

**BELOW-THE-HOOK LIFTING DEVICE**  
**Engineering Note Cover Page**

Lifting Device Numbers:

FNAL Site No/	Div. Specific No.	178 Modified	Asset No.
		for	
		MicroBooNE	
		Vessel Lift	
_____	_____	_____	_____
If applicable	If applicable	If applicable	If applicable
ASME B30.20 Group:	<input checked="" type="checkbox"/> Group I	Structural and Mechanical Lifting Devices	
(check one)	<input type="checkbox"/> Group II	Vacuum Lifting Devices	
	<input type="checkbox"/> Group III	Magnets, Close Proximity Operated	
	<input type="checkbox"/> Group IV	Magnets, Remote Operated	

Device Name or Description \_\_\_\_\_

Device was  Purchased from a Commercial Lifting  
Device Manufacturer. Mfg Name \_\_\_\_\_

(check all  Designed and Built at Fermilab  
applicable)

Designed by Fermilab and Built by a  
Vendor. Assy drawing number \_\_\_\_\_

Provided by a User or other Laboratory  
 Other: Describe \_\_\_\_\_

Engineering Note Prepared by R. J. Woods Date 1/7/2013Engineering Note Reviewed by Amy Lee Date 1-10-2013

Lifting Device Data:

Capacity 40,000#Fixture Weight 6,000# As modifiedService:  normal  heavy  severe (refer to B30.20 for definitions)Duty Cycle N.A. 8, 16 or 24 hour rating (applicable to groups III, and IV)Inspections Frequency Before each use

Rated Load Test by FNAL (if applicable)	Date	Load	Previously tested for
_____	_____	_____	80,000#

 Check if Load Test was by Vendor and attach the certificate

Satisfactory Load Test Witnessed by: \_\_\_\_\_

Signature (of Load Test Witness) \_\_\_\_\_

Notes or Special Information:

This fixture was originally designed and used for a 80,000 pound lifted load. The W24X62 Cross Beam assembly was relocated to the center of the Transverse Beams.

## Particle Physics Division

### Mechanical Department Engineering Note

Number: MD-ENG-455

Date: 7 January, 2013

Project: MicroBooNE

Project Internal Reference:

Title: Modification of Lifting Fixture #178 for MicroBooNE Vessel

Author(s): R. J. Woods

Reviewer(s):

Key Words:

Abstract/Summary:

Lifting fixture 178 was previously designed and tested for lifting NOvA FHEP Table sections at CDF. The original design load was 80,000 pounds. In order to lift a vessel for MicroBooNE, this fixture was slightly modified by moving the W24X62 cross beam assembly to the center of the W27X84 Longitudinal beams and adding two HSS 3X3 square tubes, one at each end, spanning between these W27X84 beams. These tubes were necessary since the spacing of the lifting lugs on the fixture is 116.5 inches while the spacing of the lugs on the vessel is 143.6 inches. This would produce a small horizontal load that would induce torsion in the W27X84 beams. The tubes take the load in tension, eliminating this twisting force. The new design load is 40,000 pounds, one half of the original design load. For this reason, all the calculations for the original fixture in Engineering Note MD-ENG-283 are still valid. Only the differences caused by the modifications are covered here.

Applicable Codes:

ASME B30.20

AISC Manual of Steel Construction, Ninth Edition

CHECK MOMENT IN W27X34 BEAM DUE TO RELOCATION  
OF W64X62 BEAM ASSEMBLY:

USE LOAD CASE 7, AISC P. 298

$$\text{TOTAL LOAD OF VESSEL} = 40,000 \#$$

$$\text{LOAD ON EACH BEAM} = 40,000/2 = 20,000 \#$$

$$M = Pl/4 = 20,000(174.25)/4 \\ = 871,250 \#-IN$$

$$f_b = M/S = 871,250/213 \\ = 4090 \text{ PSI}$$

FROM ENCL. NOTE MW-ENCL-283

$$\text{ALLOWABLE BEARING STRESS} = 11,880 \text{ PSI} > 4090$$

OK

LIFTING FIXTURE 178 CAN BE USED  
TO LIFT MICROBOONE VESSEL

WIDTH OF LIFTING FIXTURE LUGS = 116.5"  
 WIDTH OF VESSEL LUGS = 71.804 x 2 = 143.6"

$$143.6 - 116.5 = 27.1" \quad (\text{SEE FIG. 1 FOR DIMS.})$$

$$27.1/2 = 13.6" \text{ PER SIDE}$$

USING 6'-0" SLINGS

$$\text{LIFT ANGLE} = \sin^{-1} 13.6/72 \\ = 10.9^\circ$$

$$\text{SLING LOAD} = 10,000 \# / \cos A \\ = 10,000 / \cos 10.9 = 10,184 \#$$

$$\text{HORIZ. LOAD} = 10,000 \times \tan 10.9 = 1926 \#$$

CHECK TENSION ON 3x3x1/4 TUBE ATUBE =

$$1926 \# / 2.59102 = 744 \text{ PSI}$$

$$\text{FOR LIFTING FIXTURE } F_T = 1/3 (46,000 \text{ PSI}) \\ = 15,330 \text{ PSI} > 744 \text{ PSI}$$

OK

Using 4 BOLTS:

$$\text{LOAD/BOLT} = 744/4 \\ = 186 \#/\text{BOLT}$$

$$F_t = 44.0 \text{ ksi FOR GRADE 5 BOLTS}$$

Assume 3/4"  $\phi$  BOLTS

$$F_t = 44/3 (.4418) = 6.5 \text{ k/BOLT}$$

$$6,500 \# > 186 \# \text{ OK}$$

WELD BETWEEN PLATE & TUBE

FOR 3/16" FILLET

$$F_t = (70(.707)(3/16))/3 = 3.09 \text{ k/in}$$

$$\text{OR } F_t = 0.3(70)(.707)(3/16) = 2.78 \text{ k/in (USE TAB J2.5 p 5-70)}$$

USE 2.78 k/in

2" PER FACE OF GOOD WELD

$$\text{TOTAL WELD} = 2(4)(2.78) = 22.2 \text{ k}$$

$$22,200 \# > 1926 \# \text{ OK}$$

USE HIGH 3x3x1/4 W/ 1/2" PLATE EA END  
 CONNECT TO EXIST. FRAME W/ 4 - 3/4"  $\phi$  GRADE 5  
 BOLTS EA. END.

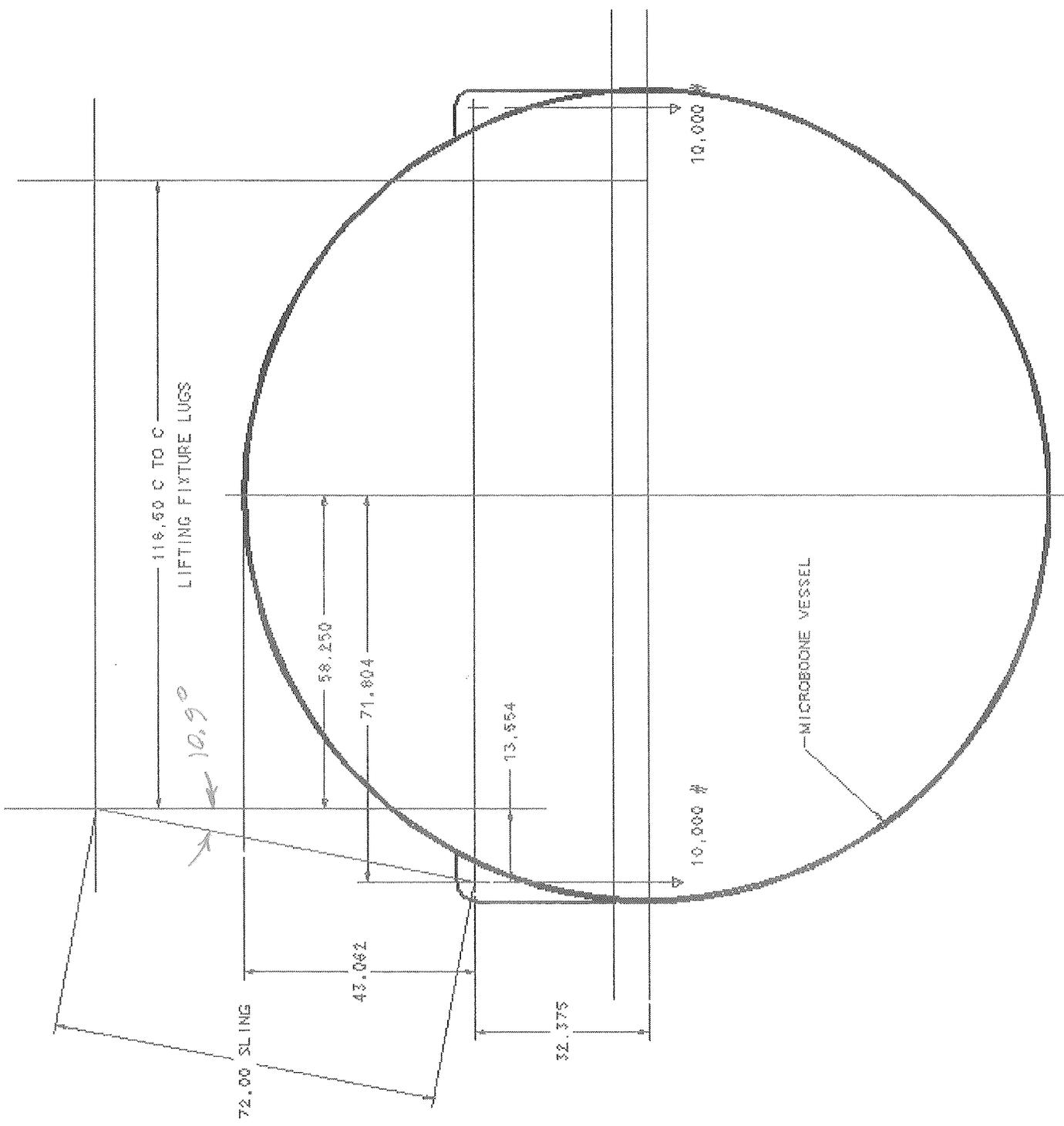


FIGURE 1