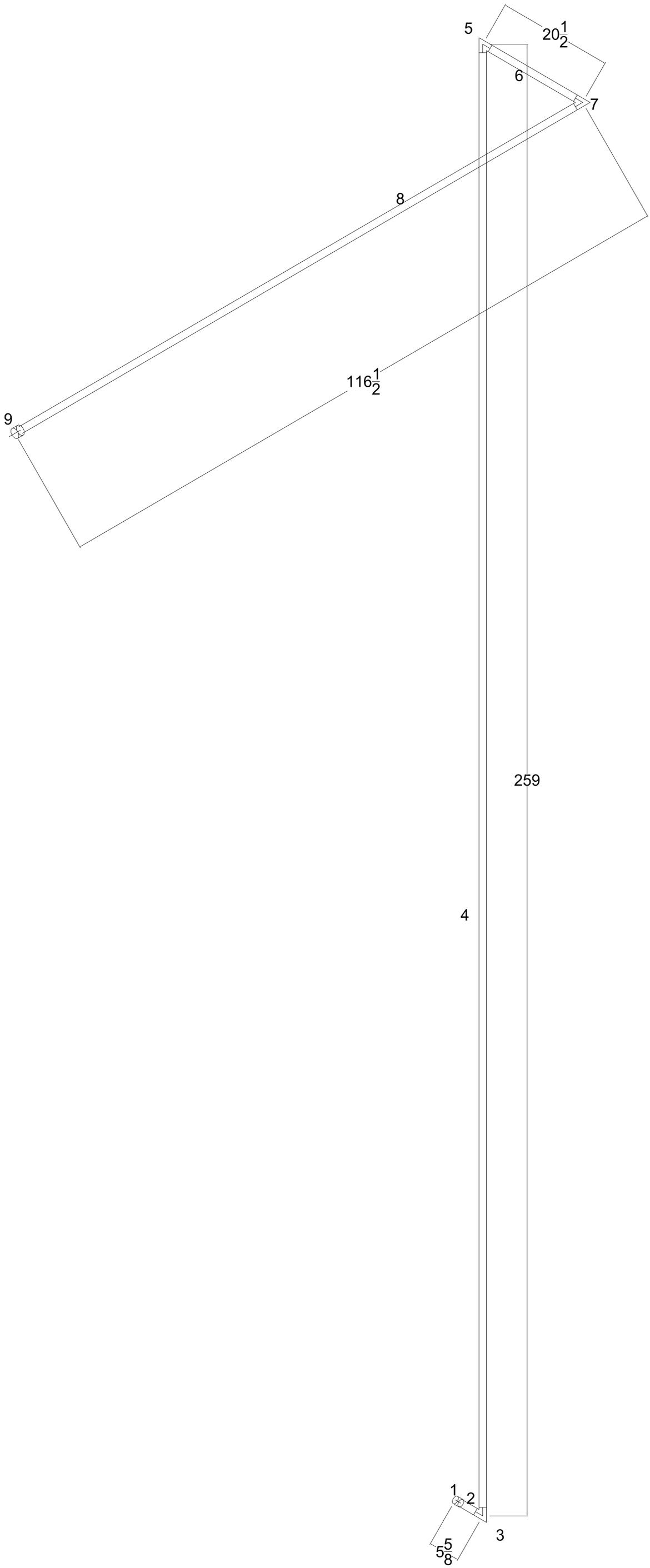




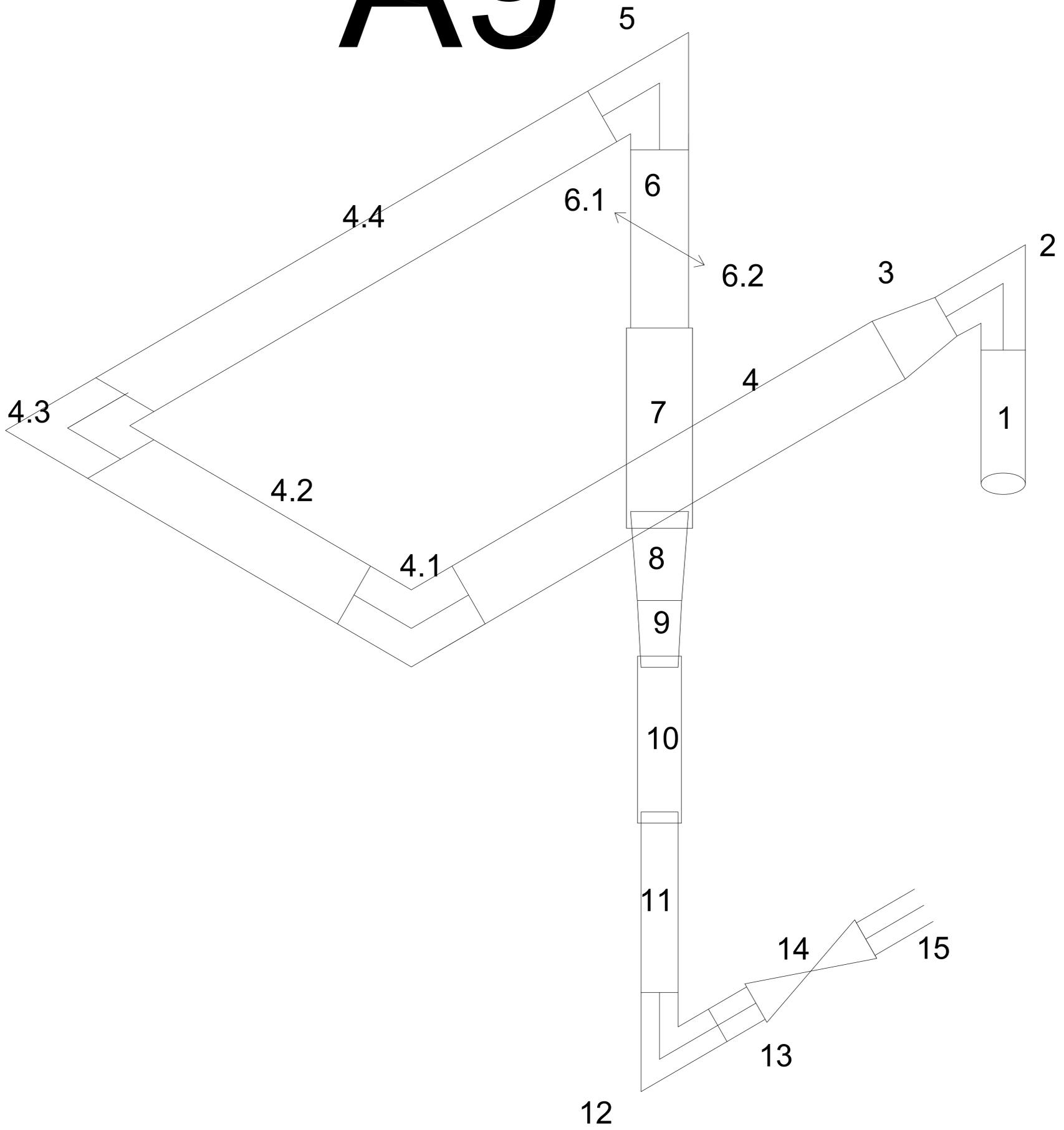


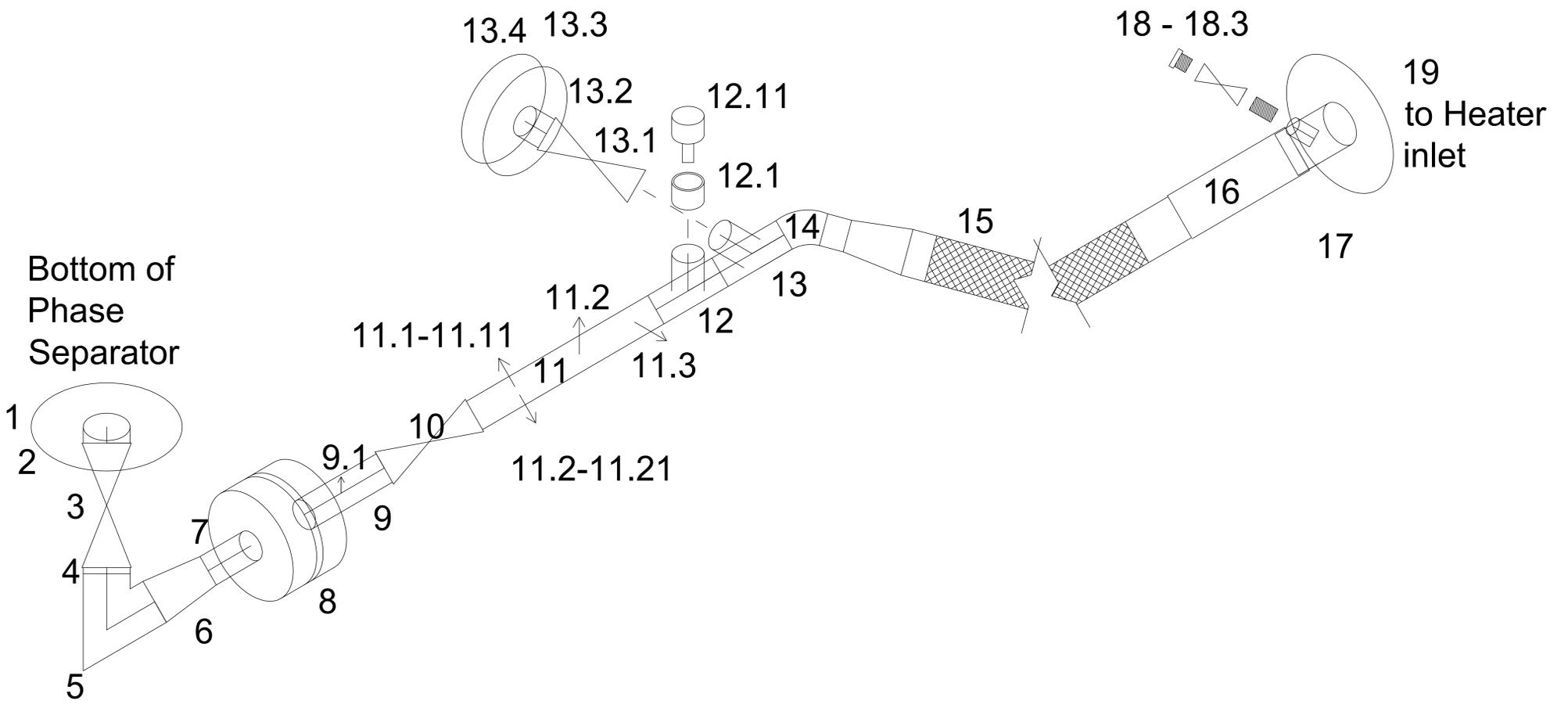




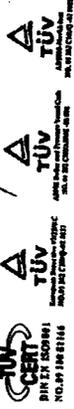


# A9





WL 52816006 n07  
WL 52816017 n19



WBS4498

# MILL INSPECTION CERTIFICATE

CHANGSHU WALSN SPECIALTY STEEL CO., LTD.  
EN10204 3.1



CUSTOMER:   
DATE OF ISSUE: 2009/07/09   
HEAT NO.: 3B712   
CONDITION: COLD FINISHED, ANNEALED, PICKLED, PLAIN END   
COMMODITY: STAINLESS STEEL SEAMLESS PIPES   
CERTIFICATE NO.: 200907098962006   
GRADE: TP304/304L

ELEMENTS	CHEMICAL COMPOSITION (WT%)															
	C	Si	Mn	P	S	Ni	Cr	Mo	N	Cu	Ti	Ch+Ta	Co	Al	V	B
SPECIFICATION	0.035	1.000	2.000	0.045	0.030	8.000	18.000									
RESULTS (LADLE)	0.017	0.3	1.77	0.025	0.002	8.52	18.32									
RESULTS (PRODUCT)	0.013	0.3	1.82	0.026	0.002	8.43	18.35									

SIZE NPS(T)*SCH(C)	PKG NO.	PIECES	WEIGHT		TS MPa	YS		EL %	HARDNESS HRB	FLATTENING TEST	FLARING TEST	I.C. TEST	GRAIN SIZE	HYDROSTATIC TEST	EDDY CURRENT TEST	ULTRASONIC TEST
			FT	(kg)		0.2% MPa	1% MPa									
1**80S	AC-13	53	1193	1204	545	285	290	57.5	79	GOOD	/	GOOD	/	/	GOOD	/
3/4**40S	AC-4	74	1627	856	590	290	290	64	78	GOOD	/	GOOD	/	/	GOOD	/
1**80S	DC-22	49	1124	1132	560	330	330	56.5	84	GOOD	/	GOOD	/	/	GOOD	/
1/2**80S	DC-29	99	2123	1062	565	245	245	60.5	75	GOOD	/	GOOD	/	/	GOOD	/
1/2**10S	DC-55	30	674	211	555	285	285	66	79	GOOD	/	GOOD	/	/	GOOD	/
TOTAL:		305	6741	4465												

REMARK:   
AS PER ASTM A312-98/A376-06, ASME SA312-07/SA376-07   
NACE MR0175-2003   
LENGTH: 2024FT   
AS PER PROFORMA INVOICE NO.: L26088   
I.C. TEST PER ASTM A262-02a E MIL-P24691/3 MIL-P1144D   
NO REPAIR BY WELDING   
MATERIAL FREE FROM MERCURY CONTAMINATION MELTED & MANUFACTURED IN CHINA   
ET standard practice: ASTM E426   
Reference discontinuity: drilled hole water quenched   
ANNEALING TEMPERATURE: 1060°C

1. WE HEREBY CERTIFY THAT THE MATERIAL DESCRIBED HEREIN BEEN MADE IN ACCORDANCE WITH THE RESULTS OF THE CONTRACT, AND CONFORM TO THE SPECIFICATION ABOVE.

2. THE CERTIFICATE SHALL NOT BE REPRODUCED EXCEPT IN FULL WITHOUT THE WRITTEN APPROVAL OF THE COMPANY.

**Bin Sun**

DIRECTOR, TECHNOLOGY

WLCS-QP-T24-06

# MILL INSPECTION CERTIFICATE

WL 58677022 v23



CHANGSHU WALSHIN SPECIALTY STEEL CO., LTD.

EN10204 3.1

WLPS4668

CUSTOMER: 2009/08/01  
 HEAT NO.: 38863  
 CONDITION: COLD FINISHED, ANNEALED, PICKLED, PLAIN END  
 CERTIFICATE NO.: 200908068962012  
 COMMODITY: STAINLESS STEEL SEAMLESS PIPES  
 GRADE: TP304/304L

ELEMENTS	CHEMICAL COMPOSITION (WT%)														
	C	Si	Mn	P	S	Ni	Cr	Mo	N	Cu	Ti	Co	Al	V	B
SPECIFICATION	min					8.000	18.000								
	max	0.035	1.000	2.000	0.045	0.050	20.000								
RESULTS (LADLE)		0.016	0.330	1.760	0.024	8.090	18.150								
RESULTS (PRODUCT)		0.014	0.339	1.762	0.025	8.072	18.136								

SIZE (mm) NPS (") * SCH (")	BUNDLE NO.	PIECES	WEIGHT		TS MPa	YS			EL %	HARDNESS HRB	FLATTENING TEST	FLARING TEST	I.C. TEST	GRAIN SIZE	HYDROSTATIC TEST	EDDY CURRENT TEST	ULTRASONIC TEST
			FT	(kg)		0.2%	1%										
1 1/2" * 40S	YH-2	40	883	1094	550/560	285/285	/	58/58	78/78	GOOD	/	GOOD	/	GOOD	/	GOOD	/
2" * 10S	2D-45	24	516	619	540	305	/	55.5	75	GOOD	/	GOOD	/	GOOD	/	GOOD	/
TOTAL:		64	1399	1713													

REMARK:  
 AS PER ASTM A312-08/A376-06-ASME SA312-07/SA376-07  
 NACE MR0175-2003  
 LENGTH : 20'24FT  
 AS PER PROFORMA INVOICE NO.: L26089  
 I.C. TEST PER ASTM A262-02a E MIL-P24691/3 MIL-P1144D  
 NO REPAIR BY WELDING  
 MATERIAL FREE FROM MERCURY CONTAMINATION  
 MELTED & MANUFACTURED IN CHINA  
 ET standard practice: ASTM E426  
 Reference discontinuity: drilled hole  
 ANNEALING TEMPERATURE: 1060°C  
 water quenched

1. WE HEREBY CERTIFY THAT THE MATERIAL DESCRIBED HEREIN BEEN MADE IN ACCORDANCE WITH THE RESULTS OF THE CONTRACT, AND CONFORM TO THE SPECIFICATION ABOVE.

2. THE CERTIFICATE SHALL NOT BE REPRODUCED EXCEPT IN FULL WITHOUT THE WRITTEN APPROVAL OF THE COMPANY.

**Bin Sun**

QUALITY MANAGER

# MILL INSPECTION CERTIFICATE

WL 65811007 ~ 08; WL 65811015 ~ 16



CHANGSHU WALSN SPECIALTY STEEL CO., LTD.  
EN10204 3.1

WIPSS491

CUSTOMER: 20100428  
HEAT NO.: 00910955  
CONDITION: COLD FINISHED, ANNEALED, PICKLED, PLAIN END  
CERTIFICATE NO.: 201004288962004  
COMMODITY: STAINLESS STEEL SEAMLESS PIPES  
GRADE: TP304/304L

ELEMENTS	CHEMICAL COMPOSITION (WT%)															
	C	Si	Mn	P	S	Ni	Cr	Mo	N	Cu	Ti	Ch+Ta	Co	Al	V	B
SPECIFICATION	min					8.000	18.000									
	max	0.750	2.000	0.045	0.030	11.000	20.000									
RESULTS (LADLE)		0.025	0.460	1.650	0.027	0.001	8.690	18.270								
RESULTS (PRODUCT)		0.025	0.497	1.505	0.021	8.547	18.459									

SIZE (mm)	BUNDLE NO.	PIECES	WEIGHT	TS		YS		EL (50mm)	HARDNESS	FLATTENING TEST	FLARING TEST	I.C. TEST	GRAIN SIZE	Lot No.	HYDROSTATIC TEST	EDDY CURRENT TEST	ULTRASONIC TEST
				MPa	MPa	0.2%	1%										
1*10S	K-2	55	1198.13	792	615605	340240	/	90.552	81/82	ACCEPTABLE	/	ACCEPTABLE	/	201002-A-335	/	ACCEPTABLE	/
3/4*40S	K-23	73	1610.53	835	655645	320310	/	59.959	82/81	ACCEPTABLE	/	ACCEPTABLE	/	201003-A-030	/	ACCEPTABLE	/
1 1/4*40S	K-35	24	552.43	591	635645	365280	/	53.905	85/86	ACCEPTABLE	/	ACCEPTABLE	/	201003-A-506	/	ACCEPTABLE	/
1 1/4*40S	K-36	23	526.67	563	635645	365280	/	53.905	85/86	ACCEPTABLE	/	ACCEPTABLE	/	201003-A-506	/	ACCEPTABLE	/
1 1/4*40S	K-37	25	574.15	606	620635	345255	/	56.525	83/84	ACCEPTABLE	/	ACCEPTABLE	/	201003-A-522	/	ACCEPTABLE	/
3/8*80S	K-86	60	1389.76	467	605605	275270	/	57.58	76/76	ACCEPTABLE	/	ACCEPTABLE	/	201003-A-106	/	ACCEPTABLE	/
3/8*80S	K-87	65	1494.36	503	605605	275270	/	57.58	76/76	ACCEPTABLE	/	ACCEPTABLE	/	201003-A-106	/	ACCEPTABLE	/
TOTAL:		325	7346.03	4357													

REMARK:  
AS PER ASTM A312-09/A376-06, ASME SA312-07/SA376-07  
NACE MR0175:2003  
LENGTH: 2024FT  
AS PER PROFORMA INVOICE NO. L27690  
I.C. TEST PER ASTM A262-02a E MIL-P24691/3 MIL-P1144D  
NO REPAIR BY WELDING  
MATERIAL FREE FROM MERCURY CONTAMINATION  
MELTED & MANUFACTURED IN CHINA  
ET standard practice: ASTM E426  
Reference discontinuity: drilled hole water quenched  
ANNEALING TEMPERATURE: 1060°C

Shun Yang

QUALITY MANAGER

WLCS-QP-T24-06







## PURCHASE REQUISITION

### Requisition

Requisition Number (Filled in by System)	Oracle Preparer (Filled in by System)	Date <b>08/05/10</b>	Request Originator: Erik Voirin	Extension: #5168
Division/Section Approval		Date	NEPA Approval	
Business Office Approval		Date		
Directorate Approval		Date		

### Requisition Header

Description (of entire requisition) <b>Swing Type Check Valves</b>	
Note to Approver For the CMS CO2 cooling system. Ref. Quote #7220652	
Justification (To Approver)	

### Requisition Entry Defaults

Requester <b>Erik Voirin</b>	Deliver-To-Location <b>Lab F</b>	Buyer Note (use attachments)		
Suggested Vendor <b>McJunkin</b>	Suggested Vendor Site 4026 MOUND ROAD JOLIET IL 60436	Suggested Vendor Contact <b>ANNE ALCORN</b>	Suggested Vendor Telephone: 815-729-7742	
Reference #	Need-By-Date <b>08/15/10</b>	Project/Task/Expenditure Type and Expenditure Organization 45A / 45A.20.16.2.11.3.1	Building Maintenance: Yes or <input checked="" type="radio"/> No (Circle One)	
Note to Receiver This is for CMS CO2 Cooling System			FIMS #	Total of Requisition \$1235.53

### Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
				Quantity	Unit of Measure	Price per Unit	Extended Price	
1	GR	Check Valve	6985-XXXX 1.0000 EA 305.1800 305.18 08/03/10 1/2" VELAN W03-2114C-14GX 600# 316SS SW CHECK VALVE (BORED OUT FROM THRD) ** AND CHANGED TO SX TRIM (TEFLON GSKT)	1	each	\$305.18	\$305.18	45A
								45A.20.16.2.11.3.1
								Material purchase
								CMS

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
				Quantity	Unit of Measure	Price per Unit	Extended Price	
2	GR	Check Valve	6985-XXXX 1.0000 EA 413.7500 413.75 08/03/10 1" VELAN W05-2114C-14GX 600# 316SS SW CHECK VALVE (BORED FROM THRD) ** CHANGED TO 13SX W/ TEFLON GSKT ***	1	Each	\$413.75	\$413.75	45A
								45A.20.16.2.11.3.1
								Material purchase
								CMS





## PURCHASE REQUISITION

### Requisition

Requisition Number (Filled in by System)	Oracle Preparer (Filled in by System)	Date <b>08/18/10</b>	Request originator: <b>Erik Voirin</b>	Extension: 5168 MS: 219
Division/Section Approval		Date	NEPA Approval	
Business Office Approval		Date		
Directorate Approval		Date		

### Requisition Header

Description (of entire requisition) <b>Manual Control Valve for regulating saturated mixture CO2 flow out of phase separation tank returning to storage tank.</b>
Note to Approver
Justification (To Approver)

### Requisition Entry Defaults

Requester <b>Erik Voirin</b>	Deliver-To-Location <b>Lab F</b>	Buyer Note (use attachments) (i.e., Previous PO)		
Suggested Vendors <b>FCX Performance Inc</b>	Suggested Vendor Site <b>55 N Lively Blvd Elk Grove Village, IL 60007-1618</b>	Suggested Vendor Contact <b>Michael McKee</b>	Suggested Vendors <b>Telephone # 847-806-1885</b>	
Reference #	Need-By-Date 09-10-2010	Project/Task/Expenditure Type and Expenditure Organization <b>45A / 45A.20.16.2.11.3.1</b>	Building Maintenance: Yes or No (Circle One) FIMS #	
Note to Receiver <b>This is for CMS CO2 Cooling System</b>			Total of Requisition <b>\$280.00</b>	

### Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's			
				Quantity	Unit of Measure	Price per Unit	Extended Price		Project	Task	Exp. Type
1	GR	Manual Control Valve	1pc Part Number- V8-SW-0050-SXX-3, 1/2" 3-Piece, 316SST BV Socket Weld Ends 30 Deg V-Port, 50% STFE Seats. Your cost \$280.00 Net.  UN Number _____ Hazard Class _____	1	each	\$280.00	\$280.00	45A	45A.20.16.2.11.3.1	Material purchase	CMS





















## PURCHASE REQUISITION

### Requisition

Requisition Number (Filled in by System)	Oracle Preparer (Filled in by System)	Date <b>07/15/10</b>	Request originator: <b>Erik Voirin</b>	Extension: 5168 MS: 219
Division/Section Approval		Date	NEPA Approval	
Business Office Approval		Date		
Directorate Approval		Date		

### Requisition Header

Description (of entire requisition) <b>Parts for pressure testing system for NOVA PVC modules</b>
Note to Approver
Justification (To Approver)

### Requisition Entry Defaults

Requester <b>Erik Voirin</b>	Deliver-To-Location <b>Lab F</b>	Buyer Note (use attachments) (i.e., Previous PO)		
Suggested Vendors <b>McMaster-Carr</b>	Suggested Vendor Site <b>200 Aurora Industrial Pkwy. Aurora, OH 44202-8087</b>	Suggested Vendor Contact	Suggested Vendors <b>Telephone #(330) 995-5500</b>	
Reference #	Need-By-Date 08-15-2010	Project/Task/Expenditure Type and Expenditure Organization <b>///PPD-425 NOVA 1.8.9.5 NOVA Assembly RD///</b>		Building Maintenance: Yes or No (Circle One) FIMS #
Note to Receiver <b>Parts for pressure testing system for NOVA PVC modules</b>				Total of Requisition <b>\$376.34</b>

### Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's		
				Quantity	Unit of Measure	Price per Unit	Extended Price		Project	Task
1	GR	Cylinder Regulator	7897A65	1	each	\$102.35	\$102.35	425	1.8.9.5	Material purchase  NOVA
			Gas Pressure Regulator Std Duty, 1-Stage, Argon, 0-100 PSI, Cga #580							
			<i>In stock</i> at \$102.35 Each							
			UN Number							

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
2	GR	Thread adaptor	7919A51 Welding Hose Fitting Brass Adapter, 1/4" NPT Male to 9/16"-18 Female Rh <i>In stock</i> at \$8.79 Each	Quantity	1	Project	425	
				Unit of Measure	each	Task	1.4.6.5	
				Price per Unit	\$8.79	Exp. Type	Material purchase	
				Extended Price	\$8.79	Exp. Org.	NOVA	
			UN Number	Hazard Class				
3	GR	Tube fitting	5520K174 Solder-Joint Copper Tube Fitting for Water Female Reducing Adapter for 1/8" Tube Sz, 1/4" NPT <i>In stock</i> at \$3.56 Each	Quantity	1	Project	425	
				Unit of Measure	Each	Task	1.4.6.5	
				Price per Unit	\$3.56	Exp. Type	Material purchase	
				Extended Price	\$3.56	Exp. Org.	NOVA	
			UN Number	Hazard Class				
4	GR	Tube fitting	5520K121 Solder-Joint Copper Tube Fitting for Water Male Reducing Adapter for 1/8" Tube Size, 1/4" NPT <i>In stock</i> at \$4.26 Each	Quantity	1	Project	425	
				Unit of Measure	Each	Task	1.4.6.5	
				Price per Unit	\$4.26	Exp. Type	Material purchase	
				Extended Price	\$4.26	Exp. Org.	NOVA	
			UN Number	Hazard Class				
5	GR	Pressure regulator	1888K1 Aluminum Body HI-Flow Precision Air Regulator 1/4" Pipe, 80 Maximum SCFM @ 100 PSI \$71.96 Each	Quantity	1	Project	425	
				Unit of Measure	each	Task	1.4.6.5	
				Price per Unit	\$71.96	Exp. Type	Material purchase	
				Extended Price	\$71.96	Exp. Org.	NOVA	
			UN Number	Hazard Class				



Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
				Quantity	Unit of Measure	Price	Project	
10	GR	Pipe fitting	<p style="text-align: center;">4429K226</p> Low-Pressure Brass Threaded Pipe Fitting 1/2" X 1/4" X 1/2" Pipe Size, Reducing Tee <i>In stock</i> at \$9.01 Each  UN Number _____ Hazard Class _____	Quantity	1	Project	425	
				Unit of Measure	Each	Task	1.4.6.5	
				Price per Unit	\$9.01	Exp. Type	Material purchase	
				Extended Price	\$9.01	Exp. Org.	NOVA	
11	GR	Threaded pipe	<p style="text-align: center;">9176K133</p> Std-Wall Chrm-Pltd Brass Threaded Pipe Nipple 3/8" Pipe Size X 2" L, 13/32" Thread Length, Sch 40 <i>In stock</i> at \$4.47 Each  UN Number _____ Hazard Class _____	Quantity	1	Project	425	
				Unit of Measure	Each	Task	1.4.6.5	
				Price per Unit	\$4.47	Exp. Type	Material purchase	
				Extended Price	\$4.47	Exp. Org.	NOVA	
12	GR	Ball valve	<p style="text-align: center;">47865K22</p> Brass Ball Valve 3/8" NPT Female Connections <i>In stock</i> at \$7.62 Each  UN Number _____ Hazard Class _____	Quantity	1	Project	425	
				Unit of Measure	Each	Task	1.4.6.5	
				Price per Unit	\$7.62	Exp. Type	Material purchase	
				Extended Price	\$7.62	Exp. Org.	NOVA	
13	GR	Hose fitting	<p style="text-align: center;">5346K65</p> Brass Barbed Hose Fitting Adapter for 5/8" Hose ID X 3/8" NPTF Male Pipe <i>In stock</i> at \$8.49 per Pack  UN Number _____ Hazard Class _____	Quantity	1	Project	425	
				Unit of Measure	Each	Task	1.4.6.5	
				Price per Unit	\$8.49	Exp. Type	Material purchase	
				Extended Price	\$8.49	Exp. Org.	NOVA	









## PURCHASE REQUISITION

### Requisition

Requisition Number (Filled in by System)	Oracle Preparer (Filled in by System)	Date <b>09/07/10</b>	Request originator: <b>Erik Voirin</b>	Extension: 5168 MS: 219
Division/Section Approval		Date	NEPA Approval	
Business Office Approval		Date		
Directorate Approval		Date		

### Requisition Header

Description (of entire requisition) <b>Orifice Flange for CMS CO2 Test Stand Flowmeter</b>
Note to Approver
Justification (To Approver)

### Requisition Entry Defaults

Requester <b>Erik Voirin</b>	Deliver-To-Location <b>Lab F</b>	Buyer Note (use attachments) (i.e., Previous PO)		
Suggested Vendors <b>Specialty Flange &amp; Fitting, Inc</b>	Suggested Vendor Site <b>649 Lebanon Avenue Williamstown, NJ 08094</b>	Suggested Vendor Contact	Suggested Vendors <b>Phone #(856) 728-8530</b>	
Reference #	Need-By-Date 9/30/2010	Project/Task/Expenditure Type and Expenditure Organization <b>45A / 45A.20.16.2.11.3.1</b>		Building Maintenance: <b>No</b>
Note to Receiver				Total of Requisition
<b>Company does not accept credit cards – Fax# (856) 728-1304 – see line 3</b>				<b>\$443.00</b>

### Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
				Quantity	Unit of Measure	Price per Unit	Extended Price	
1	GR	Pipe Fittings	Orifice Flanges - 1" 600# 304 Stainless Steel. Slip-on raised face ½"NPT Taps Includes SS Bolts gaskets and nuts	1			45A	
					pair		45A.20.16.2.11.3.1	
				\$ 298.00		Material purchase		
				\$298.00		CMS		
			UN Number		Hazard Class			

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
				Quantity	Unit of Measure	Project	Task	
2	GR	Pipe Fittings	Orifice Plate For above 1" 600# flange 304 Stainless Steel Center bored with 0.290" orifice  UN Number _____ Hazard Class _____	1	each	45A	45A.20.16.2.11.3.1	
					\$ 70	Material purchase		
					\$70	CMS		

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
				Quantity	Unit of Measure	Project	Task	
3	GR	Pipe Fittings	Orifice Plate For 1.5" 600# flange 304 Stainless Steel Furnished Blank (no orifice hole) <b>Please Provide gaskets for orifice plate, If additional charge is necessary, add to total price.</b>  UN Number _____ Hazard Class _____	1	each	45A	45A.20.16.2.11.3.1	
					\$ 75	Material purchase		
					\$75	CMS		



Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's	
				Quantity	Unit of Measure	Price	Project		Task
2	GR	Pipe Fittings	45735K253 Thin-Wall 304/304L SS Butt-Weld Pipe Fitting Unthreaded, 1" Pipe Size, Tee, Schedule 10 In stock at \$18.13 Each  UN Number _____ Hazard Class _____	6	each		45A		
						\$ 18.13			45A.20.16.2.11.3.1
									Material purchase
						\$108.78			CMS

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's	
				Quantity	Unit of Measure	Price	Project		Task
3	GR	Pipe Fittings	44965K458 Unthreaded HI-Pressure SS Sckt-Weld Fitting 304 SS, 1-1/2" Pipe Size, Coupling In stock at \$31.65 Each  UN Number _____ Hazard Class _____	2	each		45A		
						\$ 31.65			45A.20.16.2.11.3.1
									Material purchase
						\$63.30			CMS

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's	
				Quantity	Unit of Measure	Price	Project		Task
4	GR	Pipe Fittings	44965K456 Unthreaded HI-Pressure SS Sckt-Weld Fitting 304 SS, 1" Pipe Size, Coupling In stock at \$15.50 Each  UN Number _____ Hazard Class _____	1	each		45A		
						\$ 15.50			45A.20.16.2.11.3.1
									Material purchase
						\$15.50			CMS

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's	
				Quantity	Unit of Measure	Price	Project		Task
5	GR	Pipe Fittings	45735K321 Thin-Wall 304/304L SS Butt-Weld Pipe Fitting Unthreaded, 1" 90 Degree Short Radius Elbow, Sch 10 In stock at \$37.07 Each  UN Number _____ Hazard Class _____	16	each		45A		
						\$ 37.07			45A.20.16.2.11.3.1
									Material purchase
						\$593.12			CMS

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's	
				Quantity	Unit of Measure	Price	Project		Task
6	GR	Pipe Fittings	45735K323  Thin-Wall 304/304L SS Butt-Weld Pipe Fitting Unthreaded, 1-1/2" 90 Deg Short Radius Elbow, Sch 10 In stock at \$39.49 Each  UN Number _____ Hazard Class _____	7	each	\$ 39.49	45A	Material purchase	
							45A.20.16.2.11.3.1		
						\$276.43	Exp. Org.	CMS	

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's	
				Quantity	Unit of Measure	Price	Project		Task
7	GR	Pipe Fittings	45735K211  Thin-Wall 304/304L SS Butt-Weld Pipe Fitting Unthreaded, 1/2" 90 Deg Long Radius Elbow, Sch 10 In stock at \$5.04 Each  UN Number _____ Hazard Class _____	5	each	\$ 5.04	45A	Material purchase	
							45A.20.16.2.11.3.1		
						\$25.20	Exp. Org.	CMS	

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's	
				Quantity	Unit of Measure	Price	Project		Task
8	GR	Pipe Fittings	45735K231  Thin-Wall 304/304L SS Butt-Weld Pipe Fitting Unthreaded, 1/2" 45 Degree Elbow, Schedule 10 In stock at \$6.45 Each  UN Number _____ Hazard Class _____	1	each	\$ 6.45	45A	Material purchase	
							45A.20.16.2.11.3.1		
						\$6.45	Exp. Org.	CMS	

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's	
				Quantity	Unit of Measure	Price	Project		Task
9	GR	Pipe Fittings	4565T332  HI-Pressure 304/304L SS Weld-on Pipe Fitting Threaded, 1/2" Outlet, Fits 3/4" to 36" Pipe Size  UN Number _____ Hazard Class _____	2	each	\$ 34.50	45A	Material purchase	
							45A.20.16.2.11.3.1		
						\$69.00	Exp. Org.	CMS	



Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's		
				Quantity	Unit of Measure	Price	Project		Task	Exp. Type
14	GR	Pipe Fittings	45735K413  Thin-Wall 304/304L SS Butt-Weld Pipe Fitting Unthrd, 1" X 3/4" Pipe Size, Reducing Cplg, Sch 10  UN Number _____ Hazard Class _____	3	each		45A			
						\$ 13.30		45A.20.16.2.11.3.1	Material purchase	
						\$39.90				CMS

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's		
				Quantity	Unit of Measure	Price	Project		Task	Exp. Type
15	GR	Pipe Fittings	4475K64  Thick-Wall 316/316L SS Thrd Seamless Nipple 1/2" Pipe Sz, 3/4" OD, 5" L, 13/16" Thread Length In stock at \$20.34 Each  UN Number _____ Hazard Class _____	1	each		45A			
						\$ 20.34		45A.20.16.2.11.3.1	Material purchase	
						\$20.34				CMS

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's		
				Quantity	Unit of Measure	Price	Project		Task	Exp. Type
16	GR	Pipe Fittings	51205K202  Extreme-Pressure 316 SS Threaded Pipe Fitting 3/4" X 1/2" Pipe Size, Hex Nipple, 6600 Max PSI In stock at \$23.06 Each  UN Number _____ Hazard Class _____	1	each		45A			
						\$ 23.06		45A.20.16.2.11.3.1	Material purchase	
						\$23.06				CMS

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
				Quantity	Unit of Measure	Price	Project	
17	GR	Pipe Fittings	48805K911  Precision Threaded Type 316 SS Pipe Fitting 1/2" X 1/2" Pipe, 1-7/8" Lg, Hex Nipple, 6600 PSI	Quantity	1	Project	45A	
				Unit of Measure	each	Task	45A.20.16.2.11.3.1	
				Price per Unit	\$ 14.87	Exp. Type	Material purchase	
				Extended Price	\$14.87	Exp. Org.	CMS	
			UN Number				Hazard Class	

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
				Quantity	Unit of Measure	Price	Project	
18	GR	Pipe Fittings	4565T312  HI-Pressure 304/304L SS Weld-on Pipe Fitting Threaded, 1/4" Outlet, Fits 1/2" to 36" Pipe Size	Quantity	6	Project	45A	
				Unit of Measure	each	Task	45A.20.16.2.11.3.1	
				Price per Unit	\$ 26.22	Exp. Type	Material purchase	
				Extended Price	\$157.32	Exp. Org.	CMS	
			UN Number				Hazard Class	

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
				Quantity	Unit of Measure	Price	Project	
19	GR	Pipe Fittings	4565T371  HI-Pressure 304/304L SS Weld-on Pipe Fitting Threaded, 1-1/2" Outlet, Fits 1-1/2" Pipe Size	Quantity	2	Project	45A	
				Unit of Measure	each	Task	45A.20.16.2.11.3.1	
				Price per Unit	\$ 91.83	Exp. Type	Material purchase	
				Extended Price	\$183.66	Exp. Org.	CMS	
			UN Number				Hazard Class	

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
				Quantity	Unit of Measure	Price	Project	
20	GR	Pipe Fittings	4565T351  HI-Pressure 304/304L SS Weld-on Pipe Fitting Threaded, 1" Outlet, Fits 1" Pipe Size	Quantity	7	Project	45A	
				Unit of Measure	each	Task	45A.20.16.2.11.3.1	
				Price per Unit	\$ 54.24	Exp. Type	Material purchase	
				Extended Price	\$379.68	Exp. Org.	CMS	
			UN Number				Hazard Class	

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
21	GR	Pipe Fittings	4565T331  HI-Pressure 304/304L SS Weld-on Pipe Fitting Threaded, 1/2" Outlet, Fits 1/2" Pipe Size  UN Number <span style="float: right;">Hazard Class</span>	Quantity	1	Project	45A	
				Unit of Measure	each	Task	45A.20.16.2.11.3.1	
				Price per Unit	\$ 34.50	Exp. Type	Material purchase	
				Extended Price	\$34.50	Exp. Org.	CMS	

*Requisition Lines*

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
22	GR	Pipe Fittings	4565T352  HI-Pressure 304/304L SS Weld-on Pipe Fitting Threaded, 1" Outlet, Fits 1-1/4" to 2-1/2" Pipe Size In stock at \$54.24  UN Number <span style="float: right;">Hazard Class</span>	Quantity	1	Project	45A	
				Unit of Measure	each	Task	45A.20.16.2.11.3.1	
				Price per Unit	\$ 54.24	Exp. Type	Material purchase	
				Extended Price	\$54.24	Exp. Org.	CMS	

*Requisition Lines*

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
23	GR	Pipe Fittings	4443K752  High-Pressure 316 SS Threaded Pipe Fitting 1/2" Male X 1/4" Female NPT, Hex Bushing, 3000 PSI  UN Number <span style="float: right;">Hazard Class</span>	Quantity	1	Project	45A	
				Unit of Measure	each	Task	45A.20.16.2.11.3.1	
				Price per Unit	\$ 5.05	Exp. Type	Material purchase	
				Extended Price	\$5.05	Exp. Org.	CMS	

*Requisition Lines*

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
24	GR	Pipe Fittings	4565T432  HI-Pressure 304/304L SS Weld-on Pipe Fitting Socket, 1/2" Outlet, Fits 3/4" to 36" Pipe Size  UN Number <span style="float: right;">Hazard Class</span>	Quantity	1	Project	45A	
				Unit of Measure	each	Task	45A.20.16.2.11.3.1	
				Price per Unit	\$ 34.50	Exp. Type	Material purchase	
				Extended Price	\$34.50	Exp. Org.	CMS	

*Requisition Lines*



















**Requisition Lines**

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's	
				Quantity	Unit of Measure	Price	Project		Task
2	GR	Pipe	1 Sections – avg. length 23 feet 153-216 Ft. (9 Random Lengths) 1 Sch 10 T304/304L Seamless Pipe \$5.525/Ft.  UN Number Hazard Class	23			45A		
					ft			45A.20.16.2.11.3.1	
						\$5.525	Exp. Type	Material purchase	
						\$127.08	Exp. Org.	CMS	

**Requisition Lines**

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's	
				Quantity	Unit of Measure	Price	Project		Task
3	GR	Pipe	3 Sections – avg. length 23 feet 153-216 Ft. (9 Random Lengths) 1.5 Sch 10 T304/304L Seamless Pipe \$5.42/Ft.  UN Number Hazard Class	184.5			45A		
					ft			45A.20.16.2.11.3.1	
						\$7.875	Exp. Type	Material purchase	
						\$181.13	Exp. Org.	CMS	

**Requisition Lines**

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's	
				Quantity	Unit of Measure	Price	Project		Task
3	GR	Pipe	Contingency for random lengths for this and previous order  UN Number Hazard Class	1			45A		
					-			45A.20.16.2.11.3.1	
						\$63.02	Exp. Type	Material purchase	
						\$63.02	Exp. Org.	CMS	







Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
				Quantity	Unit of Measure	Project	Task	
2	GR	Fasteners	<b>SKU: 0187842</b>  3/4"-10x4-1/4" (OAL 4-1/2") A320 L7 Fully Threaded Stud w/ Gr7 Nuts  UN Number _____ Hazard Class _____	56	each	45A	45A.20.16.2.11.3.1	
						Exp. Type	Material purchase	
						Exp. Org.	CMS	

Requisition Lines

Line #	Line Type	PO Line Category	Description (Start with a Noun) (240 Characters Maximum, Enter Additional Description in Cell Below Line Item)	Quantity, Unit of Measure and Price		Project Information		Split Coding Qty's
				Quantity	Unit of Measure	Project	Task	
3	GR	Fasteners	<b>SKU: 0187809</b>  5/8"-11x3-1/4" (OAL 3-1/2") A320 L7 Fully Threaded Stud w/ Gr7 Nuts  UN Number _____ Hazard Class _____	22	Each	45A	45A.20.16.2.11.3.1	
						Exp. Type	Material purchase	
						Exp. Org.	CMS	













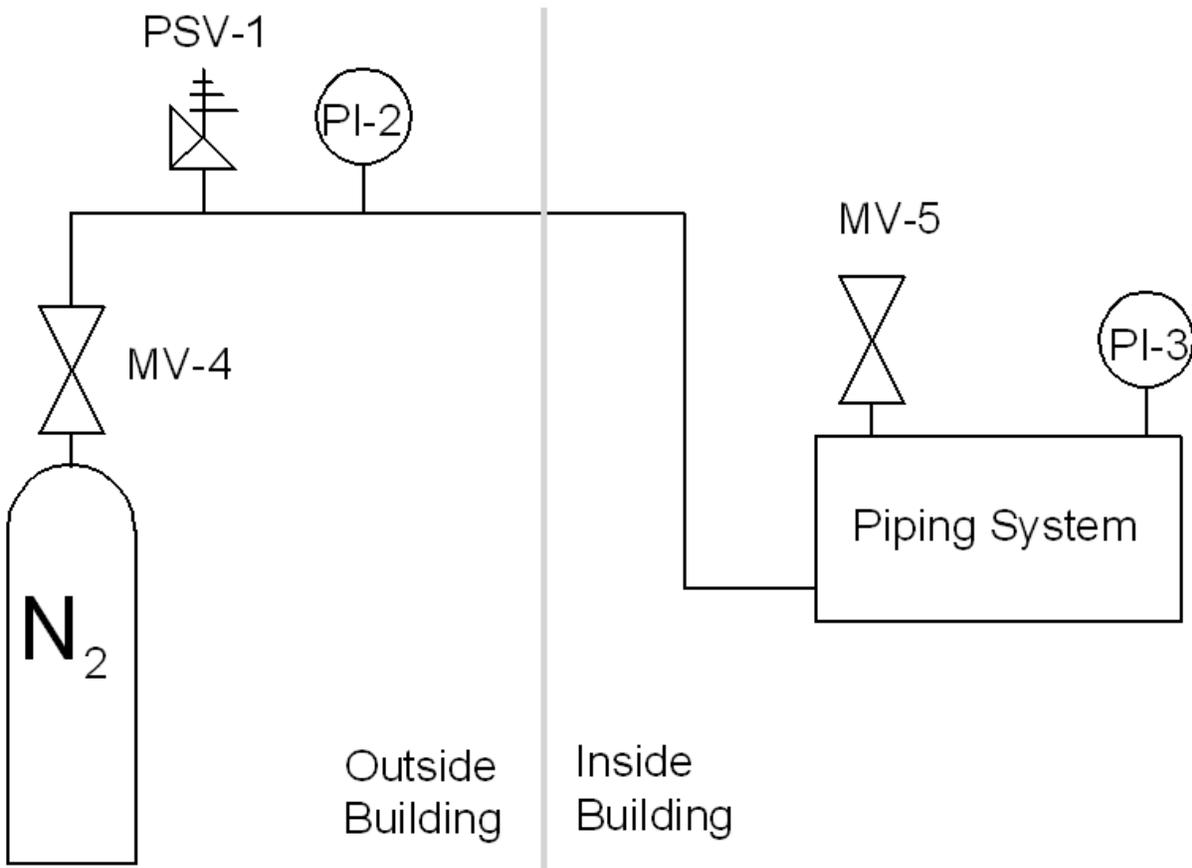
## **9. Leak / Pressure Test Procedures**

## APPENDIX G

### PRESSURE TESTING INFORMATION

#### Testing Procedures:

The CMS CO<sub>2</sub> Piping Network will be leak checked and pressure tested in accordance with FESHM 5034 and ASME 31.3 code for process piping. The Layout of the pressure test will be as in the diagram below.



The proposed leak and pressure test will begin once Lab C is cleared of all personnel and the building is blocked of all through traffic. The Main Storage Tank will be blocked off with plates as it has been previously tested and will not be included in this test. The nitrogen supply cylinder will be located outside of the building and be connected to the CO<sub>2</sub> Piping by a ¼" copper tube. The cylinder will contain a relief valve (PSV-1) set to 1350 psi as close as possible after

the manual valve on the cylinder. The cylinder will be run without a regulator due to a regulator being unable to supply the high pressure involved in the test. A pressure gauge (PI-2) will follow the relief valve, then the copper tubing will route into the building and attach to a ¼" fitting on the piping network.

### **Pressure Step 1: 25 psi**

Pressurization will begin by slowly opening the valve and pressurizing to 25psi as given by PI-2. At this time MV-4 will be closed and the system pressure monitored for pressure holding in an attempt to find gross leaks. After 3 minutes, testers will enter the building and bubble test all welds, joints, and flex hoses for leaks.

### **Pressure Step 2: 330 psi**

If no leaks are found the pressure will be raised slowly to 330 psi, and held for 5 minutes monitoring the system pressure for changes via PI-2. If the pressure decreases, implying a leak, the system pressure will be reduced by throttling MV-5 back to pressure step 1 (25 psi) where another bubble test will be performed in an attempt to locate the leak. If the system pressure does not decrease as seen on PI-2 pressurization will proceed to pressure step 3.

### **Pressure Step 3: 660 psi**

The pressure will be raised slowly to 660 psi, and held for 5 minutes monitoring the system pressure for changes via PI-2. The previous circumstances for moving to the next pressure step or reducing pressure and bubble testing will be followed in this pressure step as well as any subsequent pressure steps.

### **Pressure Step 4: 990 psi**

The pressure will be raised slowly to 990 psi, and held for 5 minutes monitoring the system pressure for changes via PI-2.

### **Pressure Step 5: 1320 psi**

The pressure will be raised slowly to 990 psi, and held for 10 minutes monitoring the system pressure for changes via PI-2.

### **Pressure Step 6: 1200 psi**

The pressure will be decreased slowly to 1200 psi as indicated by PI-2. The pressure reading of PI-3 will be noted at this time as well. All joints, welds, gaskets and flex hoses will be visually examined and bubble tested. If all piping areas pass the visual inspection and the readings of PI-2 and PI-3 have not decreased, the system will be considered to pass the leak and pressure test.

### **Relieving Pressure**

MV-5 will be slowly opened and the system pressure slowly decreased back to atmospheric.

## Testing Equipment:

- Test Pressure Fluid:
  - Pneumatic Test Using compressed nitrogen cylinder.
- Test Pressure:
  - 110% of design pressure.  $110\% * 1200 \text{ psi} = 1320 \text{ psi}$
- Relief Valve: (PSV-1)
  - Tamper-Resistant Adj Steel Relief Valve 1/4 NPT Male Inlet, 1/4 NPT Fem Outlet, 900-2000 PSI
  - Purchased from McMaster-Carr Part #5026K31
- Supply Tubing:
  - 1/4" OD by 0.030" wall rated at 1593 psi MAWP
  - Purchased from Fermilab Stockroom: [1065-006000](#)

American Society of  
Mechanical Engineers Code for  
Pressure Piping (ASME B31):

$$P = \frac{2S(t_{\min} - C)}{D_{\max} - 0.8(t_{\min} - C)}$$

where:

P = allowable pressure, psi

S = maximum allowable stress in  
tension, psi

$t_{\min}$  = wall thickness (min.), in.

$D_{\max}$  = outside diameter (max.), in.

C = a constant

$$C := 0$$

$$S := 6000 \text{ psi}$$

$$t_{\min} := 0.030 \text{ in}$$

$$D_{\max} := 0.25 \text{ in}$$

$$P := \frac{2 \cdot S \cdot (t_{\min} - C)}{D_{\max} - 0.8(t_{\min} - C)} = 1593 \text{ psi}$$

- Test Gauges: ( PI-2 and PI-3 )
  - Multipurpose Gauge +/-2% MID-Scale Accuracy 2-1/2" Dial, 1/4" NPT Male Bottom, 0 - 2000 PSI
  - Purchased from McMaster-Carr; Item 4089K712
  - Quantity = 2 for cross referencing.
- Manual Valve: ( MV-5 )
  - Sharpe 1/4" 99 Series Valve (standard valve on CO<sub>2</sub> piping system)